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a)

$$RL = 2 \times 10^3 \Omega$$

$$E_{\text{source}} = 200 \text{ V}$$

$$I_{dc} = ?$$

$$V_{dc} = ?$$

$$\gamma = ?$$

$$F = ?$$

$$E_{\text{sm}} = 200 \times \sqrt{2} = 282.84 \text{ V}$$

$$I_{dc} = \frac{2 I_m}{\pi}$$

$$I_m = \frac{E_{\text{sm}}}{(R_s + R_f + R_L)}$$

$$I_m = \frac{282.84}{2 \times 10^3} = 0.141 \text{ A}$$

$$I_{dc} = \frac{2 \times 0.141}{\pi} = 0.090 \text{ A}$$

$$V_{dc} = I_{dc} \times R_L$$

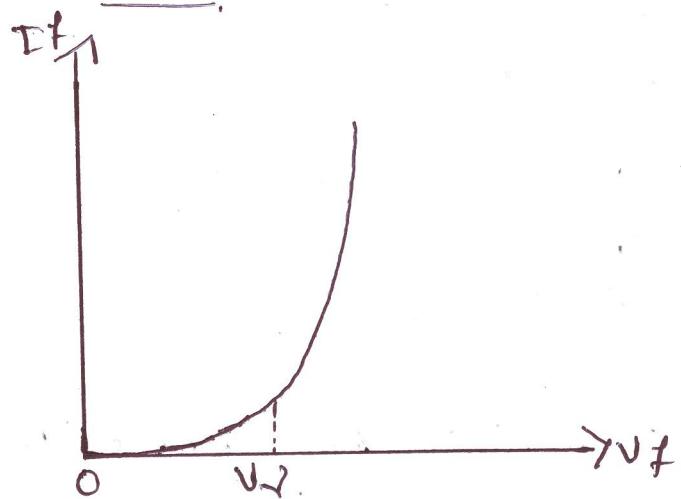
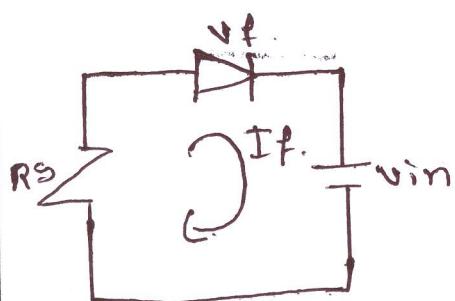
$$V_{dc} = 0.090 \times 2 \times 10^3 \Omega = 180.06 \text{ V}$$

$$\gamma = 0.48$$

b)

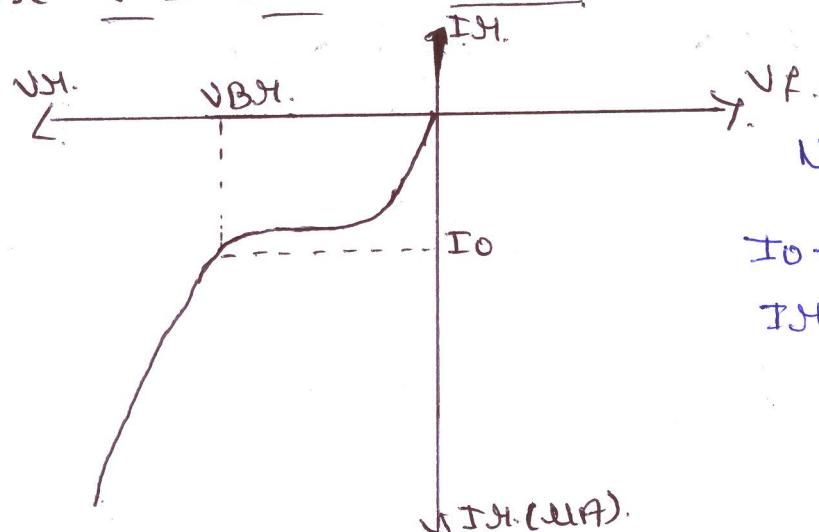
### V-I characteristics.

#### Forward V-I characteristic.



In the region 0- to  $V_K$  (Knee voltage) as the ~~forward~~ supply voltage is less than the barrier potential then there is no movement of majority charge carriers hence forward current is assumed to be nearly zero. above  $V_K$  as a voltage exceed through the barrier potential the diffusion of majority charge carriers. The recombination of arranged and mobile ion reduces due to this the current increases exponentially.

#### Reverse V-I characteristics.

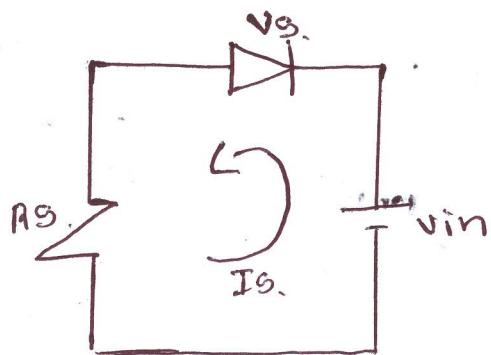


NBR - Break down voltage

$I_0$  - Saturation current

$I_R$  - Reverse current

- \* when the Reverse voltage increases the reverse current also increases due to the presence of majority charge carriers.
- \* Further increasing the reverse voltage the reverse current remains constant due to the absence of minority charge carriers.
- \* Further increasing the reverse voltage the reverse current breaks down the barrier potential it may cause damage to the diode also.



