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15CV72

Seventh Semester B.E. Degree Examination, Dec.2019/Jan.2020 Design of RCC and Steel Structures

Time: 3 hrs.

Max. Marks: 80

- Note:** 1. Answer any TWO full questions, choosing ONE full question from each module.
2. Use of IS456, IS800, SP(6)-Steel Table is permitted.
3. Assume any missing data suitably.

Module-1

- 1 Design a reinforced concrete combined rectangular slab footing for two columns located at 4.5 m apart. The overall sizes of the columns are 400mm × 400mm and 600mm × 600mm and they are transferring 600 kN and 1000 kN respectively. The centre of the lighter column is 0.4m from the property line. The safe bearing capacity of the soil 150 kN/m². Use M20 concrete and Fe 415 steel. Sketch the reinforcement details. (40 Marks)

OR

- 2 Design a cantilever retaining wall to retain an earth embankment with a horizontal top 3.5m above ground level. Density of earth 18 kN/m³, angle of internal friction $\phi = 30^\circ$. SBC of soil is 200 kN/m³. Take coefficient of friction between soil and concrete 0.5, Adopt M20 grade concrete and Fe 415 steel. (40 Marks)

Module-2

- 3 The centre line of a roof truss is as shown in the Fig.Q3. The forces in the members of the truss due to dead load, live load and wind load is given below: Design the roof truss member using M16 bolts of property class 4.6. Also design a bearing plate and anchor bolts for a pull of 40 kN. Use M20 grade concrete. Draw to suitable

(i) Elevation of truss greater than half space (ii) Support details.

Member	DL (kN)	LL (kN)	WL (kN)
AB	+ 14.37	+ 21.80	- 37.32
BC	+ 11.64	+ 17.60	- 32.08
CD	+ 12.05	+ 18.26	- 35.90
DE	- 5.13	- 7.70	+ 14.70
EC	+ 2.77	+ 4.18	- 8.42
EB	+ 2.77	+ 4.18	- 9.15
EA	- 12.85	- 19.36	+ 31.69
EF	- 7.69	- 11.61	+ 15.63

Sign :- + \Rightarrow Compression
 - \Rightarrow Tension

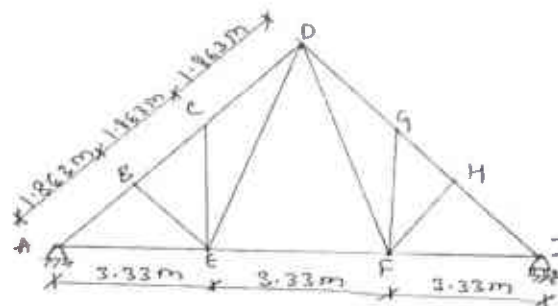


Fig.Q3

(40 Marks)

Important Note : 1. On completing your answers, compulsorily draw diagonal cross lines on the remaining blank pages.
2. Any revealing of identification, appeal to evaluator and /or equations written eg, 42+8 = 50, will be treated as malpractice.

OR

4 Design a simply supported gantry girder to carry an electrically operated travelling crane with the following details:

- (i) Span of the crane bridge \Rightarrow 25 m
- (ii) Span of the gantry girder \Rightarrow 8 m
- (iii) Wheel base \Rightarrow 3.5 m
- (iv) Crane capacity \Rightarrow 200 kN
- (v) Weight of crane bridge \Rightarrow 150 kN
- (vi) Weight of trolley (crab) \Rightarrow 75 kN
- (vii) Minimum hook distance \Rightarrow 1.0 m
- (viii) Weight of rail \Rightarrow 0.30 kN/m
- (ix) Height of rail \Rightarrow 105 mm

Draw neatly cross section of gantry girder showing all details. Also draw side view.

