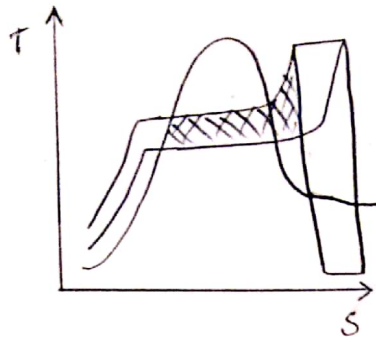


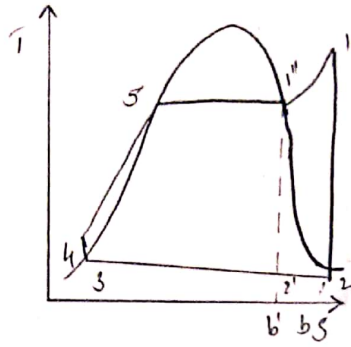
1) a) Effect of Boiler Pressure :-



The effect of increasing the boiler pressure, the Rankine cycle efficiency is illustrated on T-s diagram.

In this case, the max temp of the steam as well as exhaust pressure are kept constant. Increase in boiler pressure result in decrease in heat rejection given by the area $2-x-x'-2'-2$. Further the net work increases by the amount shown by area of double cross hatching. However it decreases by the amount shown by area of single cross hatching. Thus there will not be much change in the net work since heat rejected decreases, this results in an increase in Rankine efficiency with an increase in boiler pressure.

Effect of Superheat:-



The above figure shows the effect of superheat on the Rankine cycle. It is evident that the work increased by area $1'-1-2-2'-1'$. The heat transferred in the boiler increased by area $1'-1-b-b'-1'$. The ratio of these two areas is greater than the ratio of work to heat supply for the rest of the cycle. Hence by the given pressure, superheating the steam increases the Rankine cycle efficiency. Further when the steam is superheated the quality of the steam leaving the turbine increases.

1) b) GIVEN DATA:

