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| CMR INSTITUTE OF TECHNOLOGY | | USN <input type="text"/> | | | | | |  | |
| Internal Assessment test I | | | | | | | | | |
| Sub: | Design of RC structural elements | | | | | | Code | 15CV51 | |
| Date: | 06-09-19 | Duration : | 90 mins | Max Marks: | 50 | Sem: | 05 | Branch: | CIVIL |
| Note: Answer all the questions. Assume any missing data. Use of IS456 -2000 is permitted. | | | | | | | | | |
| | | | | | | | Marks | OBE | |
| | | | | | | | | CO | RBT |
| 1 (a) | Clearly state the five differences between working stress method and limit state method. | | | | | | [05] | C504.1 | |
| (c) | Derive stress block parameters for a singly reinforced beam. | | | | | | [12] | C504.1 | L1 |
| 2 (a) | A rectangular RCC beam 300 mm wide and 500 mm deep is reinforced with 4 bars of 16 mm dia. It is freely supported on an effective span of 6 m. Determine the max permissible imposed service load. Assuming M 20 grade concrete & Fe-500 steel. | | | | | | [12] | C504.2 | L2 |
| | | | | | | | | C504.2 | L1 |

| | | | | |
|-------|--------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|------|--------|----|
| 3 (a) | Find the moment of resistance of a doubly reinforced rectangular section 230 mm wide and 450 mm effective depth with 2 bars of 20 mm diameter are placed in compression side with an effective cover of 40 mm. Tension steel consists of 3 bars of 25 mm diameter with an effective cover of 40 mm. Assume M 20 grade concrete and Fe-415 steel. | [07] | C504.2 | L2 |
| (b) | Determine the moment of resistance of T beam $b_f = 1000$ mm, $D_f = 100$ mm, $b_w = 300$ mm, effective cover = 50 mm, $d = 450$ mm, $A_{st} = 1963\text{mm}^2$. Use M 20 and Fe-415 grade steel. | [08] | C504.2 | L2 |

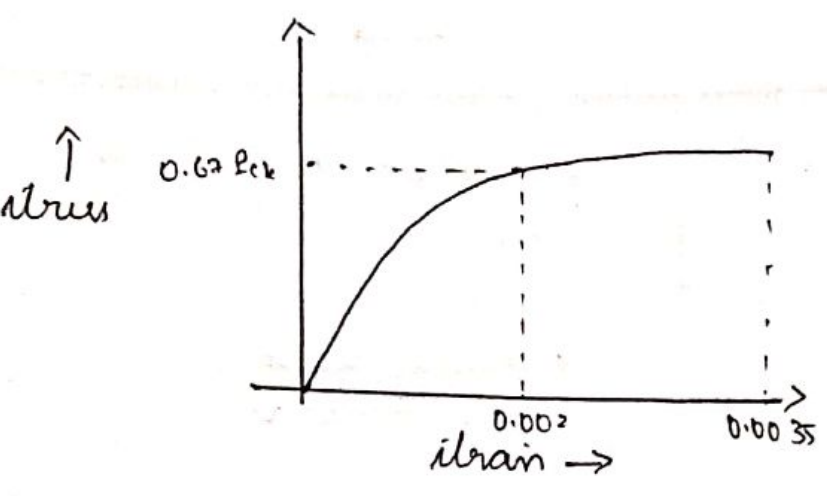
IAT-1

1) a)

