

Internal Assessment Test 1 – March 2019

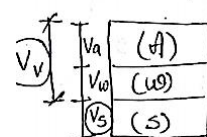
Sub:	Basic Geotechnical Engineering				Sub Code:	15CV45	Branch:	CIVIL		
Date:	7/3/2019	Duration:	90 mins	Max Marks:	50	Sem / Sec:	4A & 4B	OBE		
<b>Answer ALL Questions</b>								MARKS	CO	RBT

1 (a) Differentiate between: [4] CO1 L2

1) Void ratio and porosity

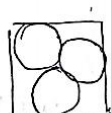
$w_s, m_s \rightarrow$  mass of water, solids

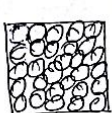
**Void Ratio ( $e$ )**: It is defined as the ratio of volume of voids to volume of solids.



$$e = \frac{V_v}{V_s}$$

{expressed as decimals}  
→ NO UNIT

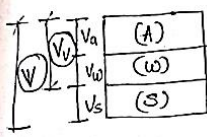




Individual voids are larger in coarse grained soils but total void ratio is more for fine grained soils.

$e_{coarse} < e_{fine}$

**Porosity ( $n$ )** - It is the ratio of volume of voids to the total volume of soil. It is another way of representing the relative voids to solids proportion.



$$n = \frac{V_v}{V} \times 100$$

expressed as a %  
→ NO UNIT

$0 \leq n \leq 100$  Max limit is 100%

2) Specific gravity of solids and mass specific gravity

**Specific gravity of solids ( $G_s$ )**

' $G_s$ ' is the ratio of weight of soil solids to the weight of equal volume of water at 4°C.

$$G_s = \frac{W_s}{V_s \cdot \gamma_w}$$

$$= \frac{W_s}{V_s} \cdot \frac{1}{\gamma_w}$$

$$G_s = \frac{\gamma_s}{\gamma_w}$$

$G_s$

Sands & gravels	2.65-2.68
Silt	2.66-2.70
Inorganic clay	2.70-2.80
Soils with iron/mica	2.75-2.85
Organic soils	< 2

wt of solids to unit

② Mass specific gravity or specific gravity

$$G_m = \frac{W}{V \cdot \gamma_w} = \frac{(w)}{\frac{\gamma_w}{\gamma_s}} = \frac{\gamma}{\gamma_w}$$

$G_m$  is the ratio of bulk unit weight to unit weight of water. or  $G_m$  is the ratio of weight of total soil mass to

1 (b) Prove from phase diagram that  $\gamma_t = \left(\frac{G_s + se}{1+e}\right) \gamma_w$  [6] CO1 L3

$$\gamma_t = \frac{W}{V} = \frac{W_s + W_w}{V_s + V_v} = \frac{\gamma_s V_s + \gamma_w V_w}{V_s + V_v}$$

we know  $V_s = 1$   $V_v = e$   $V_s = G_s \gamma_w$   $V_w = se$

$$\gamma_t = \frac{G_s \gamma_w + \gamma_w (se)}{1+e}$$

$$\gamma_t = \frac{\gamma_w (G_s + se)}{1+e}$$

To write in terms of water content (w)

$$w G_s = se$$

$$\gamma_t = \frac{\gamma_w (G_s + w G_s)}{1+e}$$

$$\gamma_t = \frac{\gamma_w G_s (1+w)}{1+e}$$

2 (a) A fully saturated soil sample has a water content of 35 % and specific gravity of solids of 2.65. Determine its porosity, saturated unit weight and dry unit weight. [4] CO1 L3

2 (b) A 5000 m<sup>3</sup> embankment is to be constructed with a void ratio of 0.85. The details of the borrow pits are given below. Find the most economical pit. [6] CO1 L3

Pit	Void ratio	Cost per m <sup>3</sup>
X	0.95	30
Y	1.65	25

③ Embankment      pit A      pit B      pit C

Given       $e = 0.85$        $e = 0.95$        $e = 0.90$        $e = 1.65$

$V = 5000 \text{ m}^3$        $R_s 30/\text{m}^3$        $R_s 16/\text{m}^3$        $R_s 25/\text{m}^3$

To find       $\rightarrow$  Which pit is economical??