(40 Marks)

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for the Academic Years 2018-19, 2019-20 and 2020-21)
Channasandra, Dr. Vishnuvardhan Road, Bengaluru - 560 098
DEPARTMENT OF CIVIL ENGINEERING

From,
Chairman
BoE-CV/TR/EV 2019
VTU, Belagavi

It is hereby informed that the Question Paper, Scheme and Solutions in the following subjects are found to be in order

Sl No	Subject Code	Name of the Subject	Remarks
1	15CV71	Municipal and Industrial Wastewater Engineering	Found correct
1	15CV72	Design of RCC and Steel Structures	Found Correct ✓

Thanking you



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Registrar (Evaluation)

Vivekananda Technological University
BELAGAVI - 590018



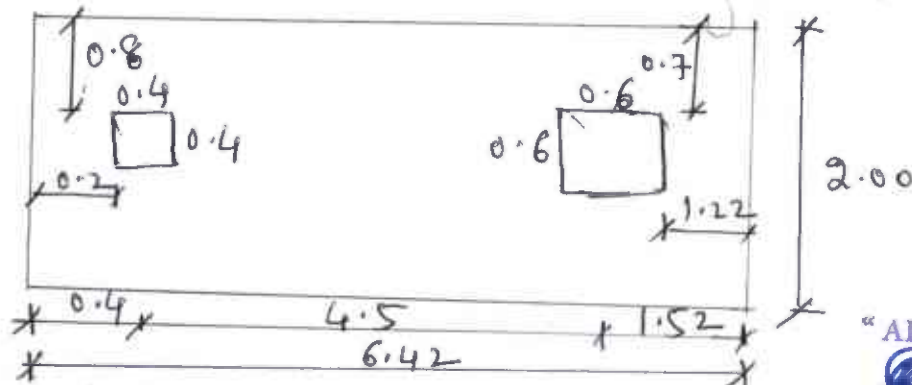
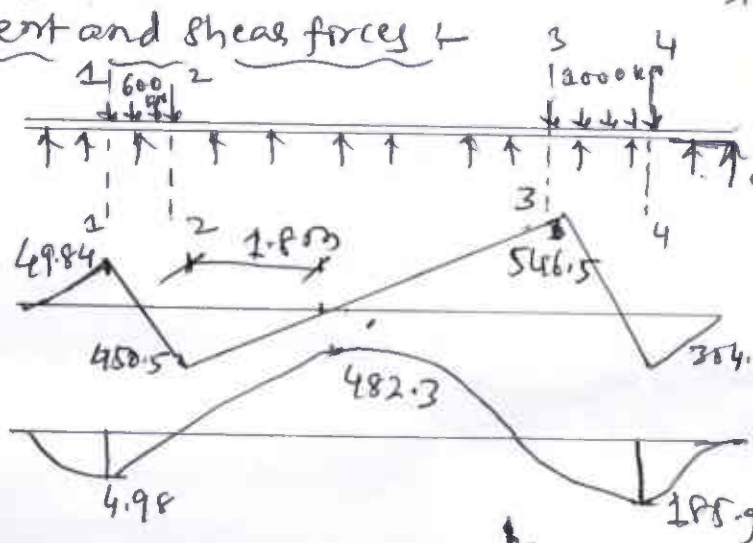
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Belagavi, Karnataka - 590 018

15CV72

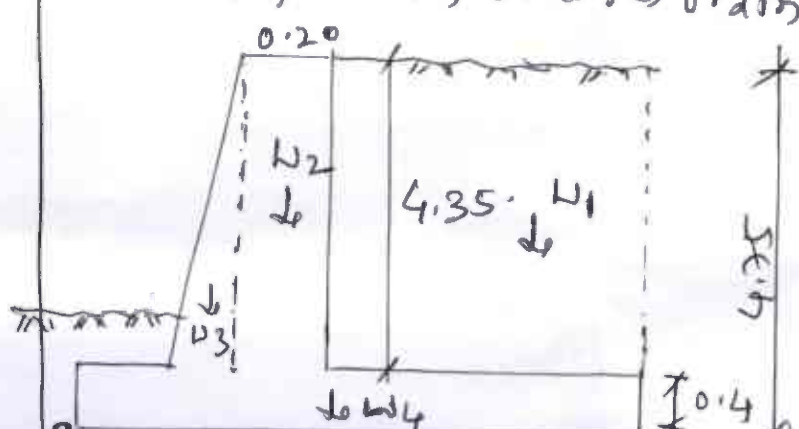
Scheme & Solution

Signature of Scrutinizer
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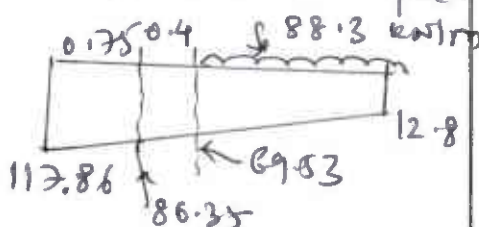
Subject Title: Design of RCC & Steel structures Subject Code: 15CV72