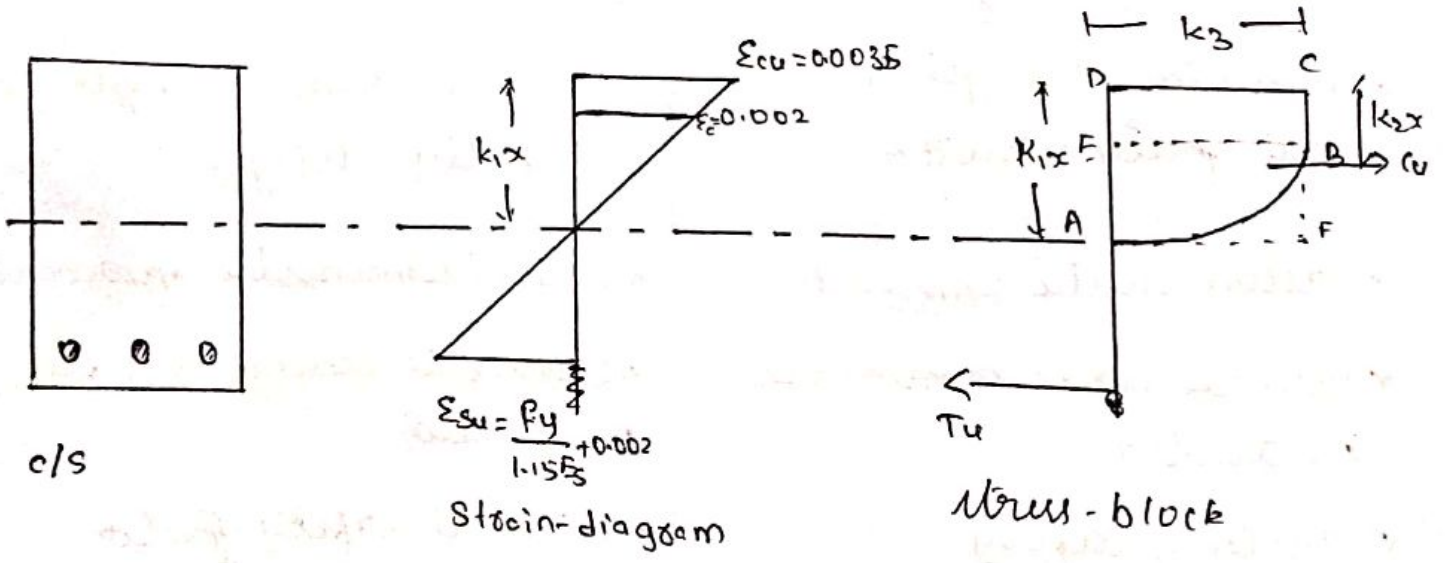
| Working stress method | Limit state method |
|--------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|
| <ul style="list-style-type: none"> * Based on linear elastic theory * thicker sections, uneconomical * No check on serviceability * Material strength is not fully utilized * deterministic approach * ultimate loads cannot be reduced * Factor of safety - permissible stresses | <ul style="list-style-type: none"> * based on actual stress-strain curves * thinner section, economical * check on serviceability * Material strength is fully utilized * non deterministic approach * ultimate loads can be reduced * partial safety factors |

b) Stress-block parameter

The stress-strain relationship for a concrete cube is uniform, but it varies with depth under bending



C/S & S/S



- At ϵ_{cu} = ultimate strain in concrete = 0.0035
- ϵ_c = strain in concrete at yielding = 0.002
- ϵ_{su} = ultimate strain in steel = $\frac{f_y}{1.15 E_s} + 0.002$

- k_1 = shape factor
- k_2 = depth factor
- k_3 = stress factor

$$k_1 = \text{shape factor} = \frac{\text{area of the stress block } ABCDA}{\text{area of rectangle } AFCD}$$

$$\text{NOW, } \frac{\Sigma c_u}{\epsilon_c} = \frac{0.0035}{0.002} = \frac{AD}{AE}$$

