

**CBCS Scheme**

15EC36

USN 15EC36

Third Semester B.E. Degree Examination, Dec.2017/Jan.2018

**Engineering Electromagnetics**

Max. Marks: 80

Time: 3 hrs.

Note: Answer any FIVE full questions, choosing one full question from each module.

Important Note - 1. On completing your answers, compulsorily draw diagonal cross lines on the remaining blank pages.  
2. Any revealing of identifications, appeal to evaluate and for equations written (eg.  $42 \times 8 = 50$ ) will be treated as malpractice.

- Module-1** (05 Marks)
- 1 a. State and explain Coulomb's law in vector form. (05 Marks)
  - b. Find the electric field  $\vec{E}$  at origin, if the following charge distributions are present in free space:
    - i) Point charge 12 nC at  $P(2, 0, 6)$ .
    - ii) Uniform line charge of linear charge density  $3 \mu\text{C/m}$  at  $x = 2, y = 3$ . (06 Marks)
    - iii) Uniform surface charge of density  $\rho_s = 0.2 \text{ nC/m}^2$  at  $x = 2$ .
  - c. Define volume charge density. Also find the total charge within each of the indicated volumes.
    - i)  $0 \leq \rho \leq 0.1, 0 \leq \phi \leq \pi, 2 \leq z \leq 4, A = \rho^2 \sin(0.6\phi)$  (05 Marks)
    - ii) Universe:  $\rho_v = \frac{e^{-2r}}{r^2}$  (05 Marks)
- OR** (04 Marks)
- 2 a. Define Electric flux and flux density. (04 Marks)
  - b. Given a 60  $\mu\text{C}$  point charge located at the origin, find the total electric flux passing through:
    - i) That portion of the sphere  $r = 26 \text{ cm}$  bounded by  $\theta = 0, \frac{\pi}{2}$  and  $0 < \phi < \frac{\pi}{2}$ .
    - ii) The closed surface defined by  $\rho = 26 \text{ cm}$  and  $z = \pm 26 \text{ cm}$ .
    - iii) The plane  $z = 26 \text{ cm}$ .
  - c. Derive the expression for  $\vec{E}$  due to infinite line charge of charge density  $\rho_L \text{ (C/m)}$ . (05 Marks)
- Module-2**
- 3 a. State and prove Gauss law for point charge. (05 Marks)
  - b. State and prove divergence theorem. (05 Marks)
  - c. In each of the following parts, find value for  $\text{div } \vec{D}$  at the point specified:
    - i)  $\vec{D} = (2xyz - y^2)\vec{a}_x + (x^2z - 2xy)\vec{a}_y + x^2y\vec{a}_z, \text{ C/m}^2$  at  $P_1(2, 3, -1)$ .
    - ii)  $\vec{D} = 2\rho z^2 \sin^2 \phi \vec{a}_\rho + \rho z^2 \sin 2\phi \vec{a}_\phi + 2\rho^2 z \sin^2 \phi \vec{a}_z, \text{ C/m}^2$  at  $P_2(\rho = 2, \phi = 110^\circ, z = -1)$ . (06 Marks)
- OR**
- 4 a. Define potential difference and absolute potential. (04 Marks)
  - b. A point charge of 6 nC is located at origin in free space, find potential of point p, if p is located at  $(0.2, -0.4, 0.4)$  and
    - i)  $V = 0$  at infinity
    - ii)  $V = 0$  at  $(1, 0, 0)$
    - iii)  $V = 20 \text{ V}$  at  $(-0.5, 1, -1)$
  - c. Derive point form of continuity equation for current. (06 Marks)

1 of 2

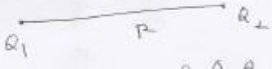
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- Module-3** (05 Marks)
- 5 a. Derive the expression for Poisson's and Laplace's equation. (05 Marks)
  - b. Two plates of parallel plate capacitors are separated by distance 'd' and maintained at potential zero and  $V_0$  respectively. Assuming negligible fringing effect, determine potential at any point between the plates. (06 Marks)
  - c. State and prove uniqueness theorem. (05 Marks)
- OR**
- 6 a. State and explain Biot-Savart law. (06 Marks)
  - b. Find the magnetic flux density at the centre 'O' of a square of sides equal to 5m and carrying 10 amperes of current. (06 Marks)
  - c. At a point  $P(x, y, z)$ , the components of vector magnetic potential  $\vec{A}$  are given as  $A_x = 4x + 3y + 2z, A_y = 5x + 6y + 3z$  and  $A_z = 2x + 3y + 5z$ . Determine  $\vec{B}$  at point P. (04 Marks)
- Module-4**
- 7 a. Derive Lorentz force equation. (05 Marks)
  - b. Derive an expression for the force on a differential current element placed in a magnetic field. (06 Marks)
  - c. A conductor 4m long lies along the y-axis with a current of 10 amps in the  $\vec{a}_y$  direction. Find the force on the conductor if the field is  $\vec{B} = 0.005 \vec{a}_x$  Tesla. (05 Marks)
- OR**
- 8 a. Define: i) Magnetization, ii) Permeability. (04 Marks)
  - b. Find the magnetization in a magnetic material where
    - i)  $\mu = 1.8 \times 10^2 \text{ (H/m)}$  and  $120 \text{ (A/m)}$
    - ii)  $\mu_r = 22$ , there are  $8.2 \times 10^{23}$  atoms/m<sup>3</sup> and each atom has a dipole moment of  $4.5 \times 10^{-27} \text{ (A/m}^2\text{)}$  and
    - iii)  $B = 300 \mu\text{T}$  and  $\chi_m = 46$ . (06 Marks)
  - c. Discuss the boundary conditions at the interface between two media of different permeabilities. (06 Marks)
- Module-5**
- 9 a. State and explain Faraday's law of electromagnetic induction. (04 Marks)
  - b. Find the frequency at which conduction current density and displacement current are equal in a medium with  $\sigma = 2 \times 10^{-4} \text{ U/m}$  and  $\epsilon_r = 81$ . (06 Marks)
  - c. List Maxwell's equations in point form and integral form. (06 Marks)
- OR**
- 10 a. Obtain solution of the wave equation for a uniform plane wave in free space. (06 Marks)
  - b. State and prove Poynting theorem. (06 Marks)
  - c. The depth of penetration in a certain conducting medium is 0.1 m and the frequency of the electromagnetic wave is 1.0 MHz. Find the conductivity of the conducting medium. (04 Marks)