Question Number	Solution	Marks Allocated
1	<p align="center"><u>Module 1</u></p> <p>$\bar{x} = \frac{600 \times 0 + 1000 \times 4.5}{(600 + 1000)} \Rightarrow 2.81 \text{ m}$</p> <p>Property line is at distance $\Rightarrow 0.4 \text{ m}$ from centre line of column 1.</p> <p>\therefore Length of footing = $L = 2 [2.81 + 0.4]$ $L \Rightarrow 6.42 \text{ m}$</p> <p>Area of footing = $\frac{1}{150} [600 + 1000] \Rightarrow 11.73 \text{ m}^2$</p> <p>$\therefore$ Width of footing = $b = \frac{11.73}{6.42} \Rightarrow 1.83 \text{ m}$ $\approx 2.00 \text{ m}$</p>  <p align="center"><u>Moment and Shear forces</u></p>  <p>$q = \frac{600 + 1000}{6.42} \Rightarrow 249.2 \text{ kN/m}$</p> <p align="right">SFD BMD</p>	<p align="center">05</p> <p align="center">"APPROVED" <i>[Signature]</i> Registrar (Evaluation) Visvesvaraya Technological University BELAGAVI - 590018</p> <p align="center">05</p>

Question Number	Solution	Marks Allocated
	<p>SF @ 1-1 \Rightarrow 49.84 kN SF @ 2-2 \Rightarrow -450.5 kN " " 3-3 \Rightarrow 546.5 kN " " 4-4 \Rightarrow -304 kN</p> <p>B.M @ 1-1 \Rightarrow -4.98 kNm " " 2-2 \Rightarrow -185.9 kNm max B.M \Rightarrow 482.3 kNm</p>	
	<p>$M_u = 1.5 \times 482.3 \Rightarrow 723.5 \text{ kNm}$</p> <p>Critical section for shear is @ a distance 'd' from the face of heavier column.</p> <p>$\therefore [V_u = 546.5 - 249.2 \times \frac{d}{1000} \text{ kN}]$</p> <p><u>Depth of footing</u>: For minimum of 0.2% reinforcement strength of concrete is 0.32 N/mm², Equating the resisting shear to shear force, we get-</p> <p>$[\therefore d = 614.6 \text{ mm} \approx 620 \text{ mm}]$</p> <p>$M_u = 0.36 f_{ck} b \times u_{lim} (d - 0.42 \times u_{lim})$ $= 21219 \text{ kN-m} > M_u$ Hence depth is okay.</p> <p>\rightarrow check the depth for two way shear [for both columns]</p> <p>\rightarrow <u>Reinforcement in long direction</u> $\leftarrow M_u = 723.5 \text{ kNm}$</p> <p>$A_{st} = 3428 \text{ mm}^2$ [provide 16mm bars @ 110mm c/c]</p> <p><u>maximum -ve moment</u> $\leftarrow M_u = 185.5 \text{ kNm}$ $[M_u = 1.5 \times 185.5]$</p> <p>$[A_{st} = 1270 \text{ mm}^2]$</p> <p>$[A_{st_{min}} = 912 \text{ mm}^2]$ [provide 16mm bars @ 300mm c/c]</p> <p><u>Transverse steel</u> \leftarrow</p>	<p>05</p> <p>05</p> <p>10</p>