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$$a) \quad I_{Z\min} = 10 \text{ mA}, \quad V_{IMAX} = 12 + 3 = 15 \text{ V}, \quad V_{IN\min} = 12 - 3 = 9 \text{ V}.$$

$$I_L = 20 \text{ mA}, \quad V_Z = 5 \text{ V}, \quad P_{Z\max} = 500 \text{ mW}.$$

$$R_{S\max} = \frac{V_{IN(\min)} - V_Z}{I_L(\max) + I_Z(\min)}$$

$$R_{S(\max)} = \frac{9 - 5}{20 \times 10^{-3} + 10 + 10^{-3}}$$

$$R_{S(\max)} = 133.33 \Omega.$$

$$P_{Z\max} = V_Z(\max) \times I_Z(\max)$$

$$I_Z(\max) = \frac{P_{Z(\max)}}{V_Z(\max)}$$

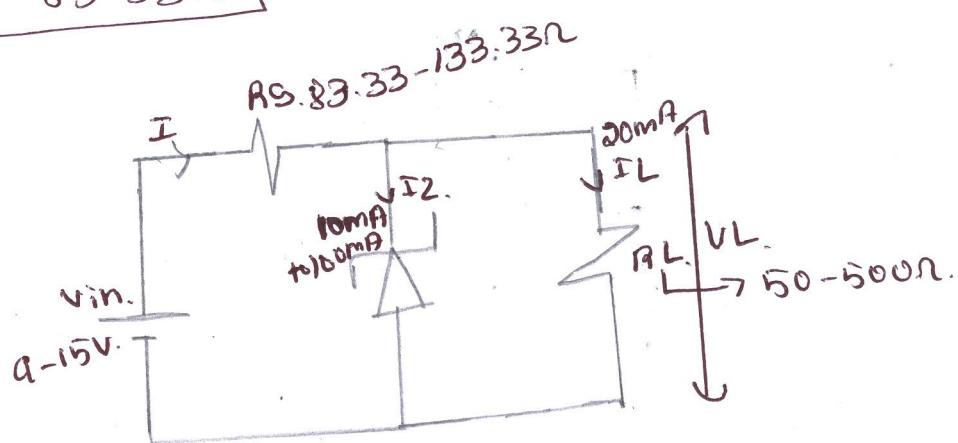
$$I_Z(\max) = \frac{100}{500 \times 10^{-3}} = 200 \text{ mA}$$