$$T_1 = 400^\circ\text{C} \rightarrow P_1 = 10 \text{ bar}$$

$$T_3 = 300^\circ\text{C} \rightarrow P_3 = 1 \text{ bar}$$

$$T_2 = 40^\circ\text{C} \rightarrow P_{\text{sat}} = 0.07 \text{ bar}$$

$$x = 100 - 14.67 = 85.33\% = 0.85$$

$$h_1 = 3180$$

$$h_g = h_f \text{ at } 40^\circ\text{C}$$

$$h_2 = 2780$$

$$h_g = 167.4$$

$$h_3 = 3040$$

$$h_4 = 2220$$

$$w_p = v_f (P_1 - P_2) \times 100$$

$$w_p = 6.89 \text{ kJ/kg}$$

$$w_p = h_6 - h_5$$

$$h_6 = w_p + h_5$$

$$h_6 = 173.43 \text{ kJ/kg}$$

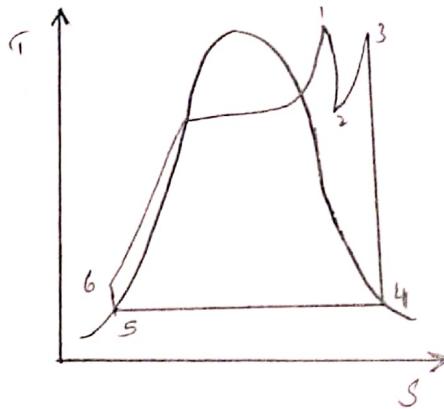
$$\eta = \frac{w_T - w_p}{Q_s}$$

$$= \frac{1220 - 6.39}{3006.57}$$

$$= 0.4036 \times 100 = \underline{40.36\%}$$

$$h_f = 167.4 \text{ kJ/kg}$$

$$v_f = 0.001$$



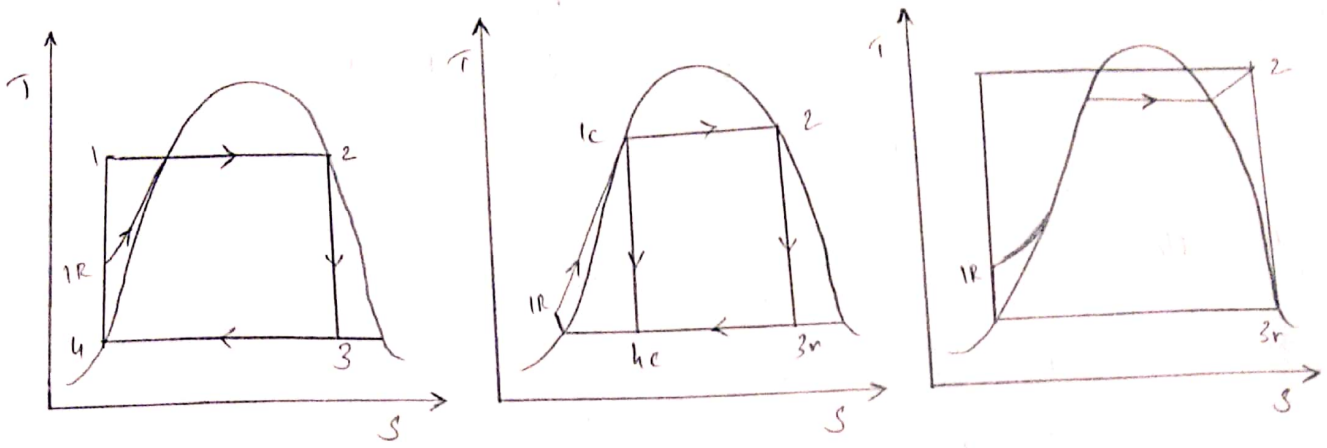
$$w_T = (h_1 - h_2) + (h_3 - h_4)$$

$$w_T = (3180 - 2780) + (3040 - 2220)$$

$$w_T = \underline{1220} \text{ kJ/kg}$$

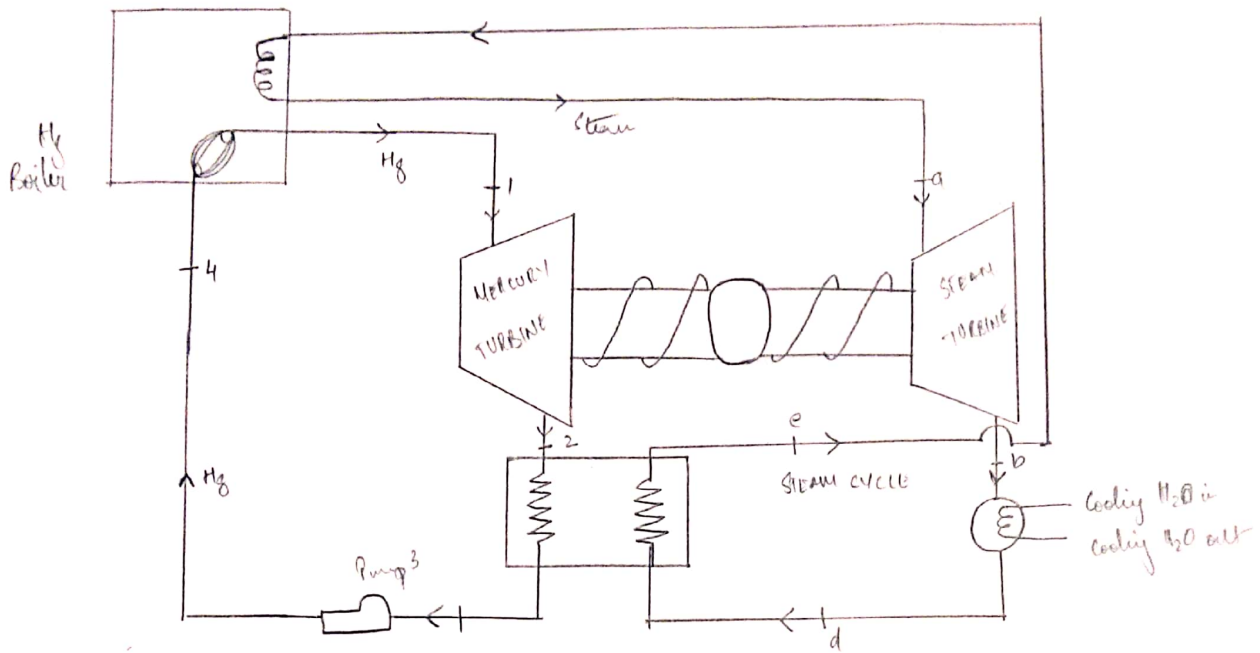
$$Q_s = h_1 - h_6 = 3180 - 173.43$$
$$= \underline{3006.57} \text{ kJ/kg}$$

