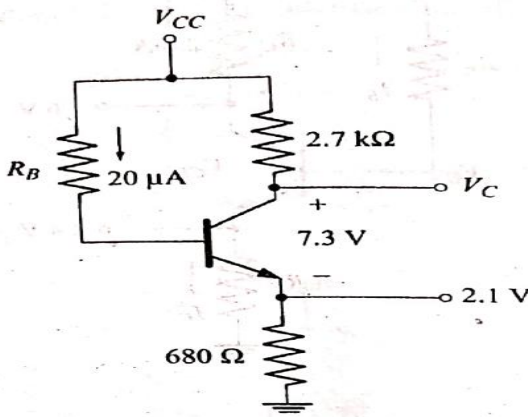
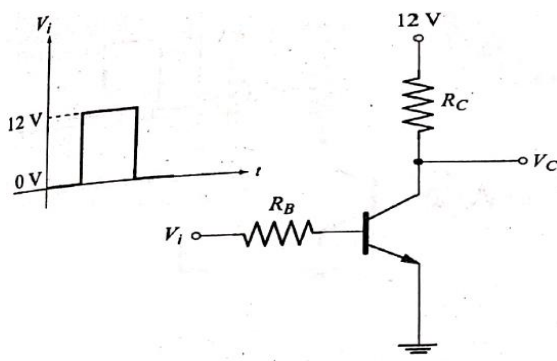
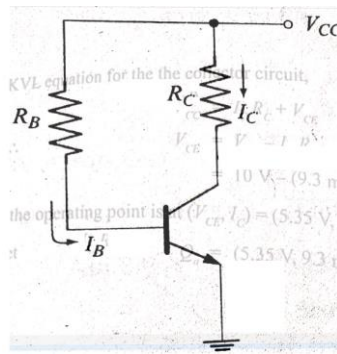


Internal Assessment Test - I

Sub:	ANALOG ELECTRONIC CIRCUITS	Code:	18EE34						
Date:	09/09/2019	Duration:	90 mins	Max Marks:	50	Sem:	3rd	Branch:	EEE
Answer <b>Any FIVE FULL</b> Questions									
		Marks	OBE						
			CO	RBT					
1	<p>For the fixed-bias circuit, <math>R_B=50K\Omega</math>, <math>R_C=500\Omega</math>, <math>V_{CC} = 10V</math>.</p> <p>a) Draw the neat circuit diagram.</p> <p>b) Find the coordinates of the operating point.</p> <p>c) Draw the dc load line and locate the operating point on the dc load line.</p> <p>Assume silicon transistor with <math>\beta = 50</math> and <math>V_{BE} = 0.7V</math>.</p>	10	CO1	L3					
2	<p>The circuit shown below uses silicon transistor. Calculate</p> <p>a) <math>\beta</math> (b) <math>V_{CC}</math> (c) <math>R_B</math> (d) <math>V_C</math> (e) <math>I_{C(sat)}</math></p> 	10	CO1	L3					
3	Derive the expression for stability factor $S(I_{CO})$ and $S(V_{BE})$ for Emitter Bias configuration.	10	CO1	L3					
4	<p>Determine the stability factor <math>S(V_{BE})</math> and the change in <math>I_C</math> from <math>25^{\circ}C</math> to <math>100^{\circ}C</math> for the transistor with <math>V_{BE}(25^{\circ}C) = 0.65V</math> and <math>V_{BE}(100^{\circ}C) = 0.48V</math> for the following bias arrangements.</p> <p>a) Fixed bias with <math>R_B = 270k\Omega</math> and <math>\beta = 120</math></p> <p>b) Voltage divider bias with <math>R_1 = 39k\Omega</math>, <math>R_2 = 10k\Omega</math>, <math>R_E = 1k\Omega</math> and <math>\beta = 120</math></p>	10	CO1	L3					
5	Derive the expression for stability factor $S(I_{CO})$ and $S(V_{BE})$ for fixed Bias configuration	10	CO1	L3					
6	<p>For the transistor inverter shown, determine the values of <math>R_B</math> and <math>R_C</math>. Take <math>I_{C(sat)} = 12mA</math>, <math>\beta = 200</math> and <math>V_{CE(sat)} = 0V</math>. Also draw the output voltage Waveform.</p> 	10	CO1	L3					
7	What is Clamping circuits? Draw the circuit and output waveforms for negative clamper and positive clamper.	10	CO1	L1					