$$I_Z(\max) = 100 \text{ mA}$$

$$R_S(\min) = \frac{V_{in(\max)} - V_2}{I_2(\min) + I_2(\max)}$$

$$R_S(\min) = \frac{15 - 5}{20 \times 10^{-3} + 100 \times 10^{-3}}$$

$$R_S(\min) = 83.33\Omega$$



$$V = IR.$$

$$R_L \max = \frac{V_2}{I_{\min}}$$

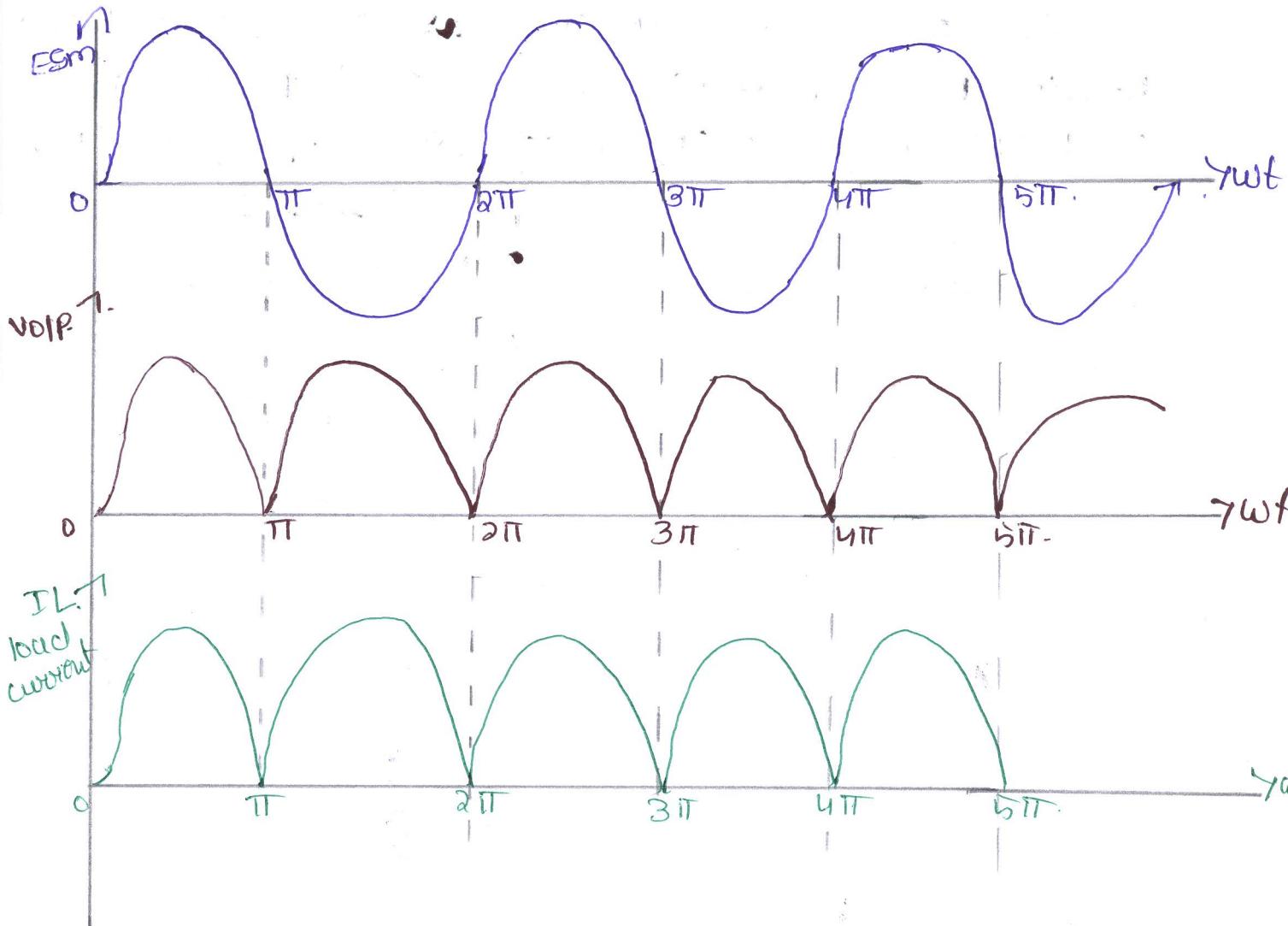
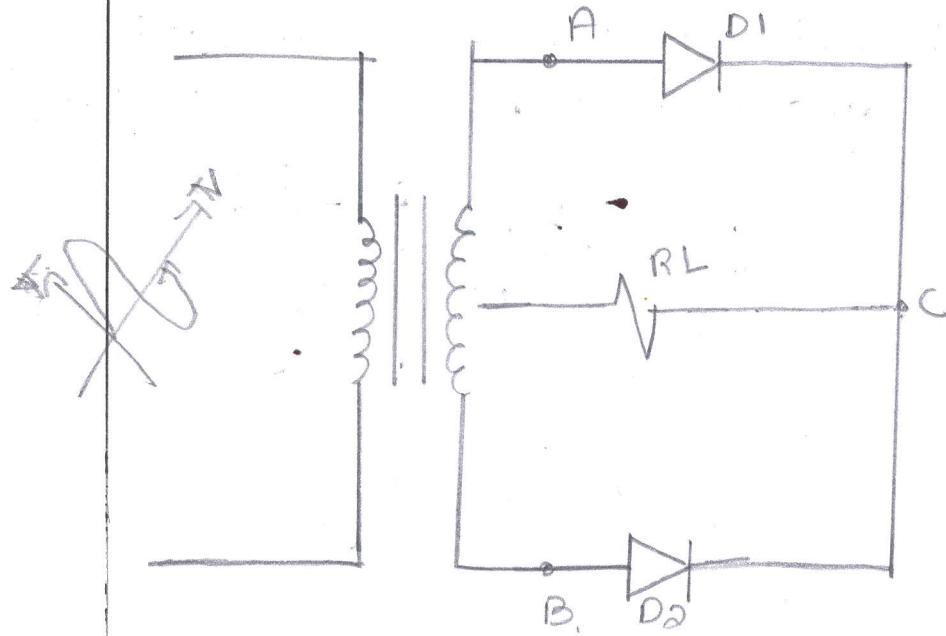
$$= \frac{5}{10 \times 10^{-3}}$$

$$R_L \max = 500\Omega.$$

$$R_L \min = \frac{5}{100 \times 10^{-3}}$$

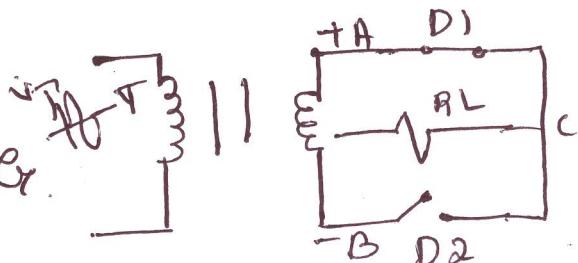
$$R_L \min = 50\Omega.$$

b7.



- \* consider a point A is positive and point B is negative so the circuit acts as a forward bias hence  $D_1$  conducts current and  $D_2$  does not conduct current so.

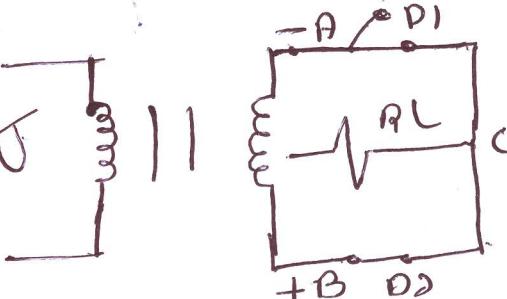
$$A \rightarrow D_1 \rightarrow C \rightarrow RL \rightarrow G$$



so  $D_1$  acts as a closed switch and  $D_2$  acts as a open switch

- \* consider a point A is negative and point B is positive so the circuit acts as a reverse bias hence  $D_2$  conducts current and  $D_1$  does not conduct because ( $D_1$ ) acts as a open switch.