$n = \frac{e}{1+e}$   
 $= \frac{0.85}{1.85}$   
 $= 0.46$

$\frac{V_v}{V} = 0.46$

$V_v = 0.46(5000)$   
 $= 2300 \text{ m}^3$

$V_s = V - V_v$   
 $= 5000 - 2300$   
 $= 2700 \text{ m}^3$

$V_s = \sqrt{2700 \text{ m}^3}$

$e = \frac{V_v}{V_s} = 0.95$

$V_v = 0.95(2700)$   
 $= 2565 \text{ m}^3$

$V = V_s + V_v$   
 $= 5265 \text{ m}^3$

Cost =  $30 \times V$   
 $= 30 \times 5265$   
 $= \text{Rs } 1,57,950$

$V_s = \sqrt{2700 \text{ m}^3}$

$e = \frac{V_v}{V_s} = 0.90$

$V_v = 0.90(2700)$   
 $= 2430 \text{ m}^3$

$V = V_s + V_v$   
 $= 5130 \text{ m}^3$

Cost =  $16 \times 5130$   
 $= \text{Rs } 82,080$

$V_s = \sqrt{2700 \text{ m}^3}$

$e = \frac{V_v}{V_s} = 1.65$

$V_v = 1.65(2700)$   
 $= 4455 \text{ m}^3$

$V = V_s + V_v$   
 $= 7155 \text{ m}^3$

Cost =  $25 \times 7155$   
 $= \text{Rs } 1,78,875$

$\leftarrow$  pit C cost the highest \$  
 pit B cost the least hence  
 pit B is the most economical.

3(a) Explain the determination of water content by oven drying method.

[4] CO1 L1

① Oven Drying Method

The soil is taken in an airtight container. The weight of soil + container is  $W_1$ . Set the temperature to  $110^\circ\text{C}$  and keep the container in oven for 24 hours. After drying the soil + container is weighed as  $W_2$ . The weight of dry empty container  $W_3$ .

water content =  $\frac{\text{Weight of water}}{\text{Weight of soil}} = \frac{W_1 - W_2}{W_2 - W_3}$

The minimum quantity of sample to be kept in oven depends on the size of particles. If size of particles is more than the sample required is more.

Temperature

A temperature of  $110^\circ\text{C}$  is not good for soils having gypsum or more organic content.

gypsum has its water of crystallization @ high temp.  
 organic soils starts decomposing @ high temperature.

Hence for soils having gypsum or organic matter a temp of  $60^\circ\text{C} - 80^\circ\text{C}$  is sufficient.

3(b) In a specific gravity test the following observations were recorded :

[6] CO1 L3

Mass of dry soil = 103 g  
 Mass of density bottle + soil + water = 538 g  
 Mass of density bottle + water = 474.6 g  
 What is the specific gravity of solids? What is the percentage error in calculating specific gravity if 2.5 ml of air got entrapped in mass of density bottle + soil + water?

Part 1

Given

$$W_2 - W_1 = 103 \text{ g}$$

$$W_3 = 538 \text{ g}$$

$$W_4 = 474.6 \text{ g}$$

Solution (Part 1)

$$G_s = \frac{W_2 - W_1}{(W_4 - W_1) - (W_3 - W_2)}$$

$$= \frac{W_2 - W_1}{W_4 - W_1 - W_3 + W_2}$$

$$= \frac{W_2 - W_1}{W_4 - W_3 + (W_2 - W_1)}$$

$$= \frac{103}{474.6 - 538 + 103}$$

$$G_s = 2.601$$

To find

$G_s$

$W_1$  = weight of density bottle which is not given

Part 2

Given

2.5 ml of air was entrapped in weight of density bottle + soil + water

To find

% error in calculating  $G_s$

Solution

$W_3$  = weight of density bottle + soil + water  
2.5 ml of air in  $W_3$  will cause change in weight of water

2.5 ml of air is in  $W_3 = 538 \text{ g}$   
To remove it 2.5 ml of water should be added  
 $\approx 2.5 \text{ ml} \times 1 \text{ g/ml} = 2.5 \text{ g}$  of water

$$\text{Corrected } W_3 = W_3 - 2.5 = 538 - 2.5 = 540.5 \text{ g}$$

$$\text{Corrected } G_s = G_s = \frac{103}{474.6 - 540.5 + 103} = 2.77$$

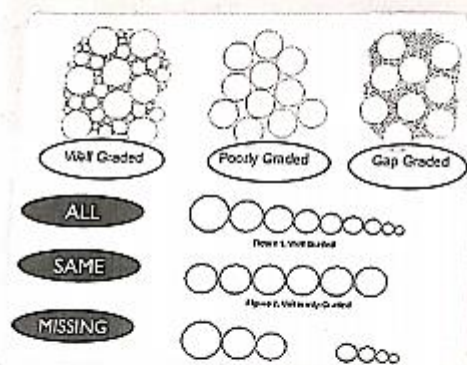
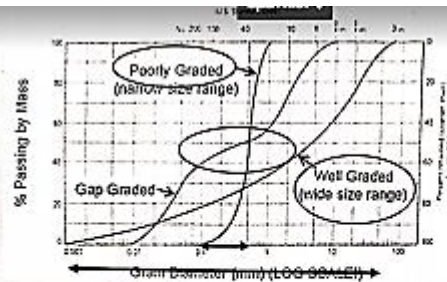
$$\% \text{ error} = \frac{\text{Exact value} - \text{Estimated value}}{\text{Exact value}}$$

$$= \frac{2.77 - 2.601}{2.77} = +6.1\%$$

4 (a) Explain with a particle size analysis curve :

- 1) Well graded soil
- 2) Gap graded soil
- 3) Poorly graded soil
- 4) Fine grained soil

[4] CO1 L2



Well graded - All particle sizes are present. They have very less voids, good strength and less settlement.