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1.(a) State and explain Coulomb's law in vector form. Express the result in Cartesian coordinates.

Soln The force b/w two very small charged objects separated in vacuum or free space by a distance which is large compared to their size is proportional to the charge on each and inversely proportional to the square of the dist. b/w them.



$$F = \frac{k Q_1 Q_2}{R^2}$$

$Q_1$  &  $Q_2 \rightarrow$  +ve or -ve quantities of charge  
unit Coulomb (C)

$R \rightarrow$  separation in m.

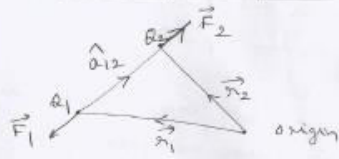
$k \rightarrow$  constant of proportionality.

$k = \frac{1}{4\pi\epsilon_0}$   
where,  $\epsilon_0 \rightarrow$  permittivity of free space.

$\epsilon_0 = 8.854 \times 10^{-12} \text{ F/m}$   
 $= \frac{1}{36\pi} \times 10^{-9} \text{ F/m}$

$F \rightarrow$  force in Newton.

1.(a) Vector form of Coulomb's law



$\vec{r}_1 \rightarrow$  locates  $Q_1$

$\vec{r}_2 \rightarrow$  locates  $Q_2$

$Q_1, Q_2$  of same sign,  $F_2$  in the direction as indicated.

$F_2 \rightarrow$  force exerted on  $Q_2$  by  $Q_1$ .

$\hat{a}_{12} \rightarrow$  unit vector along  $\vec{R}_{12}$ .

Then, the vector form of Coulomb's law is,

$$\vec{F}_2 = \frac{Q_1 Q_2}{4\pi\epsilon_0 R_{12}^2} \hat{a}_{12}$$

where,  $\hat{a}_{12} = \frac{\vec{R}_{12}}{|\vec{R}_{12}|} = \frac{\vec{r}_2 - \vec{r}_1}{|\vec{r}_2 - \vec{r}_1|}$

$|\vec{R}_{12}| = R =$  distance b/w the two charges.

Let,  $\vec{F}_1$  be the force exerted by  $Q_1$  on  $Q_2$ .

$$\vec{r}_1 = \vec{r}_2 + \vec{R}_{21}$$

$$\Rightarrow \vec{R}_{21} = \vec{r}_1 - \vec{r}_2 = -(\vec{r}_2 - \vec{r}_1)$$

$$\therefore \hat{a}_{12} = -\hat{a}_{21}$$

1.(a)  $\therefore F_1 = \frac{Q_1 Q_2}{4\pi\epsilon_0 R_{21}^2} (-\hat{a}_{21}) = -\vec{F}_2$

$\Rightarrow$  Coulomb's law is a mutual force.

Important observations:

- i) charges should be point charges and stationary in nature.
- ii) should consider the signs of the charges to decide whether the force will be attractive or repulsive.

iii) Coulomb's law is linear.

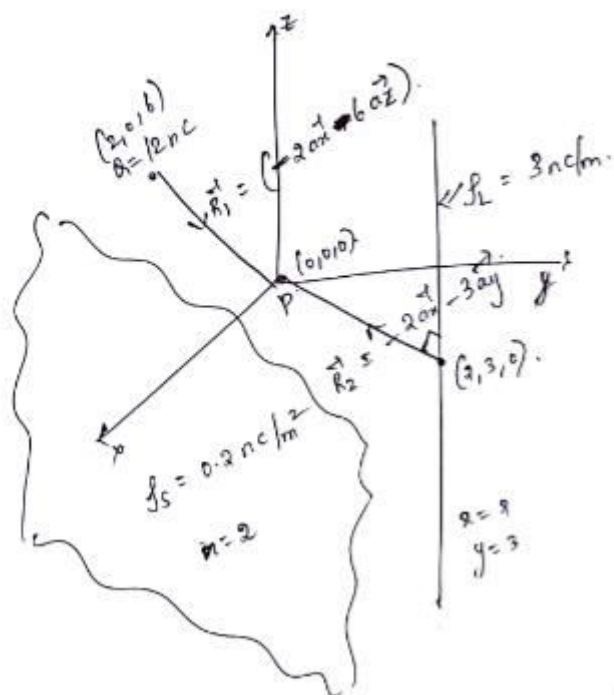
i.e. if  $\vec{F}_2 = -\vec{F}_1$

then,  $n\vec{F}_2 = -n\vec{F}_1$

where  $n$  is a scalar.

iv) Force on a charge in the presence of several other charges is the sum of the forces on that charge due to each of the other charges acting alone.