Question Number	Solution	Marks Allocated
	<p><u>under column 1</u> $M_u = 118.03 \times 10^6 \text{ N-mm}$ [provide 16mm $A_{st} = 544 \text{ mm}^2$ bars @ 220 mm c/c $A_{st} = 816 \text{ mm}^2$ (mm)]</p> <p><u>under column 2</u> $M_u = 61.25 \times 10^6 \text{ N-mm}$ $< 118.03 \times 10^6 \text{ N-mm}$ \therefore [provide 16mm bars @ 220 mm c/c and provide 16mm @ 300 mm c/c in the middle] \rightarrow draw neat sketch</p>	<p>05</p> <hr/> <p>05</p> <hr/> <p>10</p>
<p>Q2)</p>	<p>$\sqrt{s} = 18 \text{ kN/m}^3, \phi = 30^\circ, \text{SBC} = 200 \text{ kN/m}^2 = 90$ $M = 0.15, f_{ck} = 20 \text{ N/mm}^2, f_y = 415 \text{ N/mm}^2$ $K_a = \frac{1 - \sin \phi}{1 + \sin \phi} \Rightarrow \frac{1}{3}$, min. depth of foundation $\Rightarrow \frac{90}{\sqrt{s}} K_a^2 \Rightarrow 1.23 \text{ m} \approx 1.25 \text{ m}$ \therefore Height of retaining wall $\Rightarrow 3.5 + 1.25 \Rightarrow 4.75 \text{ m}$ <u>Dimensions of retaining wall</u> :- $B = 0.48H + 0.56H \Rightarrow 2.50 \text{ m}$ toe projection $\Rightarrow 0.36 \Rightarrow 0.75 \text{ m}$ Thickness of base slab \Rightarrow Thickness of stem $= \frac{H}{12} \Rightarrow 0.4 \text{ m}$ Let the top width of stem $\Rightarrow 0.2 \text{ m}$</p> 	<p>05</p>