$$B \rightarrow D_2 \rightarrow C \rightarrow RL \rightarrow G$$



$$\beta = \frac{I_C}{I_B} \quad d = \frac{I_C}{I_E}$$

$$\beta = \frac{I_C}{I_B}$$

$$\text{WKT} \quad I_E = I_B + I_C$$

$$\beta = \frac{I_C}{I_E - I_C} \quad \text{by } I_E$$

$$\beta = \frac{\frac{I_C}{I_E}}{1 - \frac{I_C}{I_E}}$$

$$\boxed{\beta = \frac{d}{1-d}}$$

$$d = \frac{I_C}{I_E}$$

$$d = \frac{I_C}{I_B + I_C} \quad \text{by } I_C$$

$$\boxed{d = \frac{\beta}{1+\beta}}$$

$$I_{\text{sums}} = I_{ac} + I_{dc}$$

$$I_{\text{sums}}^2 = (I_{ac} + I_{dc})^2$$

$$I^2_{\text{rms}} = I_{\text{ac}}^2 + I_{\text{dc}}^2 + 2I_{\text{ac}}I_{\text{dc}}.$$

$$I^2_{\text{rms}} = I_{\text{ac}}^2 + I_{\text{dc}}^2.$$

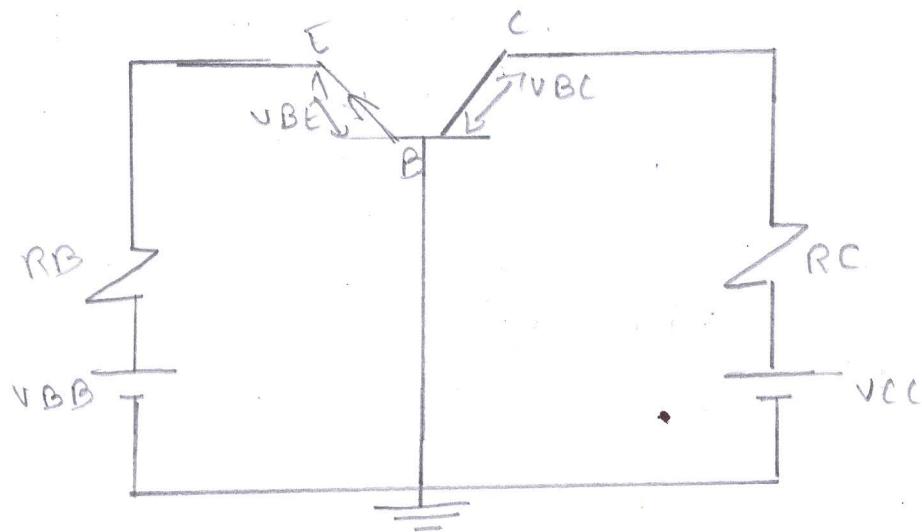
$$I_{\text{ac}}^2 = I^2_{\text{rms}} - I_{\text{dc}}^2.$$

$$\gamma = \sqrt{I^2_{\text{rms}} - I_{\text{dc}}^2}$$

$$\boxed{\gamma = \sqrt{\frac{I^2_{\text{rms}}}{I_{\text{dc}}^2} - 1}}$$

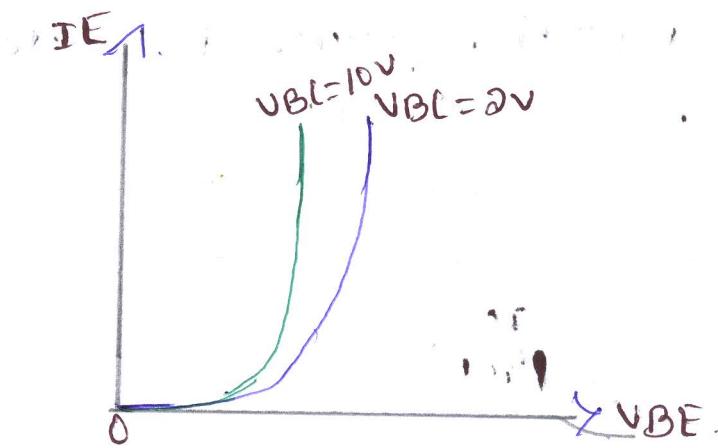
for Half wave = 1.01  
 for full wave = 0.48.

b7.



In CE mode consider an n-p-n transistor working in an active region.