1(b)



$$\vec{E} = \vec{E}_p + \vec{E}_L + \vec{E}_s = \frac{q}{4\pi\epsilon_0 |\vec{R}_1|^3} \vec{R}_1 + \frac{\lambda_L}{2\pi\epsilon_0 |\vec{R}_2|^2} \vec{R}_2 + \frac{\lambda_s}{2\epsilon_0} \vec{a}_n$$

$$\vec{E} = \frac{12 \times 10^{-9} \times 9 \times 10^9 \times (-2\vec{a}_x - 3\vec{a}_z)}{(\sqrt{4+36})^3} + \frac{3 \times 10^{-9} \times 18 \times 10^9 \times (-2\vec{a}_x - 3\vec{a}_y)}{(\sqrt{4+9})^2} + \frac{0.2 \times 10^{-9} \times 36\pi \times 10^9}{2} (-\vec{a}_n)$$

$$\vec{E} = -20.4545 \vec{a}_x - 12.46 \vec{a}_y - 2.56 \vec{a}_z \text{ V/m}$$

1.(c) (i)

$$\begin{aligned}
 Q_{enc} &= \iiint_V \rho_V dv = \int_{z=2}^4 \int_{\phi=0}^{\pi} \int_{\rho=0}^{0.1} \rho^2 z \sin 0.6\phi \rho d\rho d\phi dz \\
 &= \int_0^{0.1} \rho^3 d\rho \times \int_0^{\pi} \sin 0.6\phi d\phi \times \int_2^4 z^2 dz \\
 &= \left[ \frac{\rho^4}{4} \right]_0^{0.1} \left[ -\frac{\cos 0.6\phi}{0.6} \right]_0^{\pi} \times \left[ \frac{z^3}{3} \right]_2^4 \\
 &= \frac{(0.1)^4}{4} \times \left[ \frac{0.309}{0.6} + \frac{1}{0.6} \right] \times \left[ \frac{1}{3} (4^3 - 2^3) \right]
 \end{aligned}$$

$$Q_{enc} = 1.018 \text{ mC}$$

$$\begin{aligned}
 Q_{enc} &= \iiint_V \rho_V dv \\
 &= \int_{\phi=0}^{2\pi} \int_{\theta=0}^{\pi} \int_{r=0}^{\infty} \frac{e^{-2r}}{r^2} r^2 \sin\theta dr d\theta d\phi \\
 &= \int_0^{\infty} e^{-2r} dr \times \int_0^{\pi} \sin\theta d\theta \times \int_0^{2\pi} d\phi \\
 &= \left[ \frac{e^{-2r}}{-2} \right]_0^{\infty} \left[ -\cos\theta \right]_0^{\pi} \left[ \phi \right]_0^{2\pi} \\
 &= -\frac{1}{2} (0 - 1) \times (1 - 1) \times 2\pi
 \end{aligned}$$

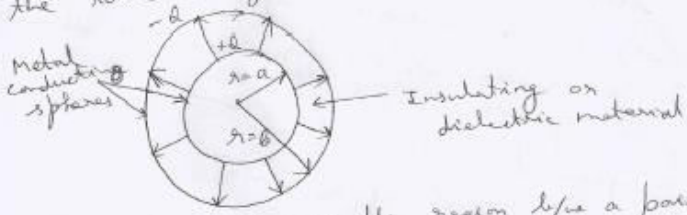
$$= 2\pi$$

$$Q_{enc} = 6.28 \text{ C}$$

2.(a)

Soln.

Gauss's law states that the electric flux passing through any closed surface is equal to the total charge enclosed by that surface.



The electric flux in the region b/w a pair of charged concentric spheres. The direction and mag. of  $D$  are not functions of the dielectric b/w the spheres.

The mathematical form of Gauss's law is,

$$\Psi = \oint \vec{D}_s \cdot d\vec{s} - \text{charge enclosed} = Q.$$

where,  $Q = \int_{\text{vol}} \rho_s \, dv.$

$\Psi \rightarrow$  total flux passing through the closed surface.