$$\frac{AE}{AD} = \frac{0.002}{0.0035}$$

$$AE = \frac{4}{7} AD$$

$$\frac{DE}{AD} = \frac{0.0015}{0.0035}$$

$$DE = \frac{3}{7} AD$$

NOW,

$$k_1 = \frac{DC \times DE + \frac{2}{3} \times AE \times BE}{AD \times DC}$$

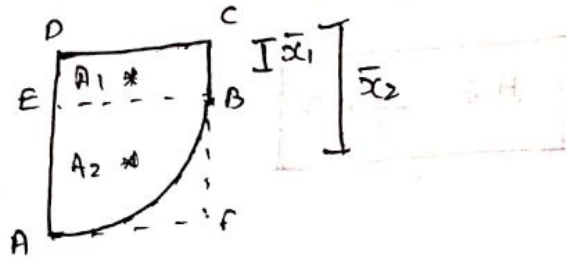
$$= \frac{DC \times \frac{3}{7} \times AD + \frac{2}{3} \times \frac{4}{7} \times AD \times DC}{AD \times DC}$$

$$= \frac{AD \times DC \left(\frac{3}{7} + \frac{2 \times 4}{3 \times 7} \right)}{AD \times DC}$$

$$K_{2x} = \text{depth factor} = \frac{A_1 \cdot \bar{x}_1 + A_2 \cdot \bar{x}_2}{A_1 + A_2}$$

A_1 → area of rect. part, \bar{x}_1 → distance of centroid of rectangular part of stress block from top

A_2 → area of parabolic part of the stress block, \bar{x}_2 → its centroid from top



$$\bar{x}_1 = \frac{DE}{2}$$

$$= \frac{3}{7} \times AD \times \frac{1}{2}$$

$$\boxed{\bar{x}_1 = \frac{3}{14} \times AD}$$

$$\bar{x}_2 = DE + \frac{3}{8} \times AE$$

$$= \frac{3}{7} \times AD + \frac{3}{8} \times \frac{4}{7} \times AD$$

$$\boxed{\bar{x}_2 = \frac{9}{14} \times AD}$$

$$K_{2y} \quad A_1 = DE \times DC$$

$$\boxed{A_1 = \frac{3}{7} \times AD \times DC}$$

$$A_2 = \frac{2}{3} \times AE \times BE$$

$$= \frac{2}{3} \times \frac{4}{7} \times AD \times DC$$

$$\boxed{A_2 = \frac{8}{21} \times AD \times DC}$$

$$\therefore K_{2x} = \frac{\frac{3}{7} \times AD \times DC \times \frac{3}{14} \times AD + \frac{8}{21} \times AD \times DC \times \frac{9}{14} \times AD}{\frac{3}{7} \times AD \times DC + \frac{8}{21} \times AD \times DC}$$

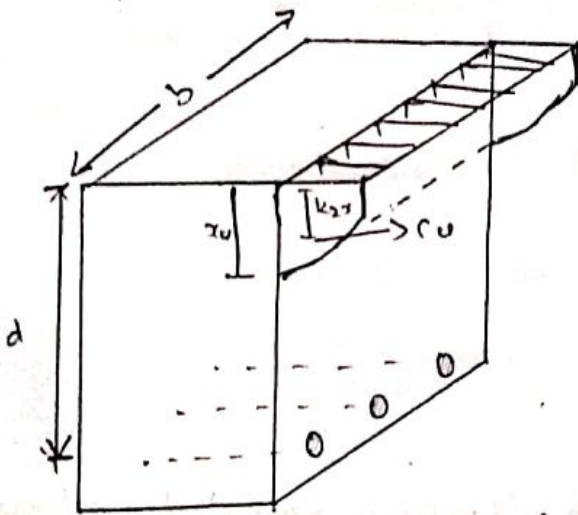
$$\therefore \frac{\left(\frac{3}{7} \times \frac{3}{14}\right) AD + \left(\frac{3}{21} \times \frac{9}{14}\right) AD}{\frac{3}{7} + \frac{8}{21}}$$

$$K_2 \cdot \tau = 0.42 AD$$

but here $AD = \tau$

$$\therefore K_2 = 0.42$$

stress factor



compressive force = compressive strength \times area

$$\text{compressive strength} = \frac{\text{compressive load / force}}{\text{area}}$$