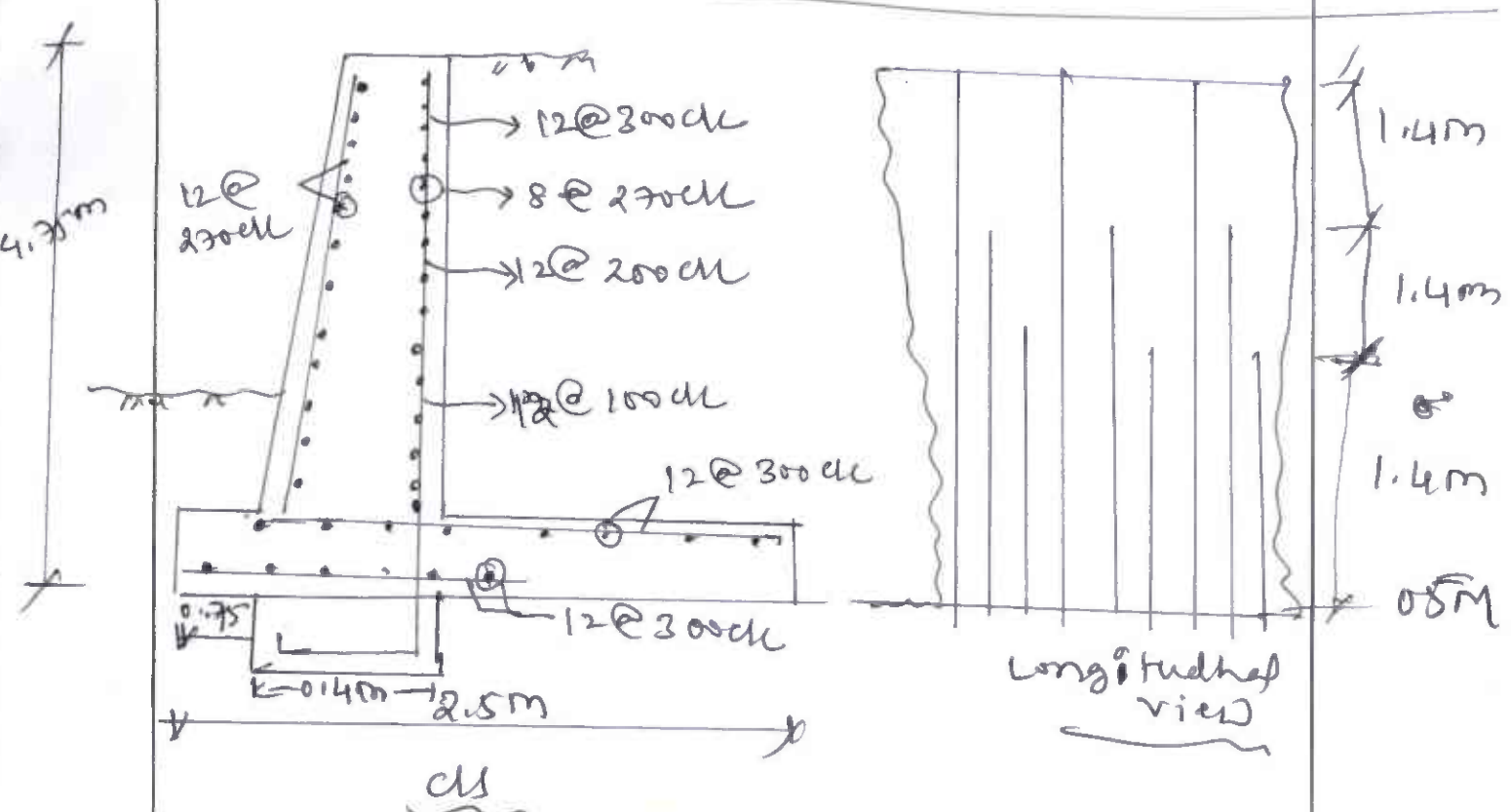
Question Number	Solution	Marks Allocated																				
	<p><u>Check for stability</u> ←</p> <table border="1" data-bbox="263 336 1348 918"> <thead> <tr> <th>Weight (kN)</th> <th>Weight (kN)</th> <th>\bar{x} in m</th> <th>M in kNm</th> </tr> </thead> <tbody> <tr> <td>1) Weight of base fill [W1]</td> <td>105.7</td> <td>1.825</td> <td>192.9</td> </tr> <tr> <td>2) Rectangular portion of stem [W2]</td> <td>21.75</td> <td>1.05</td> <td>23.84</td> </tr> <tr> <td>3) Triangular portion of stem [W3]</td> <td>10.88</td> <td>0.88</td> <td>9.61</td> </tr> <tr> <td>4) Base slab [W4]</td> <td>25</td> <td>1.25</td> <td>31.25</td> </tr> </tbody> </table> <p style="text-align: center;">$\Sigma W = 163.33$ kN $\Sigma M = 286.6$ kNm</p> <p>$P_H = \frac{1}{2} k_a \sqrt{H^2} \Rightarrow 67.688$ kN</p> <p>Overturning moment; $M_o = P_H \frac{h}{3} \Rightarrow 107.17$ kNm</p> <p>F.S. for overturning $\Rightarrow \frac{0.9 \times 286.6}{107.17} \Rightarrow 2.45 > 1.4$ OK</p> <p>Sliding $\Rightarrow \frac{0.9 \Sigma W}{P_H} \Rightarrow 1.09 > 1.4$</p> <p>[Hence shear key is to be provided.]</p> <p>pressure under slab ← moment about 'o'</p> <p>$\Rightarrow 286.6 - 107.17 \Rightarrow 179.43$ kNm</p> <p>Total vertical load $\Rightarrow 163.33$ kN</p> <p>$\bar{x} = 0.915$ m, & $e \Rightarrow 0.335$ m</p> <p>$P_{max/min} \Rightarrow \frac{\Sigma W}{b} \left[1 \pm \frac{6e}{b} \right]$</p> <p>[$P_{max} \Rightarrow 117.86$ kN/m² < safe stress]</p> <p>$P_{min} \Rightarrow 12.8$ kN/m²</p>	Weight (kN)	Weight (kN)	\bar{x} in m	M in kNm	1) Weight of base fill [W1]	105.7	1.825	192.9	2) Rectangular portion of stem [W2]	21.75	1.05	23.84	3) Triangular portion of stem [W3]	10.88	0.88	9.61	4) Base slab [W4]	25	1.25	31.25	05
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Question Number	Solution	Marks Allocated
	<p><u>Design of stem</u> ← Max moment $\Rightarrow \frac{1}{2} k_a \sqrt{h \times h^2}$ @ base of $\left[\begin{matrix} M \Rightarrow 82.31 \text{ kN} \\ M_u \Rightarrow 123.47 \text{ kNm} \end{matrix} \right]$</p> <p>$[A_{st} \Rightarrow 1041 \text{ mm}^2]$</p> <p>$[\text{provide } 12 \text{ mm } \phi \text{ bars @ } 100 \text{ mm c/c}]$</p> <p><u>Dist. Steel</u> ← $A_{st} = 360 \text{ mm}^2$</p> <p>$[\text{provide } 8 \text{ mm } \phi \text{ bars @ } 270 \text{ mm c/c}]$</p> <p><u>curtailment of bars</u> $\frac{1}{3}$rd of vertical bars may be curtailed @ a height of 1.5 m from base and another $\frac{1}{3}$rd @ a height of 3 m from the base.</p> <p>→ <u>Check for shear</u> ← $v_u = 160.75 \text{ kN}$ $\tau_v < \tau_c$ no shear reinforcement reqd.</p> <p><u>Design of Toe slab</u> ← </p> <p>$M_u = 45.285 \text{ kNm}$ $d = 350 \text{ mm}$ $A_{st} \Rightarrow 366 \text{ mm}^2 < A_{st} = 480 \text{ mm}^2$</p> <p>$[\text{provide } 12 \text{ mm } \phi \text{ bars @ } 300 \text{ mm c/c}]$</p> <p><u>Design of Heel slab</u> : $M_u = 77.35 \text{ kNm}$ $A_{st} \Rightarrow 418 \text{ mm}^2$</p> <p>$\therefore [\text{provide } 12 \text{ mm } \phi \text{ bars @ } 225 \text{ mm c/c}]$</p> <p><u>Design of shear key</u> ← pressure $\Rightarrow 86.35 \text{ kN/m}$ @ face provide 200 mm deep shear key</p>	<p>05</p> <p>05</p> <p>05</p>