1) c) Rankine and Carnot Cycle



- > In Rankine cycle steam undergoes complete condensation.
- > In Carnot cycle steam undergoes partial condensation.
- > Rankine cycle can be used with any type of steam. Where as Carnot cycle is used only with wet steam.
- > Carnot cycle gives more efficiency in practice because of large pump work.
- > Carnot cycle cannot be realized in practice because of large pump work.

2) a) Binary Vapour Cycle :-



The Carnot cycle efficiency will increase with an increase in initial supply temperature or with the decrease in exit temperature. It has been already seen that the exit temperature is limited by the length of cooling water. The atmospheric temp when steam is used as working fluid, the rise in temperature is accompanied by rise in pressure. High pressure of the steam creates many difficulties in design, operation or control. It would seem at first sight that, by superheating

high steam temperature. could be obtained without
the necessity of high pressure. It is found that the
thermal efficiency of the cycle depends more on
the saturation temperature corresponding to supply pressure
than on the superheat temperature.

2) b) Psychrometric Properties :-

→ Dry Air : The mixture of nitrogen and oxygen neglecting the water vapour and other gases is known as dry air.

→ Moist Air : Mixture of dry air and water vapour is known as moist air / saturated air.

→ Dry Bulb Temperature : The temperature of air is measured by an ordinary thermometer is known as dry bulb temperature.

→ Wet Bulb Temperature : The temperature of air measured by a thermometer where its bulb is covered to the wet cloth and is exposed to the air.

→ Dew Point Temperature : It is the temp at which water vapour mixture present in the air begins to condense when the air is cooled.

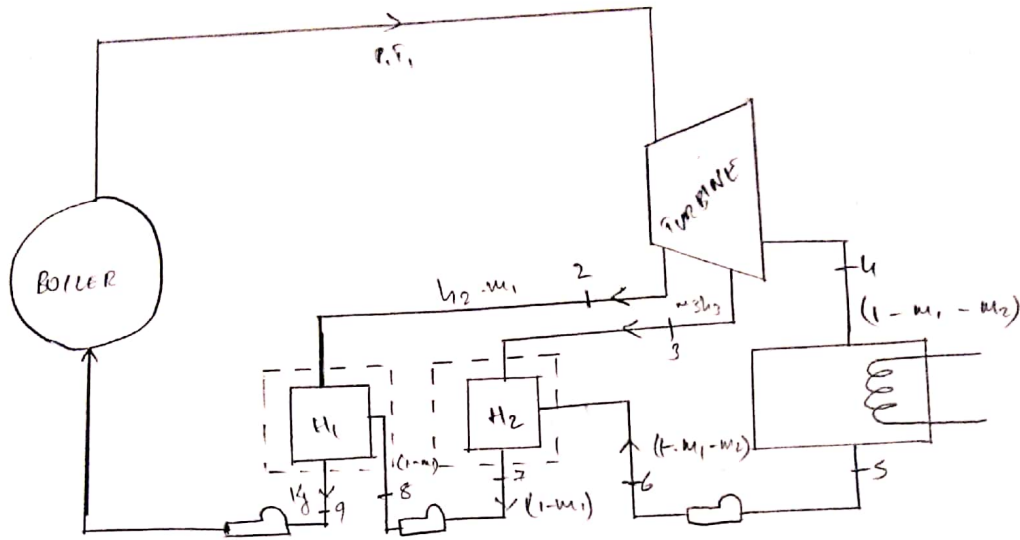
Specific Humidity : It is the mass of water vapour present in 1 kg of dry air.