The direction of  $D$  at a pt. is the direction of the flux lines at that point, and the mag. is given by the no. of flux lines crossing a surface normal to the lines divided by the surface area.

$$\therefore \vec{D} \Big|_{r=a} = \frac{Q}{4\pi a^2} \hat{a}_r \quad (\text{inner sphere})$$

$$\vec{D} \Big|_{r=b} = \frac{-Q}{4\pi b^2} \hat{a}_r \quad (\text{outer sphere}).$$

$$a \leq r \leq b$$

$$\vec{D} = \frac{Q}{4\pi r^2} \hat{a}_r.$$

Small inner sphere, smaller and smaller, we reach point charge.

$$\vec{D} = \frac{Q}{4\pi r^2} \hat{a}_r.$$

$Q$  lines of flux are symmetrically directed outward from the pt. and pass through an imaginary spherical surface of area  $4\pi r^2$ .

$$\vec{E} = \frac{Q}{4\pi \epsilon_0 r^2} \hat{a}_r.$$

$$\therefore \boxed{D = \epsilon_0 E} \rightarrow \text{free space.}$$

2.(b)

Solution

Flux = flux density  $\times$  surface area

$$\Psi = \vec{D} \cdot \text{Surface area}$$

at  $r=26\text{cm}$ ,  $\vec{D} = \frac{q}{4\pi r^2} \cdot \vec{a}_r$

$$\vec{D} = \frac{60\mu\text{C}}{4\pi \cdot (26 \times 10^{-2})^2} \cdot \vec{a}_r$$

Surface area,  $\vec{S} = \iint d\vec{S} = \int_{\phi=0}^{2\pi} \int_{\theta=0}^{\pi/2} r^2 \sin\theta \, d\theta \, d\phi \cdot \vec{a}_r$

$$= (26 \times 10^{-2})^2 \times \left[ -\cos\theta \right]_0^{\pi/2} \cdot \pi/2 \cdot \vec{a}_r$$

$$\vec{S} = (0.26)^2 \times \pi/2 \cdot \vec{a}_r$$

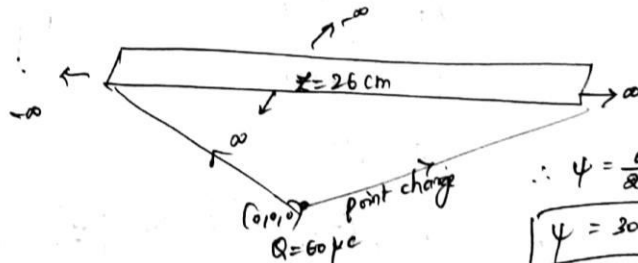
$$\Psi = \frac{60\mu\text{C}}{4\pi \times (0.26)^2} \cdot (0.26)^2 \times \pi/2$$

$$\boxed{\Psi = 7.5\mu\text{C}}$$

b) closed surface  $\Rightarrow$  total flux =  $q_{enc}$

$$\Psi = 60\mu\text{C}$$

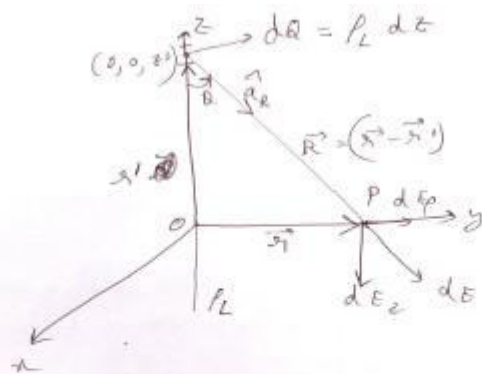
c) plane  $x=26\text{cm}$



$$\therefore \Psi = \frac{q}{2}$$

$$\boxed{\Psi = 30\mu\text{C}}$$

2.(c)



- consider a general point  $P(0, y, 0)$  on the  $y$ -axis to determine the field.

- we consider incremental charge,  $dQ = \rho_L dz'$ .

- Aim to find incremental field.

$$\therefore d\vec{E} = \frac{\rho_L dz' (\vec{x} - \vec{x}')}{4\pi\epsilon_0 |\vec{x} - \vec{x}'|^3}$$

where,  $\vec{x} = y\hat{a}_y = p\hat{a}_p$   
 $\vec{x}' = z'\hat{a}_z$

$$\therefore \vec{x} - \vec{x}' = (p\hat{a}_p - z'\hat{a}_z)$$

$$\therefore d\vec{E} = \frac{\rho_L dz' (p\hat{a}_p - z'\hat{a}_z)}{4\pi\epsilon_0 (p^2 + z'^2)^{3/2}}$$

we know only  $p$  component is present.

$$dE_p = \int_{-\infty}^{\infty} \frac{\rho_L p dz'}{4\pi\epsilon_0 (p^2 + z'^2)^{3/2}}$$



$$E_p = \int_{-\infty}^{\infty} \frac{\rho_L \rho dz'}{4\pi\epsilon_0 (r^2 + z'^2)^{3/2}}$$

Let,  $z' = \rho \cot \theta$   
 $\therefore dz' = -\rho \operatorname{cosec}^2 \theta d\theta$