Design of Rcc & steel structures . subject code : 15CV22

Q.No.

Marks



Module 2

Q 3)

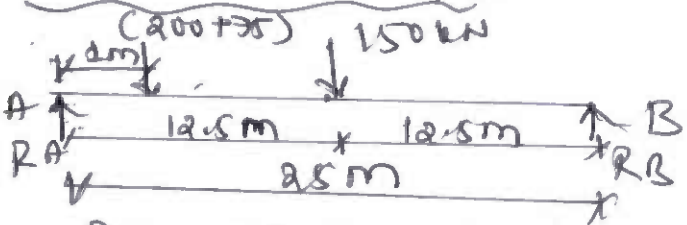
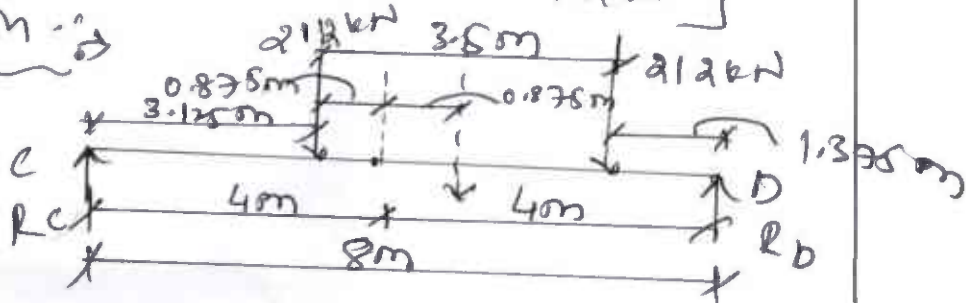
Member	DL+LL kN	DL+WL kN
AB	+36.17	-22.95
BC	+29.24	-20.44
CD	+30.31	-23.88
DE	-12.83	+9.57
EC	+6.95	-5.68
EB	+6.95	-6.38
EA	-32.21	+18.84
EF	-19.30	+7.94

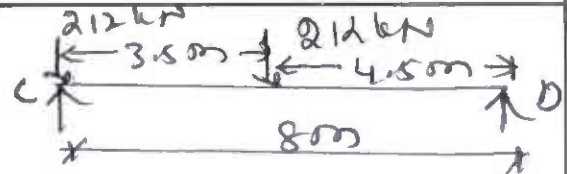
05

+ve - comp. , -ve - tension

Top chord member → +36.17 kN [C] & -23.88 kN [T]
 Bottom " → -32.21 kN [T] & +18.84 kN [C]
 Interior " → -12.83 kN [T] & +9.57 kN [C]