→ Absolute Humidity: The mass of water vapour present in
the unit volume of dry air is known
as absolute humidity.

→ Relative Humidity: It is the ratio of actual mass of
water vapour in a given volume of
dry air to the mass of water vapour.

Degree of saturation: It is defined as the mass of
water vapour in unit mass of dry air to
the mass of water vapour where air is
saturated at same temperature.

2) c) Open Feed Water Heater :-



The feed water enters the boiler at a temperature between 10 to 150°C, and it is heated by steam extracted from intermediate stages of the turbine.

For every 1 kg of steam entering the turbine, let $m_1 \text{ kg}$ of steam extracted from an intermediate stage of the turbine where the pressure is P_2 and it is used to heat up feed water ($1 - m_1 \text{ kg}$ at state 1) by mixing in heater 1. The remaining $1 - m_1 \text{ kg}$ of steam expands in the turbine from pressure P_2 (state 2) to pressure P_3 (state 3). When $m_2 \text{ kg}$ of steam is extracted for heating feed water in heater 2.

→ Cycle Efficiency $\eta_{CF} = \frac{Q_s - Q_r}{Q_s} = \frac{W_T - W_P}{W_T}$

~~5/4) Ideal requirements~~

→ Steam flow rate S.F.R. = $\frac{3600}{w_r - w_p}$ Kg (Kw.h)

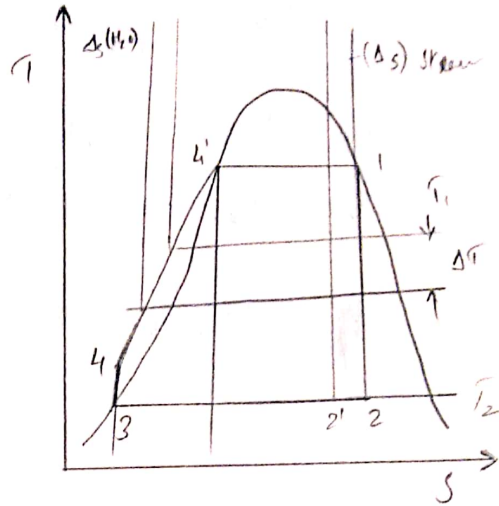
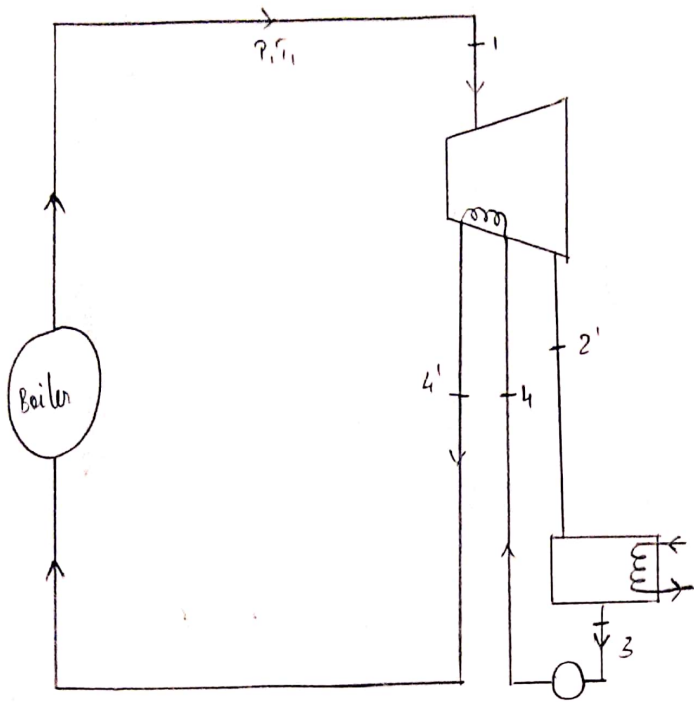
→ Energy balance for heater 1