At  $z' = \rho \frac{\cos \theta}{\sin \theta}$   
 $\infty = \frac{\cos 0}{\sin 0} \Rightarrow \text{for } z' = \infty, \theta = 0^\circ$   
 $z' = -\frac{\cos(\pi)}{\sin(\pi)} \Rightarrow z' = -\infty, \theta = \pi$

$$E_p = \frac{\rho_L}{4\pi\epsilon_0} \int_{\pi}^0 \frac{\rho \cdot (-\rho \operatorname{cosec}^2 \theta d\theta)}{(r^2 + \rho^2 \cot^2 \theta)^{3/2}}$$

$$= \frac{\rho_L}{4\pi\epsilon_0} \int_{\pi}^0 \frac{-\rho^2 \operatorname{cosec}^2 \theta d\theta}{(\rho^2/2 + \rho^2 \cot^2 \theta)^{3/2}}$$

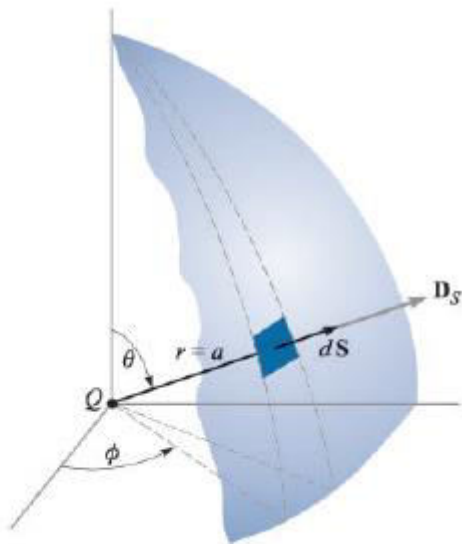
$$= \frac{\rho_L}{4\pi\epsilon_0 \rho} \int_{\pi}^0 \frac{-\operatorname{cosec}^2 \theta d\theta}{\operatorname{cosec}^3 \theta}$$

$$= \frac{\rho_L}{4\pi\epsilon_0 \rho} \int_{\pi}^0 -\sin \theta d\theta = \frac{\rho_L}{4\pi\epsilon_0 \rho} [\cos \theta]_{\pi}^0$$

$$= \frac{\rho_L}{4\pi\epsilon_0 \rho} [1 + 1] = \frac{2\rho_L}{4\pi\epsilon_0 \rho}$$

$$= \frac{\rho_L}{2\pi\epsilon_0 \rho}$$

3.(a)



Let us place a point charge  $Q$  at the origin of a spherical co-ordinate system.

Let the closed surface be a sphere of radius  $a$ .

The electric field intensity of the point charge,

$$\vec{E} = \frac{Q}{4\pi\epsilon_0 r^2} \hat{a}_r$$

Now,  $\vec{D} = \epsilon_0 \vec{E}$ .

$$\therefore \vec{D} = \frac{Q}{4\pi r^2} \hat{a}_r$$

At the surface of the sphere,

$$\vec{D}_s = \frac{Q}{4\pi a^2} \hat{a}_r$$

The differential area element in spherical co-ordinates,

$$ds = r^2 \sin\theta \, d\theta \, d\phi = a^2 \sin\theta \, d\theta \, d\phi$$

$$\text{or } \vec{ds} = a^2 \sin\theta \, d\theta \, d\phi \, \hat{a}_s$$

The integrand is,

$$\vec{D}_s \cdot \vec{ds} = \frac{Q}{4\pi a^2} \cdot a^2 \sin\theta \, d\theta \, d\phi \, \hat{a}_s \cdot \hat{a}_s$$

$$= \frac{Q}{4\pi} \sin\theta \, d\theta \, d\phi$$

∴

total is chosen

$$\therefore \int_{\phi=0}^{2\pi} \int_{\theta=0}^{\pi} \frac{Q}{4\pi} (-\cos\theta) \Big|_0^{\pi} d\theta \, d\phi$$

$$= \int_0^{2\pi} \frac{Q}{4\pi} (+1+1) d\phi$$

$$= \frac{Q}{2\pi} \cdot 2\pi = Q$$

∴ we obtain the result that  $Q$  coulombs of electric flux are crossing the surface, as we should since the enclosed charge is  $Q$  coulombs.

3.(b)

Divergence theorem: (For electric flux density).

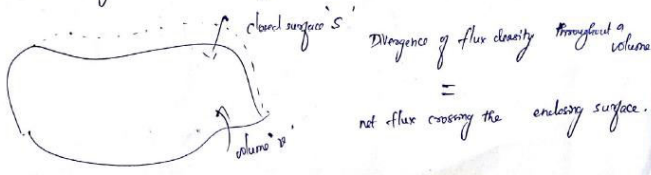
Gauss' law:

$$\oint_S \vec{D} \cdot d\vec{s} = Q \quad = \int_V \rho_v dV.$$

$$\boxed{\oint_S \vec{D} \cdot d\vec{s} = \int_V \nabla \cdot \vec{D} dV} \quad \leftarrow \text{Divergence theorem.}$$

Statement:

The integral of the normal component of any vector field over a closed surface is equal to the integral of the divergence of that vector field throughout the volume enclosed by the closed surface.