### Input characteristics

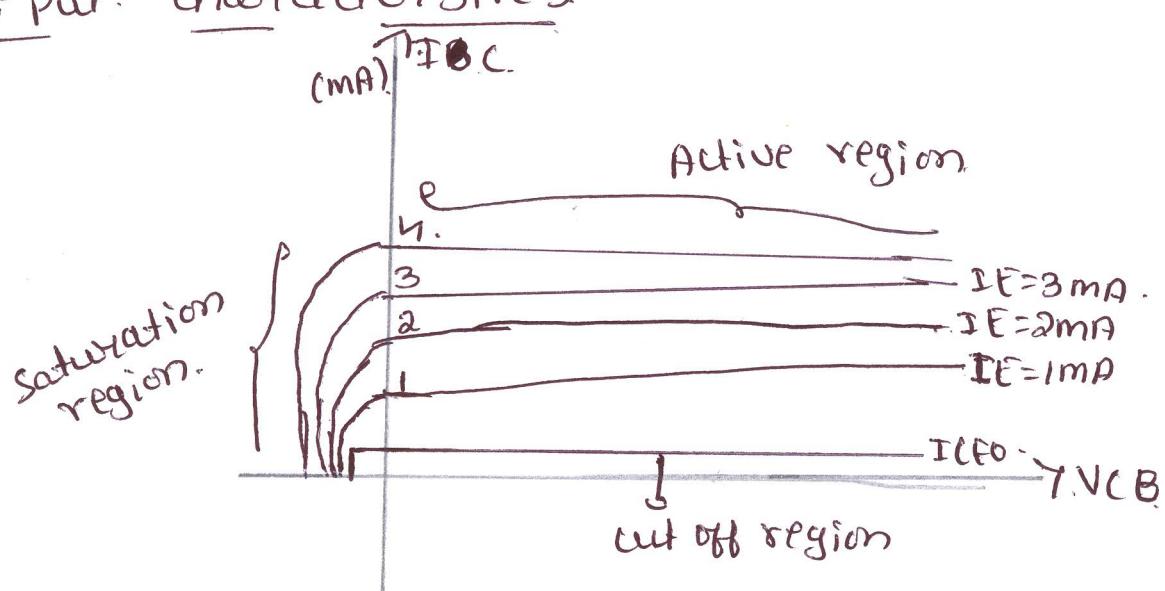


It is a graph of Input current vs Input voltage keeping output voltage as a constant.

### Base width modulation

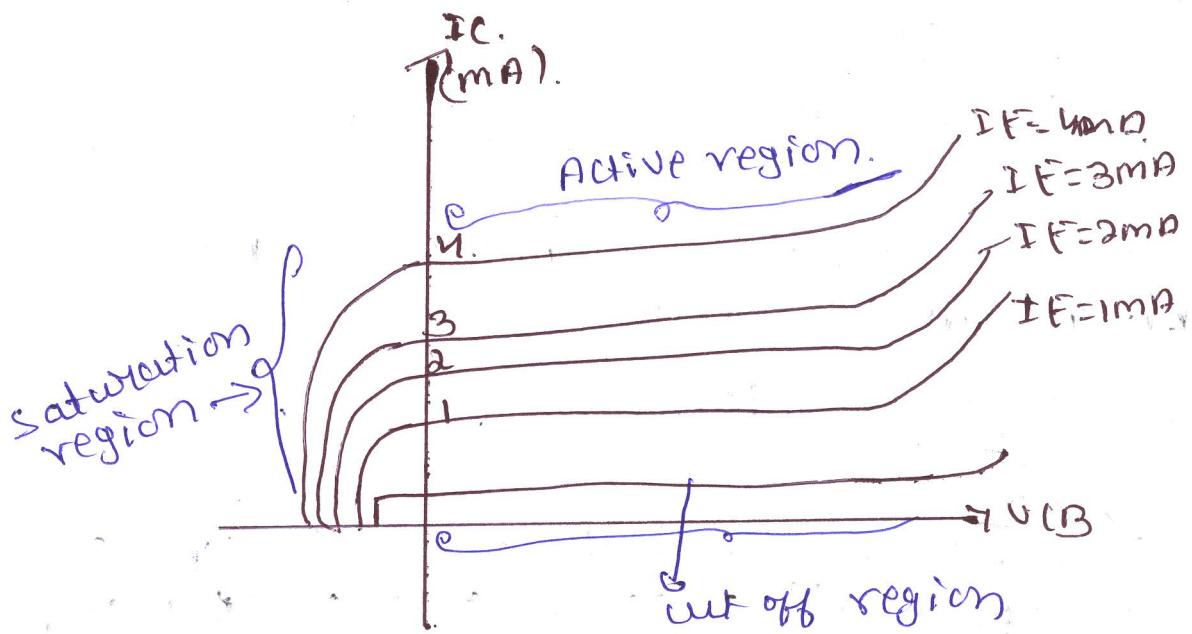
As a depletion region in CB junction increases, the electrical base width decreases. The charge concentration per unit area increases. The Input current  $I_E$  also increases.