Question Number	Solution	Marks Allocated
	<p><u>Design of Top chord member</u> \perp [AB, BC, CD]</p> <p>comp force \Rightarrow 36.17 kN, ultimate \Rightarrow 54.26 kN force</p> <p>Length of member \Rightarrow 1.865 m</p> <p>Assume $f_{cd} = 50 \text{ N/mm}^2$, $A_{reqd} \Rightarrow 1088 \text{ mm}^2$</p> <p>$\rightarrow$ Choose suitable double angle from steel table</p> <p>\rightarrow check for $\Rightarrow P_d = A_e f_{cd} > 54.26 \text{ kN}$</p> <p>$\rightarrow$ <u>connectivity</u> \perp no of bolts \Rightarrow $\frac{54.26}{\text{Bolt value}}$</p> <p><u>Bolt value</u> \perp least of $\frac{1}{\sqrt{3}} \frac{V_{des}}{m_b} = f_u (n_m A_{nb} + n_s A_{sb})$</p> <p>2) $\frac{V_{des}}{m_b} = 2.5 k_b t d f_u$ \Rightarrow $\frac{V_{des}}{m_b} = k_b t d f_u$</p> <p>$\rightarrow$ sketch</p> <p><u>Design of Bottom chord</u> \perp</p> <p>Tension force \Rightarrow 32.21 kN, ult. force \Rightarrow 48.32 kN</p> <p>\rightarrow calculate area reqd</p> <p>\rightarrow choose double angle from steel table</p> <p>\rightarrow Check \perp Tdg \rightarrow Tds \rightarrow Tdb</p> <p>\rightarrow connectivity</p> <p>\rightarrow sketch</p>	<p>10</p> <p>10</p>

Question Number	Solution	Marks Allocated
	<p><u>Design of interior member</u></p> <p>Tension $\Rightarrow 12.83 \text{ kN}$, uplift force $\Rightarrow 19.24 \text{ kN}$ force</p> <p>\rightarrow calculate area reqd</p> <p>\rightarrow select suitable single angle from steel table</p> <p>\rightarrow Check for T_d, T_{dn} & T_{db}</p> <p>\rightarrow connection</p> <p>\rightarrow sketch</p> <p>\Rightarrow Design of Bearing plate and anchor bolts</p> <p>\Rightarrow Draw half elevation & support detail</p>	<p>05</p> <p>05</p> <p>05</p> <hr/> <p>15</p>
<p>Q. 4)</p>	<p><u>Load calculation</u></p>  <p>$RA = 339 \text{ kN}$, load on each wheel $\Rightarrow \frac{339}{2} \Rightarrow 169.5 \text{ kN}$</p> <p>consider impact factor of 25%.</p> <p>[\therefore load on each wheel $\Rightarrow 1.25 \times 169.5 \approx 212 \text{ kN}$]</p> <p><u>max. BM</u></p>  <p>$RC \Rightarrow 165.63 \text{ kN}$</p> <p>$M \Rightarrow 517.6 \text{ kNm}$</p> <p>$M_u \Rightarrow 776.4 \text{ kNm}$</p>	<p>05</p>

Question Number	Solution	Marks Allocated
	<p>Man. Shear force \rightarrow </p> <p>$R_L = 331.95 \text{ kN}$</p> <p>\therefore Factored SF $\Rightarrow V_u \Rightarrow 496.88 \text{ kN}$</p>	05
	<p><u>horizontal load & moment</u></p> <p>factored horizontal force $\Rightarrow 10.5 \text{ kN}$ (on each wheel)</p> <p>factored moment $\Rightarrow 25.64 \text{ kNm}$ due to horiz. force</p>	04
	<p>\Rightarrow <u>Transverse deflection</u> Based on max. deflection</p> <p>$\frac{\text{span}}{750} \Rightarrow \frac{8000}{750} \Rightarrow 10.67 \text{ mm}$</p> <p>$\Rightarrow$ calculate actual deflection by moment area method i.e. $\delta = \frac{\text{Area} \times \bar{x}}{EI}$</p> <p>$[I_{x-0.8I_z} \Rightarrow 1.1765 \times 10^9 \text{ mm}^4]$</p> <p>increase above value by 30% $\therefore I_z = 2.29 \times 10^9 \text{ mm}^4$</p>	03
	<p>\Rightarrow choose suitable section from steel table</p> <p>\Rightarrow Check — moment of resistance $\Rightarrow M_d = \beta_b Z_p f_y$</p> <p>2) shear resistance $\Rightarrow V_d = \frac{A_v f_y}{\sqrt{3}}$</p> <p>3) web crippling $\Rightarrow F_w = (b_1 + n_2) t_w f_y$</p> <p>4) web buckling $\Rightarrow (b_1 + n_1) t_w f_y$</p> <p>$\Rightarrow$ connection design \Rightarrow [Weld size = 5mm] reqd</p> <p>sketch \rightarrow CV showing all details \rightarrow side view</p>	04 04 02 02 02

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