$$m_1 = \frac{h_7 - h_8}{h_2 - h_8}$$

→ Energy balance for heater 2

$$m_2 = \frac{(h_7 - h_6)(1 - m_1)}{(h_3 - h_6)}$$

3) a) Ideal Regenerative Cycle :-



- > For maximum efficiency all heat should be supplied at T_1 and feed water should enter the boiler at state $4'$.
- > This may be accomplished in what is known as ideal regenerative cycle.
- > The feature of the ideal ~~reg~~ regenerative cycle is that the condensate after leaving the pump circulates around the turbine casing in counter flow to the direction.
- > Δs of water is $\Delta s (H_2O) = -\Delta s (steam)$. Also the slopes of line $(1-2')$ & $(4'3)$ will be identical at every temperature and lines will be identical in contour.
- > The areas $4-4'-b-a-4$ & $2'-1-d-c-2''$ are equal. Therefore all the heat added from an external source is at contact temperature T_1 and all heat rejected is

at constant temperature.

$$Q_S = h_1 - h_4' \quad , \quad Q_R = h_2' - h_3$$

$$\therefore \eta_{RK} = \frac{Q_S - Q_R}{Q_S}$$

$$Q_S = h_1 - h_4' = T_1 (S_1 - S_4')$$

$$Q_R = h_2' - h_3 = T_2 (S_2' - S_3)$$

$$\eta_{RK} = \frac{Q_S - Q_R}{Q_S} = \frac{T_1 (S_1 - S_4') - T_2 (S_2 - S_3')}{T_1 (S_1 - S_4')}$$

b) Limitations of Carnot Cycle :-

- > Carnot cycle is the most efficient one but it is not practically possible.
- > Isothermal heat addition in boiler takes place only in wet region, but super heating of steam cannot be taken inside the boiler as it produces steam.
- > During isothermal condensation process the condensation is stopped.
- > The higher power requirement for compression reduces the plant efficiency.
- > The plant size for the specified power output is large as the specific steam consumption is higher.

c) GIVEN DATA:-

$$P_1 = 25 \text{ bar}$$

$$P_2 = 0.2 \text{ bar}$$

$$x = 80\%$$

$$T_{\text{sup}} = 16.18^\circ\text{C}$$

$$H_1 = 2640$$

$$H_2 = 2180$$

$$t_s = 60.09^\circ\text{C}$$

$$V_g = 0.0010172 \text{ m}^3/\text{kg}$$

$$h_f = 251.5 \text{ kJ/kg}$$

$$H_3 = h_f = 251.5 \text{ kJ/kg}$$

$$\begin{aligned} W_p &= V_g (P_1 - P_2) \times 100 \\ &= 0.0010172 (25 - 0.2) \times 100 \\ &= 2.52 \end{aligned}$$

$$\begin{aligned} H_4 &= W_p + H_3 \\ &= 2.52 + 251.5 \\ &= 254.02 \end{aligned}$$

$$\begin{aligned} Q_s &= (H_1 - H_4) \\ &= (2640 - 254.02) \\ &= 2385.98 \text{ kJ/kg} \end{aligned}$$

$$\begin{aligned} W_T &= (H_1 - H_2) \\ &= 2640 - 2180 \\ &= 460 \text{ kJ/kg} \end{aligned}$$

$$\begin{aligned} W_{\text{net}} &= W_T - W_p \\ &= 460 - 2.52 \\ &= 457.48 \text{ kJ/kg} \end{aligned}$$

$$\eta_p = \frac{W_{\text{net}}}{Q_s} = \frac{457.48}{2385.98} \times 100 = 19.17\%$$