### Output characteristics

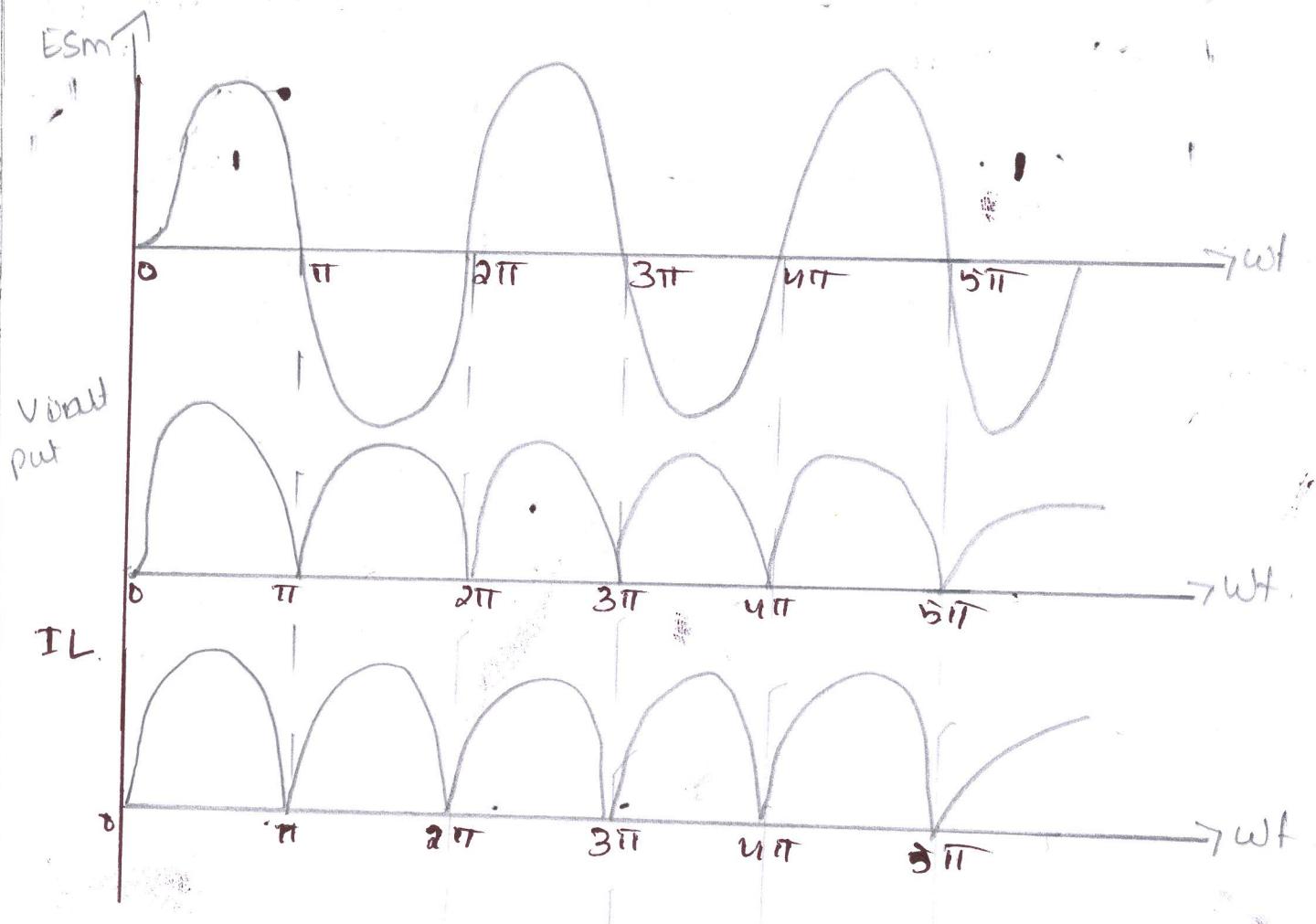
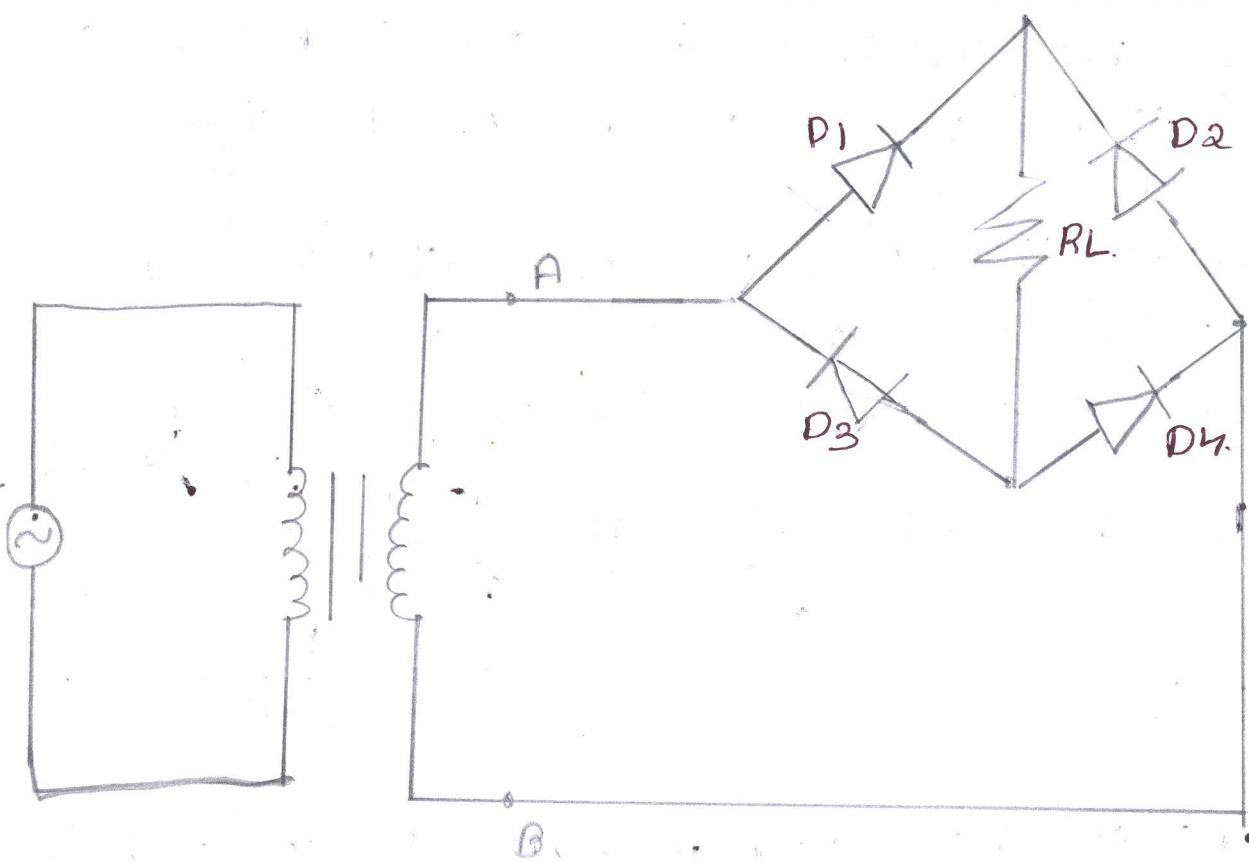


It is a graph of output voltage vs output current  
keeping input current as a constant.  
punch through effect.