Differential Volume element:

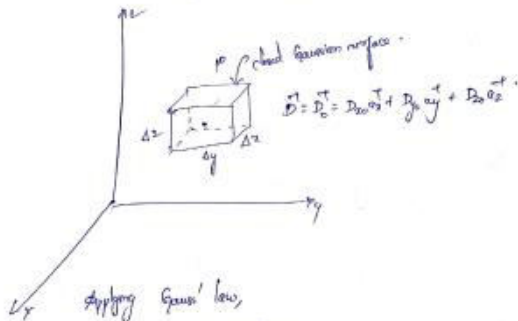
No symmetry.

Choose a small gaussian surface  $\rightarrow$  about  $\vec{D}$  is constant over that surface.

Result becomes correct only when volume  $dV \rightarrow 0$  (shrinks).

We will not obtain  $\vec{D}$ , obtain the valuable information about the way  $\vec{D}$  varies in the region.

$\Downarrow$   
one of Maxwell's four equations (base to all electromagnetic theory)



Applying Gauss' law,

$$\oint_S \vec{D} \cdot d\vec{s} = Q$$

$$\int_{\text{front}} + \int_{\text{back}} + \int_{\text{left}} + \int_{\text{right}} + \int_{\text{top}} + \int_{\text{bottom}} \vec{D} \cdot d\vec{s} = Q$$

Surface element is very small  $\rightarrow \vec{D}$  is constant over the surface.

$$\begin{aligned} \int_{\text{front}} \vec{D} \cdot d\vec{s} &= D_{x, \text{front}} \cdot \Delta s_{\text{front}} \\ &= D_{x, \text{front}} \cdot \Delta y \Delta z \\ &= D_{x, \text{front}} \cdot \Delta y \Delta z \end{aligned}$$

find face  $\rightarrow$  distance of  $\frac{\Delta z}{2}$  from P.

$$D_{n, \text{front}} = D_{z0} + \frac{\Delta z}{2} \cdot \frac{\partial D_z}{\partial z}$$

value of  $D_z$  at P.

Rate of change of  $D_z$  w.r.t  $z$   
 $\therefore \frac{\partial D_z}{\partial z}$  same with  $y \neq z$ .

Expanding Taylor series

$$\int_{\text{front}} = \left( D_{z0} + \frac{\Delta z}{2} \frac{\partial D_z}{\partial z} \right) dy dz$$

Integral over the back surface

$$\int_{\text{back}} = -D_{z, \text{back}} \cdot d\vec{\sigma}_{\text{back}}$$

$$= -D_{z, \text{back}} \cdot (-dy dz \hat{z})$$

$$\int_{\text{back}} = -D_{z, \text{back}} dy dz$$

$$= -\left[ D_{z0} + \left( -\frac{\Delta z}{2} \right) \frac{\partial D_z}{\partial z} \right] dy dz$$

$$\int_{\text{back}} = \left( -D_{z0} + \frac{\Delta z}{2} \frac{\partial D_z}{\partial z} \right) dy dz$$

$$\int_{\text{front}} + \int_{\text{back}} = \frac{\partial D_z}{\partial z} \Delta z dy dz$$

Analogous in the same way

$$\int_{\text{right}} + \int_{\text{left}} = \frac{\partial D_y}{\partial y} \Delta x dy dz$$

$$\int_{\text{top}} + \int_{\text{bottom}} = \frac{\partial D_x}{\partial x} \Delta x dy dz$$

$$\therefore \oint_{\partial V} \vec{D} \cdot d\vec{\sigma} = \frac{\partial D_x}{\partial x} \Delta x dy dz + \frac{\partial D_y}{\partial y} \Delta x dy dz + \frac{\partial D_z}{\partial z} \Delta x dy dz \quad (2)$$

$$\oint_{\partial V} \vec{D} \cdot d\vec{\sigma} = \left( \frac{\partial D_x}{\partial x} + \frac{\partial D_y}{\partial y} + \frac{\partial D_z}{\partial z} \right) \Delta x dy dz = Q$$

$\vec{D}$  is an approximation which is better when  $\Delta V$  becomes smaller.

$$\therefore \Delta V \rightarrow 0 \quad \text{where } \Delta V = \Delta x dy dz$$

$$\text{Charge enclosed in volume } \Delta V = \left( \frac{\partial D_x}{\partial x} + \frac{\partial D_y}{\partial y} + \frac{\partial D_z}{\partial z} \right) \cdot \Delta V$$

We now obtain the exact relationship by  $\Delta V \rightarrow 0$ .

$$\left( \frac{\partial m_x}{\partial x} + \frac{\partial m_y}{\partial y} + \frac{\partial m_z}{\partial z} \right) = \frac{\oint \vec{D} \cdot d\vec{s}}{\Delta V} = \frac{q}{\Delta V}$$

$$\left( \frac{\partial m_x}{\partial x} + \frac{\partial m_y}{\partial y} + \frac{\partial m_z}{\partial z} \right) = \lim_{\Delta V \rightarrow 0} \frac{\oint \vec{D} \cdot d\vec{s}}{\Delta V} = \left( \lim_{\Delta V \rightarrow 0} \frac{q}{\Delta V} \right) \rightarrow \text{volume charge density}$$

$$\boxed{\frac{\partial m_x}{\partial x} + \frac{\partial m_y}{\partial y} + \frac{\partial m_z}{\partial z} = \lim_{\Delta V \rightarrow 0} \frac{\oint \vec{D} \cdot d\vec{s}}{\Delta V} \rightarrow (1)}$$

$$\boxed{\frac{\partial D_x}{\partial x} + \frac{\partial D_y}{\partial y} + \frac{\partial D_z}{\partial z} = \rho_v \rightarrow (2)}$$

$$\text{Divergence of } \vec{D} = \text{div } \vec{D} = \lim_{\Delta V \rightarrow 0} \frac{\oint \vec{D} \cdot d\vec{s}}{\Delta V}$$