compressive force = ~~σ_c~~ ^{strength} $= 0.67 f_{ck}$

$$\sigma_c = K_3 \cdot f_{ck} \cdot b \cdot x_u$$

$$K_3 = 0.67$$

is the stress factor

d)

a)

$$b = 300 \text{ mm}$$

$$D = 500 \text{ mm}$$

$$A_{st} = 4 \times \frac{\pi}{4} \times 16^2 = 804.25 \text{ mm}^2$$

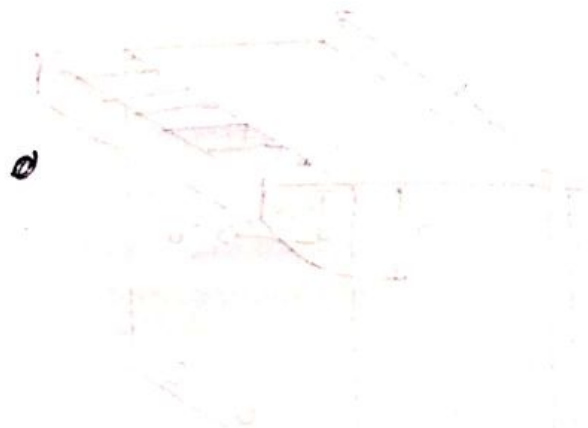
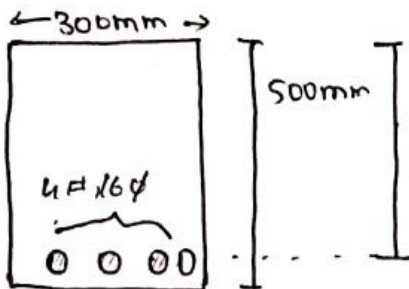
$$l = 6 \text{ m}$$

$$w_L = ?$$

⊕

$$f_{cb} = 20 \text{ N/mm}^2$$

$$f_y = 500 \text{ N/mm}^2$$



effective depth, $d = \text{overall depth} - (\text{clear cover} + \frac{1}{2} \text{ dia of bars})$

$$d = 500 - (25 + \frac{16}{2})$$

$$d = 467 \text{ mm}$$

Step 1: calculate depth of N.A

$$\frac{x_u}{d} = \frac{0.87 \cdot f_y \cdot A_{st}}{0.36 \cdot f_{cb} \cdot b \cdot d}$$

$$\frac{x_u}{d} = \frac{0.87 \cdot 500 \cdot 804.25}{0.36 \cdot 20 \cdot 300 \cdot 467}$$

#96, h1.1, IS 456-2000

$$\frac{x_u}{d} = 0.35$$

Step 2: Compare $\frac{x_u}{d}$ and $\frac{x_{u,max}}{d}$

$$\frac{x_{u,max}}{d} = 0.46 \quad \text{for Fe 500 grade steel}$$

IS 456-2000

$$0.35 < 0.46$$

$$\frac{x_u}{d} < \frac{x_{u,max}}{d}$$

\therefore the section is under-reinforced

Step 3: To calculate moment of resistance

$$M_u = 0.87 \times f_y \times A_{st} \times d \left(1 - \frac{A_{st} \times f_y}{b \cdot d \cdot f_{ck}} \right)$$

$$= 0.87 \times 500 \times 804.25 \times 467 \left(1 - \frac{804.25 \times 500}{300 \times 467 \times 20} \right)$$