When the depletion region increases across the CB junction makes time period and contact with EB junction due to this effect the large current will be produced.



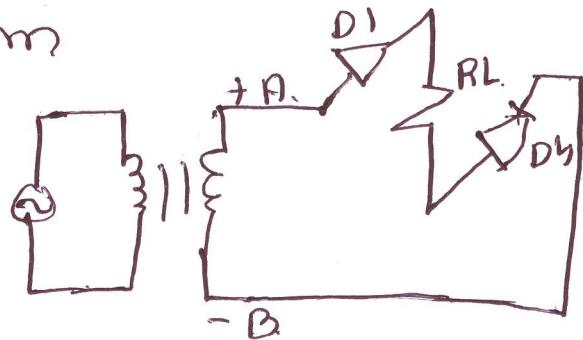
(Q)



In this rectifier there are 4 diodes are  
with their name as D<sub>1</sub>, D<sub>2</sub>, D<sub>3</sub>, D<sub>4</sub>.

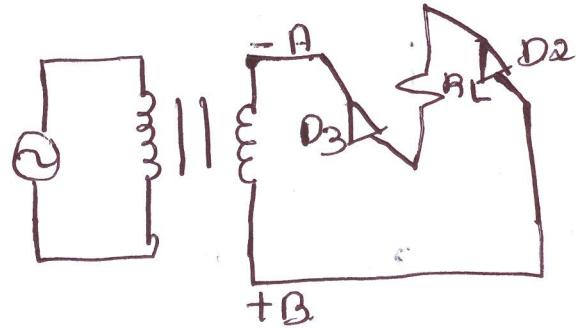
due to the forward bias the node A is positive and node B is negative hence current flows from

$$A \rightarrow D_1 \rightarrow RL \rightarrow D_4 \rightarrow B.$$



due to the reverse bias the node A is -ve and node B is positive hence the current flows from.

$$B \rightarrow D_2 \rightarrow RL \rightarrow D_3 \rightarrow A.$$



$$I_{dc} = \frac{1}{2\pi} \int_0^{2\pi} IL \, dwt.$$

$$\begin{aligned} 0 < wt < \pi & \quad IL = I_m \sin wt \\ \pi < wt < 2\pi & \quad IL = -I_m \sin wt \end{aligned}$$

$$I_{dc} = \frac{1}{2\pi} \int_0^{\pi} I_m \sin wt \, dwt + - \int_{\pi}^{2\pi} I_m \sin wt \, dwt.$$

$$I_{dc} = \frac{Im}{2\pi} - [\cos \pi - \cos 0] + \cancel{\cos \pi} + [\cos 2\pi - \cos 0].$$

$$I_{dc} = \frac{4Im}{2\pi}$$

$$I_{dc} = \frac{2Im}{\pi}$$

$$V_{dc} = I_{dc} \times RL$$

$$V_{dc} = \frac{2Im}{\pi} \times RL$$

$$V_{dc} = \frac{2Im}{\pi} \times RL$$

$$I^2_{sum} = \frac{1}{2\pi} \int_0^{2\pi} I_m^2 \sin^2 wt \, dwt.$$

$$I^2_{sum} = \frac{Im^2}{2\pi} \int_0^{\pi} 1 - \cos 2wt \, dwt + 0.$$

$$I^2_{sum} = \frac{Im^2}{2\pi} [\pi - 0] - \underbrace{[\sin \pi - \sin 0]}_0.$$