Poorly graded - (Uniformly graded), They have same sizes of particles, more voids, more settlement.

Gap graded - Some grain sizes are missing. On loading this soil will segregate causing settlement.

4 (b) A soil sample consisting of particles ranging from 0.5 mm to 0.01 mm is put on the surface of still water of 5 m deep tank. Calculate the time of settlement of the coarsest and finest particles of the sample to the bottom of the tank.  $G_s = 2.66$  and  $\eta = 0.01$  poise.

[6] CO1 L3

Given  $\sigma_w$  find  
 $\eta$

Coarse  $D = 0.5 \text{ mm}$   
 fine  $D = 0.01 \text{ mm}$   
 $H_c = 5 \text{ m}$   
 $G_s = 2.66$   
 $\eta = 0.01 \text{ poise}$   
 $= 0.01 \times 100 \frac{\text{N.s}}{\text{m}^2}$   
 $= 0.01 \frac{\text{N.s}}{\text{m}^2}$

$1 \text{ poise} = 0.1 \frac{\text{N.s}}{\text{m}^2}$

Coarse

$$\frac{H_c}{t} = \frac{(G_s - G_w) \cdot D^2}{18 \eta} = \frac{\gamma_w (G_s - 1) D^2}{18 \eta}$$

$$\frac{5}{t} = \frac{10 \times 1000 (2.66 - 1) \times (0.5 \times 10^{-3})^2}{18 \times 0.01}$$

$$\Rightarrow t = 21.68 \text{ s}$$

Fine

$$\frac{H_c}{t} = \frac{\gamma_w (G_s - 1) D^2}{18 \eta}$$

$$\frac{5}{t} = \frac{10 \times 1000 (2.66 - 1) \times (0.01 \times 10^{-3})^2}{18 \times 0.01}$$

$$\Rightarrow t = 15.06 \text{ hours}$$

5 (a) Explain the determination of in-situ density by core cutter method.

[5] CO1 L1

① CORE CUTTER METHOD.

Core cutter is an open cylindrical barrel with one cutting edge. Measure the dimensions of the core-cutter - height (H), Diameter (D). Find the volume of core-cutter as  $V = \frac{\pi D^2 H}{4}$ . Find empty weight of core-cutter ( $W_1$ )

Place the dolly over the core-cutter and ram into the earth with the dolly till few cm of dolly protrudes out of the earth. The soil surrounding the core-cutter is removed. The core-cutter along with the dolly is removed. The dolly is removed and soil extruding out of core-cutter is removed.

Weight of core-cutter + soil is  $W_2$ .

$$\text{Unit Weight (Bulk unit weight)} = \frac{W_2 - W_1}{V}$$

$$\text{In-situ - bulk density} = \frac{M_2 - M_1}{V}$$

The method is suitable for soft fine grained soil. It is unsuitable for hard soils and coarse grained soils.

5 (b)	<p>A sample of sand was found to have a water content of 20 % and bulk unit weight of 1.93 g/cc. Laboratory tests on the soil sample indicated the void ratios in the loosest and densest possible states are 0.90 and 0.50 respectively. Calculate the relative density. Take <math>G_s = 2.65</math>.</p> <p>Given <math>w = 0.20</math>  <math>\gamma_t = 1.93 \text{ g/cc}</math>  <math>e_{\max} = 0.90</math>  <math>e_{\min} = 0.50</math>  <math>G_s = 2.65</math></p> <p>To find <math>I_d, s</math></p> <p>Solution</p> $\rho_d = \frac{\gamma_t}{1+w} = \frac{1.93}{1+0.20} = 1.608 \text{ g/cc}$ $\rho_d = \frac{G_s \rho_w}{1+e} \quad \rho_w = 1 \text{ g/cc}$ $1.608 = \frac{2.65 \times 1}{1+e} \Rightarrow e = 0.648$ $I_D = \frac{e_{\max} - e}{e_{\max} - e_{\min}} \times 100$ $= \frac{0.90 - 0.648}{0.90 - 0.50} \times 100$ $= \underline{\underline{63\%}}$ $s = G_s e$ $0.20 \times 2.65 = s \times 0.648$ $\Rightarrow s = \underline{\underline{0.818}}$	[5]	CO1	L2
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Signature of CI

Signature of CCI

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