## Analog Electronic Circuits – IAT 1 solution

1.  
a) Circuit diagram:



- b)

$$I_B = \frac{V_{CC} - V_{BE}}{R_B} = \frac{10 \text{ V} - 0.7 \text{ V}}{50 \text{ k}\Omega} = 0.186 \text{ mA}$$

$$I_C = \beta I_B = 50 \times 0.186 \text{ mA} = 9.3 \text{ mA}$$

Writing KVL equation for the collector circuit,

$$V_{CC} = I_C R_C + V_{CE}$$

$$\therefore V_{CE} = V_{CC} - I_C R_C$$

$$= 10 \text{ V} - (9.3 \text{ mA} \times 0.5 \text{ k}\Omega) = 5.35 \text{ V}$$

Therefore the operating point is at  $(V_{CE}, I_C) = (5.35 \text{ V}, 9.3 \text{ mA})$

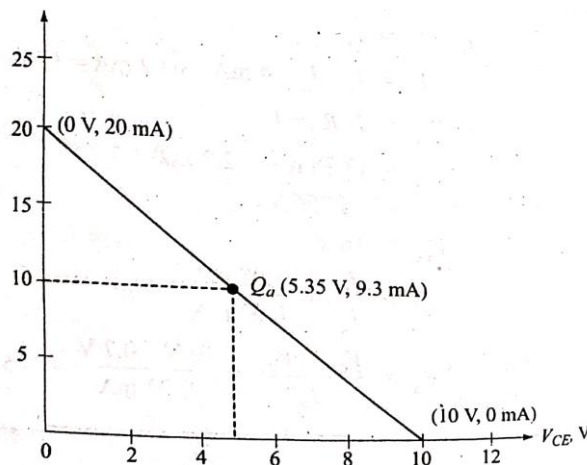
Let  $Q_a = (5.35 \text{ V}, 9.3 \text{ mA})$

The current axis intercept of the load line is

$$\frac{V_{CC}}{R_C} = \frac{10 \text{ V}}{0.5 \text{ k}\Omega} = 20 \text{ mA}$$

and the voltage axis intercept is  $V_{CC} = 10 \text{ V}$ . The load line is plotted by joining  $(0 \text{ V}, 20 \text{ mA})$  and  $(10 \text{ V}, 0 \text{ mA})$  as shown below:

- c)



- 2.

(a)  $\beta$

Given the voltage across the emitter resistance, we can obtain the emitter current as

$$I_E = \frac{V_E}{R_E} = \frac{2.1 \text{ V}}{680 \Omega} = 3.09 \text{ mA}$$

The emitter current is approximately equal to collector current.

$$\therefore I_C = 3.09 \text{ mA}$$

$$\text{Now } \beta = \frac{I_C}{I_B} = \frac{3.09 \text{ mA}}{20 \mu\text{A}} = 154.5$$

(b)  $V_{CC}$

From the KVL equation for the collector-emitter circuit, we have

$$\begin{aligned} V_{CC} &= I_C R_C + V_{CE} + V_E \\ &= (3.09 \text{ mA} \times 2.7 \text{ k}\Omega) + 7.3 \text{ V} + 2.1 \text{ V} = 17.74 \text{ V} \end{aligned}$$

(c)  $R_B$

Writing the KVL equation for the base-emitter circuit

$$V_{CC} = I_B R_B + V_{BE} + V_E$$

$$\begin{aligned} R_B &= \frac{V_{CC} - V_{BE} - V_E}{I_B} \\ &= \frac{17.74 \text{ V} - 0.7 \text{ V} - 2.1 \text{ V}}{20 \mu\text{A}} = 747 \text{ k}\Omega \end{aligned}$$

d)

$$V_C = V_{CE} + V_E = 7.3 \text{ V} + 2.1 \text{ V} = 9.4 \text{ V}$$

e)

$$I_{C(\text{sat})} = \frac{V_{CC}}{R_C + R_E} = \frac{17.74 \text{ V}}{2.7 \text{ k}\Omega + 680 \Omega} = 5.248 \text{ mA}$$