Divergence of the vector flux density  $\vec{D}$  is the outflow of flux from a small closed surface per unit volume as the volume shrinks to zero.

$$\boxed{\text{div } \vec{D} = \frac{\partial D_x}{\partial x} + \frac{\partial D_y}{\partial y} + \frac{\partial D_z}{\partial z} \quad \text{Rectangular}}$$

$$\boxed{\text{div } \vec{D} = \frac{1}{\rho} \frac{\partial (\rho D_\rho)}{\partial \rho} + \frac{1}{\rho} \frac{\partial D_\phi}{\partial \phi} + \frac{\partial D_z}{\partial z} \quad \text{cylindrical}}$$

$$\boxed{\text{div } \vec{D} = \frac{1}{r^2} \frac{\partial (r^2 D_r)}{\partial r} + \frac{1}{r \sin \theta} \frac{\partial (\sin \theta D_\theta)}{\partial \theta} + \frac{1}{r \sin \theta} \frac{\partial D_\phi}{\partial \phi} \quad \text{spherical}}$$

### MAXWELL'S FIRST EQUATION OF ELECTROSTATICS:

$$1) \text{div } \vec{D} = \lim_{\Delta V \rightarrow 0} \frac{\oint \vec{D} \cdot d\vec{s}}{\Delta V} \quad (\text{definition of divergence})$$

$$2) \text{div } \vec{D} = \frac{\partial D_x}{\partial x} + \frac{\partial D_y}{\partial y} + \frac{\partial D_z}{\partial z} \quad (\text{Result of applying the definition to a differential volume element in Rectangular co-ordinates})$$

$$3) \text{div } \vec{D} = \rho_v$$

Gauss's law  $\rightarrow$  flux leaving any closed surface

$$\boxed{\oint_S \vec{D} \cdot d\vec{s} = Q} \quad \leftarrow \text{charge enclosed}$$

Gauss law per unit volume,

$$\frac{\oint_S \vec{D} \cdot d\vec{s}}{\Delta V} = \frac{q}{\Delta V}$$

As the volume shrinks to zero,

$$\lim_{\Delta V \rightarrow 0} \frac{\oint \vec{D} \cdot d\vec{s}}{\Delta V} = \lim_{\Delta V \rightarrow 0} \frac{Q}{\Delta V}$$

divergence

volume charge density

$$\text{div } \vec{D} = \rho_v$$

First of Maxwell's four equations

Statement:

The electric flux per unit volume leaving a vanishingly small volume unit is exactly equal to the volume charge density there.

Point form of Gauss's law  
Maxwell's 1st equation

$$\text{Gauss's law} \rightarrow \oint_S \vec{D} \cdot d\vec{s} = Q = \int_V \rho_v \cdot dV$$

Integral form of Maxwell's first equation

3.(c)

3(c) Find  $\text{div } \vec{D}$ .

i)  $\vec{D} = (2xyz - y^2)\vec{a}_x + (x^2z - 2xy)\vec{a}_y + x^2y\vec{a}_z \text{ C/m}^2$   
at  $P_A (2, 3, -1)$

$$\vec{\nabla} \cdot \vec{D} = \frac{\partial}{\partial x}(2xyz - y^2) + \frac{\partial}{\partial y}(x^2z - 2xy) + \frac{\partial}{\partial z}(x^2y)$$

$$\vec{\nabla} \cdot \vec{D} = 2yz - 2x + 0$$

$$\vec{\nabla} \cdot \vec{D} = 2yz - 2x \text{ C/m}^3$$

$$\vec{\nabla} \cdot \vec{D} \text{ at } P_A (2, 3, -1) = 2(3)(-1) - 2(2) = -6 - 4$$

$$\vec{\nabla} \cdot \vec{D} = -10 \text{ C/m}^3$$

$$(iii) \vec{D} = \rho_f z^2 \sin^2 \phi \vec{a}_\rho + f z^2 \sin 2\phi \vec{a}_\phi + 2f^2 z \sin^2 \phi \vec{a}_z \text{ C/m} \\ \text{at } P_B(\rho=2, \phi=110^\circ, z=-1)$$

$$\vec{\nabla} \cdot \vec{D} = \frac{1}{\rho} \frac{\partial}{\partial \rho} (\rho \cdot \rho_f z^2 \sin^2 \phi) + \frac{1}{\rho} \frac{\partial}{\partial \phi} (f z^2 \sin 2\phi) \\ + \frac{\partial}{\partial z} (2f^2 z \sin^2 \phi)$$