$$M_u = 139.93 \text{ kN-m}$$

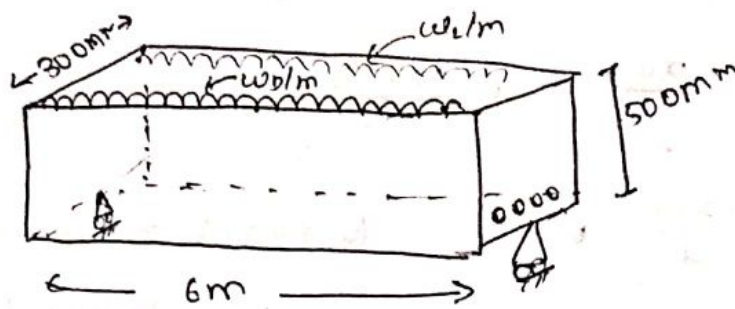
Step 4: To calculate working moment of resistance

$$M_{u,working} = \frac{M_u}{D.S.F}$$

$$= \frac{139.93}{1.5}$$

$$M_{u,working} = 93.29 \text{ kN-m}$$

Step 5: Moment due to dead load



$$\frac{w_L}{2} \times \frac{l}{2} = \frac{w_L l^2}{8}$$

$$\frac{w_L l^2}{8} = \frac{w_L l^2}{8}$$

$$\frac{w_L l^2}{8} = \frac{w_L l^2}{8}$$

dead load = density of concrete * cross sectional area

$$= 25 \text{ kN/m}^3 * 0.3 * 0.5$$

$$= 3.75 \text{ kN/m}$$

moment due to dead load

$$M_D = \frac{w_L l^2}{8} = \frac{3.75 * 6^2}{8} = 16.88 \text{ kN-m}$$

Step 6: To find the imposed service load

$$M_{u, \text{work}} = M_L + M_D$$

$$93.29 = \frac{w_L * l^2}{8} + 16.88$$

$$w_L = \frac{(93.29 - 16.88) * 8}{6^2}$$

$$w_L = 16.98 \text{ kN/m}$$

3)

o) $b = 230 \text{ mm}$

$d = 450 \text{ mm}$

$A_{sc} = 2 \times \frac{\pi}{4} \times 20^2 = 628.32 \text{ mm}^2$

$d'' = 40 \text{ mm}$

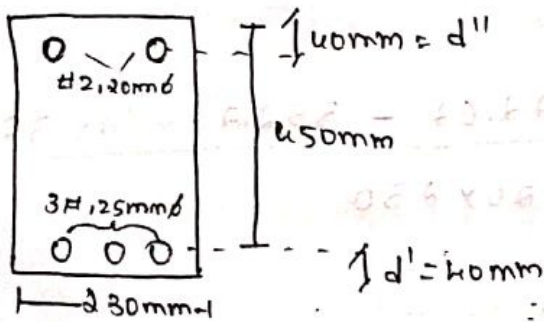
$A_{st} = 3 \times \frac{\pi}{4} \times 25^2 = 1472.62 \text{ mm}^2$

$d' = 40 \text{ mm}$

$f_{ck} = 20 \text{ N/mm}^2$

$f_y = 415 \text{ N/mm}^2$

$M_u = ?$



Step 1: Find $x_{u,max}$

$\frac{x_{u,max}}{d} = 0.48$ for Fe 415 steel, #70 IS 456-2000

$x_{u,max} = 0.48 \times 450$

$x_{u,max} = 216 \text{ mm}$

Step 2: Calculate f_{sc}

f_{sc} value corresponding to a strain of $0.0035 \left(\frac{x_{u,max} - d''}{x_{u,max}} \right)$

$$= 0.0035 \left(\frac{216 - 40}{216} \right)$$

$$= 0.0028$$

∴ from graph #23 A, page 70 IS 456-2000

$$f_{sc} \text{ value} = 0.85 f_y$$

$$f_{sc} = 0.85 * 415$$

$$f_{sc} = 352.75 \text{ N/mm}^2$$

Step 3: to find depth of N.A

$$x_u = \frac{0.87 f_y A_{st} - f_{sc} A_{sc}}{0.36 f_{cb} b}$$

$$= \frac{0.87 * 415 * 1472.62 - 352.75 * 628.32}{0.36 * 20 * 230}$$

$$x_u = 187.23 \text{ mm}$$

Step 4: Recalculate f_{sc}

f_{sc} value corresponding to a strain of $0.0035 \left(\frac{x_u - d''}{x_u} \right)$