3. Stability factor  $S(I_{CO})$

$$S(I_{CO}) = \frac{1 + \beta}{1 - \beta \frac{\partial I_B}{\partial I_C}}$$

$$V_{CC} = I_B R_B + V_{BE} + I_E R_E$$

But

$$I_E = I_B + I_C$$

$\therefore$

$$V_{CC} = I_B R_B + V_{BE} + I_B R_E + I_C R_E$$

Differentiating

$$0 = \frac{\partial I_B}{\partial I_C} R_B + \frac{\partial I_B}{\partial I_C} R_E + R_E = \frac{\partial I_B}{\partial I_C} (R_B + R_E) + R_E$$

$\therefore$

$$\frac{\partial I_B}{\partial I_C} = -\frac{R_E}{R_B + R_E}$$

$$\begin{aligned}
 S(I_{CO}) &= \frac{1+\beta}{1-\beta\left(\frac{-R_E}{R_B+R_E}\right)} = \frac{1+\beta}{1+\beta\left(\frac{R_E}{R_B+R_E}\right)} \\
 &= \frac{(\beta+1)(R_E+R_B)}{R_B+R_E+\beta R_E} = \frac{(\beta+1)(R_E+R_B)}{(\beta+1)R_E+R_B} \\
 S(I_{CO}) &= \frac{(\beta+1)\left(1+\frac{R_B}{R_E}\right)}{(\beta+1)+\frac{R_B}{R_E}}
 \end{aligned}$$

Stability factor  $S(V_{BE})$

$$S(V_{BE}) = \frac{\partial I_C}{\partial V_{BE}}$$

$$V_{CC} = I_B R_B + V_{BE} + I_B R_E + I_C R_E$$

$$V_{CC} = \frac{I_C}{\beta} R_B + V_{BE} + \frac{I_C}{\beta} R_E + I_C R_E$$

$$= \left[ \frac{R_B}{\beta} + \frac{R_E}{\beta} + R_E \right] I_C + V_{BE}$$

$$= \left[ \frac{R_B + R_E + \beta R_E}{\beta} \right] I_C + V_{BE}$$

$$V_{CC} = \left[ \frac{R_B + (1+\beta)R_E}{\beta} \right] I_C + V_{BE}$$

$$0 = \frac{R_B + (1+\beta)R_E}{\beta} + \frac{\partial V_{BE}}{\partial I_C}$$

$$S(V_{BE}) = \frac{\partial I_C}{\partial V_{BE}} = \frac{-\beta}{R_B + (1+\beta)R_E}$$

4.

$$\begin{aligned}
 \Delta V_{BE} &= V_{BE}(100^\circ \text{C}) - V_{BE}(25^\circ \text{C}) \\
 &= 0.48 \text{ V} - 0.65 \text{ V} = -0.17 \text{ V}
 \end{aligned}$$

a)

Fixed Bias  
 $R_B = 270 \text{ k}\Omega$   $\beta = 120$

$$S(V_{BE}) = \frac{-\beta}{R_B} = -\frac{120}{270 \text{ k}\Omega} = -0.44 \times 10^{-3}$$

$$\begin{aligned} \Delta I_C &= S(V_{BE}) \Delta V_{BE} \\ &= (-0.44 \times 10^{-3}) (-0.17) = 74.8 \mu\text{A} \end{aligned}$$

b)

**Voltage Divider Bias**

$R_1 = 39 \text{ k}\Omega$   $R_2 = 10 \text{ k}\Omega$   $R_E = 1 \text{ k}\Omega$   $\beta = 120$

$$S(V_{BE}) = \frac{-\beta}{R_{Th} + (1+\beta)R_E}$$

$$R_{Th} = R_1 \parallel R_2 = 39 \text{ k}\Omega \parallel 10 \text{ k}\Omega = 7.95 \text{ k}\Omega$$

$$S(V_{BE}) = \frac{-120}{7.95 \text{ k}\Omega + (121)(1 \text{ k}\Omega)} = -0.93 \times 10^{-3}$$

$$\Delta I_C = S(V_{BE}) \Delta V_{BE} = (-0.93 \times 10^{-3}) (-0.17) = 158.1 \mu\text{A}$$