$$I_{\text{sums}} = \frac{I_m}{\sqrt{2}}$$

$$P_{dc} = V_{dc} \times I_{dc}$$

$$P_{dc} = \frac{\pi I_m^2}{\pi^2} \times R_L$$

~~$$\eta_{dc} = \frac{P_{dc}}{P_{ac}}$$~~

$$\eta_{dc} = \frac{I_m^2}{2} (R_S + 2\pi f + R_L)$$

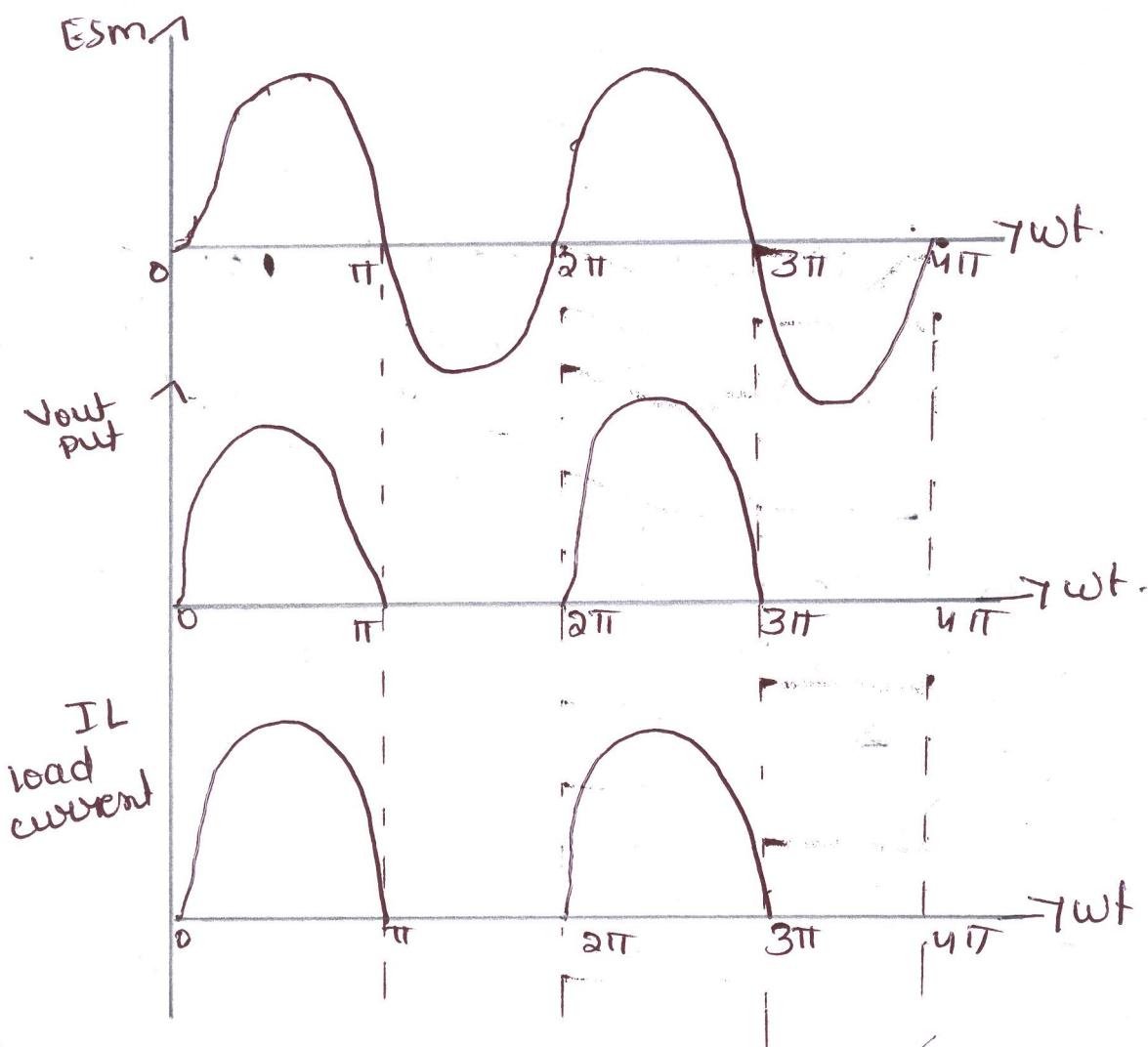
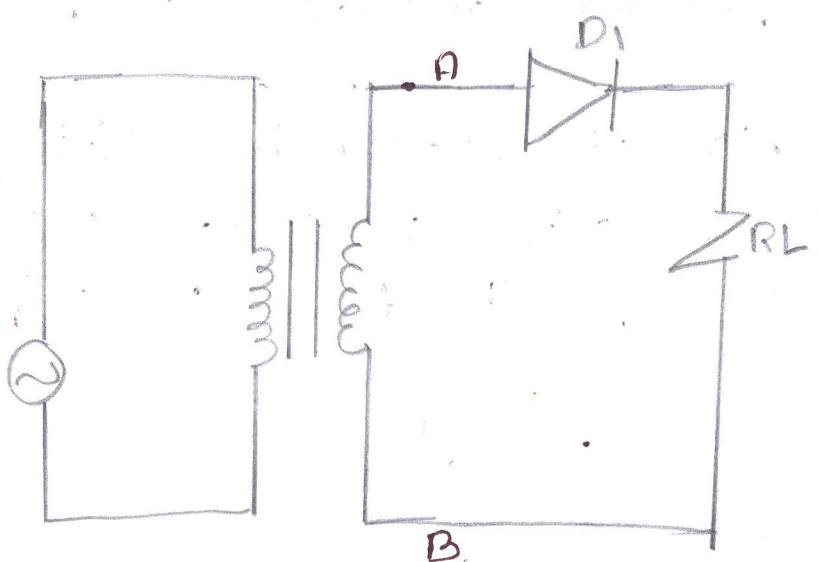
$$\eta = \frac{P_{dc}}{P_{ac}}$$

$$\eta = \frac{\frac{I_m^2}{\pi^2} \times R_L}{\frac{I_m^2}{2} \times (R_S + 2\pi f + R_L)}$$

neglect  $R_S + 2\pi f$

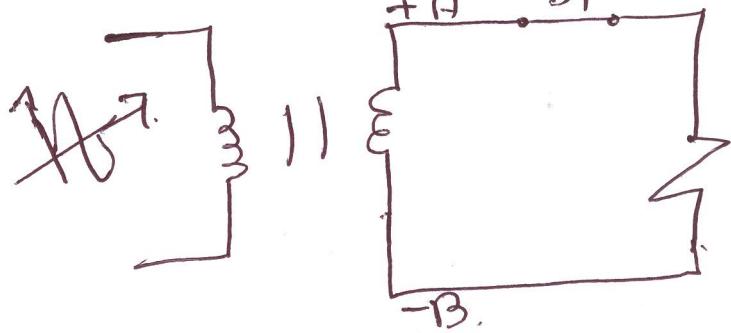
$$\eta = 80.5\%$$

3Y  
5Y.



In half wave rectifier only one diode is present

during forward bias the node A is positive and node B is negative hence diode acts as a closed switch so the current will be flow.



During reverse bias the node B is positive and node A is negative hence diode acts as an open switch so there is no flow of current.