$$= 0.0035 \left(\frac{187.23 - 40}{187.23} \right)$$

$$\approx 0.0027$$

from graph 23, A, #70 IS 456-2000

$$f_{sc} = 0.85 f_y$$

Step 5: Compare x_u & $x_{u,max}$

$$187.23 < 216 \text{ mm}$$

$$x_u < x_{u,max}$$

\therefore the column is under-reinforced

Step 6: To find M_u .

$$M_u = M_{u,lim} + f_{sc} \cdot A_{sc} (d - d'')$$

$$M_{u,lim} = 0.36 \cdot \frac{x_u}{d} \left(1 - 0.42 \frac{x_u}{d} \right) \cdot b \cdot d^2 \cdot f_{cb}$$

$$= 0.36 \times \frac{187.23}{450} \left(1 - 0.42 \times \frac{187.23}{450} \right) \times 230 \times 450^2 \times 20$$

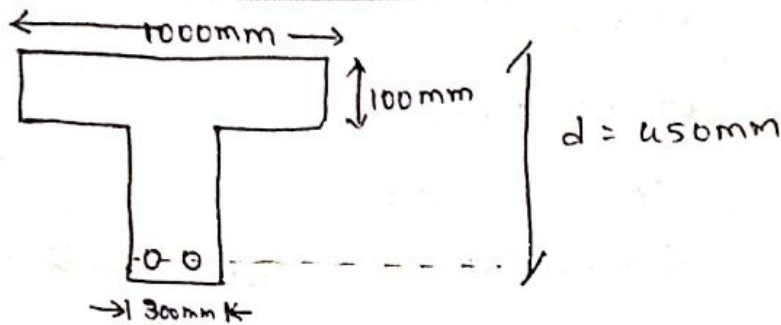
$$= 115.14 \text{ kN-m}$$

$$M_u = M_{u,lim} + f_{sc} \cdot A_{sc} (d - d'')$$

$$= 115.14 \times 10^6 + 352.75 \times 628.32 (450 - 40)$$

$$M_u = 206.01 \text{ kN-m}$$

(b)



given:

$$b_f = 1000\text{mm}$$

$$D_f = 100\text{mm}$$

$$b_w = 300\text{mm}$$

$$d' = 50\text{mm}$$

$$d = 450\text{mm}$$

$$A_{st} = 1963\text{mm}^2$$

$$f_{cb} = 20\text{N/mm}^2$$

$$f_y = 415\text{N/mm}^2$$

Step 1: Find x_u

$$x_u = \frac{0.87 f_y \cdot A_{st}}{0.36 f_{cb} \cdot b_f}$$
$$= \frac{0.87 \times 415 \times 1963}{0.36 \times 20 \times 1000}$$

$$x_u = 98.4\text{mm}$$

Step 2: Compare x_u and D_f

$$98.4\text{mm} < 100\text{mm}$$

$$x_u < D_f$$

∴ Analyse the T-beam as a rectangular beam

Step 3: calculate $x_{u,max}$

$$\frac{x_{u,max}}{d} = 0.48 \quad \text{for } F_{cu} = 45$$

$$x_{u,max} = 0.48 \times 450$$

$$x_{u,max} = 216 \text{ mm}$$

$$x_u < x_{u,max}$$

∴ the section is under reinforced

Step 4: To find ultimate moment of resistance

$$M_u = 0.87 \times f_y \times A_{st} \times d \left(1 - \frac{A_{st} \times f_y}{b \times d \times f_{ck}} \right)$$

$$= 0.87 \times 415 \times 1963 \times 450 \left(1 - \frac{1963 \times 415}{1000 \times 450 \times 20} \right)$$

$$M_u = 290.06 \text{ kNm}$$