5. Stability factor  $S(I_{CO})$

$$S(I_{CO}) \equiv \frac{\partial I_C}{\partial I_{CO}}$$

$$I_B = \frac{V_{CC} - V_{BE}}{R_B}$$

But

$$V_{CC} \gg V_{BE}$$

$$\therefore I_B \approx \frac{V_{CC}}{R_B} \text{ which is constant}$$

Differentiating with respect to  $I_C$ ,

$$\frac{\partial I_B}{\partial I_C} = 0$$

$$S(I_{CO}) = 1 + \beta$$

Stability factor  $S(V_{BE})$

$$S(V_{BE}) \equiv \frac{\partial I_C}{\partial V_{BE}}$$

$$V_{CC} = I_B R_B + V_{BE}$$

$$V_{BE} = V_{CC} - I_B R_B$$

$$I_B \approx \frac{I_C}{\beta}$$

$$V_{BE} = V_{CC} - \frac{I_C}{\beta} R_B$$

$$1 = 0 - \frac{R_B}{\beta} \frac{\partial I_C}{\partial V_{BE}}$$

$$S(V_{BE}) = -\frac{\beta}{R_B}$$

6.

Calculation of  $R_C$

$$I_{C(sat)} = \frac{V_{CC} - V_{CE(sat)}}{R_C}$$

From the output waveform,  $V_{CE(sat)} = 0 \text{ V}$

$$\therefore R_C = \frac{V_{CC}}{I_{C(sat)}} = \frac{12 \text{ V}}{12 \text{ mA}} = 1 \text{ k}\Omega$$

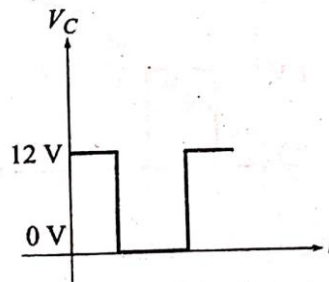
Calculation of  $R_B$

$$I_{B(max)} = \frac{I_{C(sat)}}{\beta_{dc}} = \frac{12 \text{ mA}}{200} = 60 \mu\text{A}$$

Let  $I_B = 150\% \text{ of } I_{B(max)}$  [To ensure saturation]  
 $= (1.5)(60 \mu\text{A}) = 90 \mu\text{A}$

$$R_B = \frac{V_i - V_{BE}}{I_B} = \frac{12 \text{ V} - 0.7 \text{ V}}{90 \mu\text{A}} = 125.55 \text{ k}\Omega$$

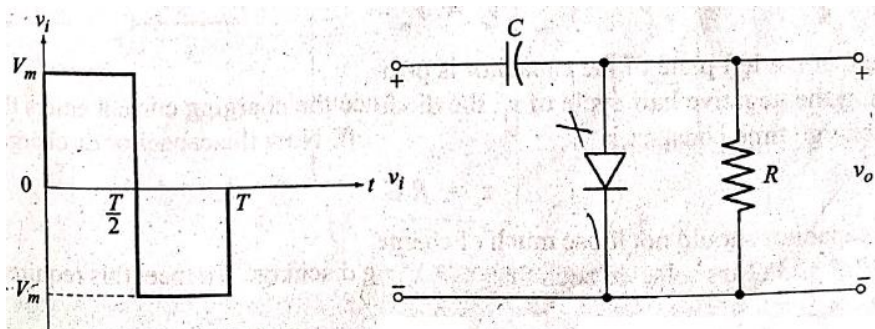
Output voltage waveform

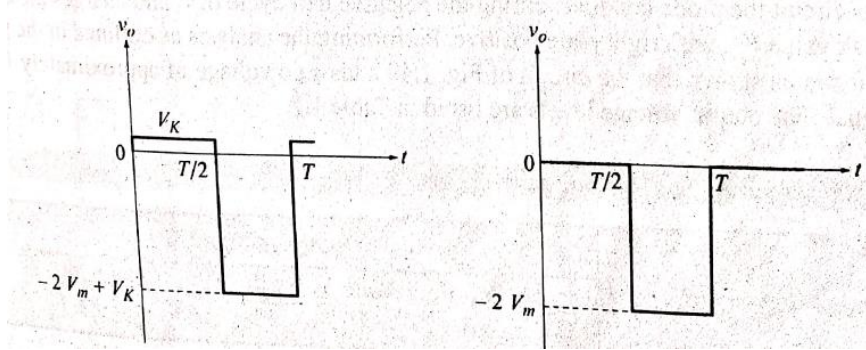


7.

Clamping circuits are used to add dc level to the input signal. They are also called dc restorers or dc inserters. It uses diode, resistors and capacitors.

Negative clamper





Positive clamper