$$= \frac{1}{\rho} \cdot \frac{\partial}{\partial \rho} (\rho_f^2 z^2 \sin^2 \phi) + \frac{1}{\rho} \frac{\partial}{\partial \phi} (f z^2 \sin 2\phi) \\ + \frac{\partial}{\partial z} (2f^2 z \sin^2 \phi)$$

$$= \frac{1}{\rho} \cdot \frac{\partial}{\partial \rho} (4f^2 z^2 \sin^2 \phi) + \frac{1}{\rho} \cdot f z^2 \cdot \cos 2\phi \cdot 2 \\ + 2f^2 \sin^2 \phi$$

$$\vec{\nabla} \cdot \vec{D} = 4z^2 \sin^2 \phi + 2z^2 \cos 2\phi + 2f^2 \sin^2 \phi \text{ C/m}^3$$

$$\vec{\nabla} \cdot \vec{D} \text{ at } P_B(2, 110^\circ, -1)$$

$$= 4(-1)^2 \sin^2(110^\circ) + 2(-1)^2 \cos(2 \times 110^\circ) + 2(2)^2 \sin^2(110^\circ)$$

$$= 3.532 + (-1.532) + \frac{7.0641}{\cancel{4.00000}}$$

$$\vec{\nabla} \cdot \vec{D} = 9.0641 \text{ C/m}^3$$



4.(a)

Potential Difference: Potential difference  $V$  is defined as the work done (by an external source) in moving a unit +ve charge from one point to another in an electric field.

$$\text{Potential difference} = V = - \int_{\text{init}}^{\text{final}} \vec{E} \cdot d\vec{l}$$

$V_{AB}$  → potential diff. b/w points A and B and is the work done in moving a unit charge from B to A.

Unit of potential difference: Joules/coulomb, commonly Volt.

Absolute potential:

The absolute potential of a point is defined as the work done in moving a unit +ve charge from infinity to that point.

The potential diff. b/w two points located at  $r = r_A$  and  $r = r_B$  in the field of a point charge  $Q$  placed at the origin.

$$V_{AB} = \frac{Q}{4\pi\epsilon_0} \left( \frac{1}{r_A} - \frac{1}{r_B} \right) = V_A - V_B$$

$V = 0$  at infinity. We let,  $r = r_B$  recede to infinity.

∴ The potential at  $r_A$  becomes,  $V_A = \frac{Q}{4\pi\epsilon_0 r_A}$

∴ This expression defines the potential at any



4) b) A point charge of  $6nC$  is located at origin in free space. Find the potential of point  $P$ , if  $P$  is located at  $(0.2, -0.4, 0.4)$  and.

(i)  $V = 0$  at infinity

(ii)  $V = 0$  at  $(1, 0, 0)$

(iii)  $V = 20V$  at  $(-0.5, 1, -1)$ .

$$V = \frac{q}{4\pi\epsilon_0 |\vec{R}|}$$

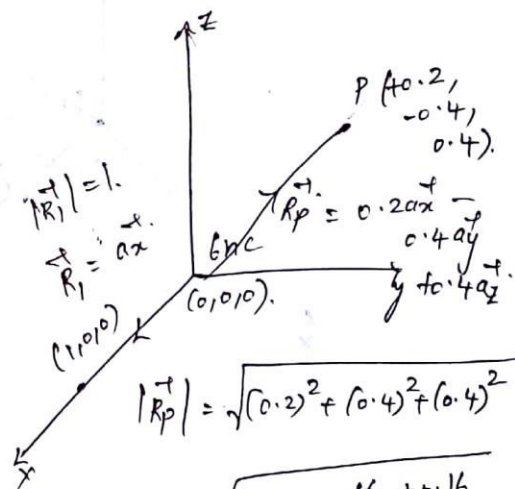
$$V_{AB} = \frac{q}{4\pi\epsilon_0 |\vec{R}_A|} - \frac{q}{4\pi\epsilon_0 |\vec{R}_B|}$$

$$\begin{aligned} \text{(i)} \quad V_{P\infty} &= V_P - V_\infty \\ &= \frac{q}{4\pi\epsilon_0 |\vec{R}_P|} - V_\infty \end{aligned}$$

$$= \frac{6 \times 10^{-9} \times 9 \times 10^9}{0.6} - \frac{1}{\infty} = 90$$

$$V_{P\infty} = 90 \text{ V}$$

$$\boxed{V_P = 90 \text{ V}}$$



$$\begin{aligned} |\vec{R}_P| &= \sqrt{(0.2)^2 + (-0.4)^2 + (0.4)^2} \\ &= \sqrt{0.04 + 0.16 + 0.16} \end{aligned}$$

$$|\vec{R}_P| = 0.6$$

$$\text{(ii)} \quad V_{P1} = \frac{q}{4\pi\epsilon_0} \left[ \frac{1}{|\vec{R}_P|} - \frac{1}{|\vec{R}_1|} \right]$$

$$= 9 \times 10^9 \times 6 \times 10^{-9} \left[ \frac{1}{0.6} - \frac{1}{1} \right]$$

$$= 9 \times 6 \times \left[ \frac{4}{6} - 1 \right] = 9 \times 6 \times \left[ \frac{4}{6} - 1 \right] \quad \boxed{V_{P1} = 36 \text{ V}}$$

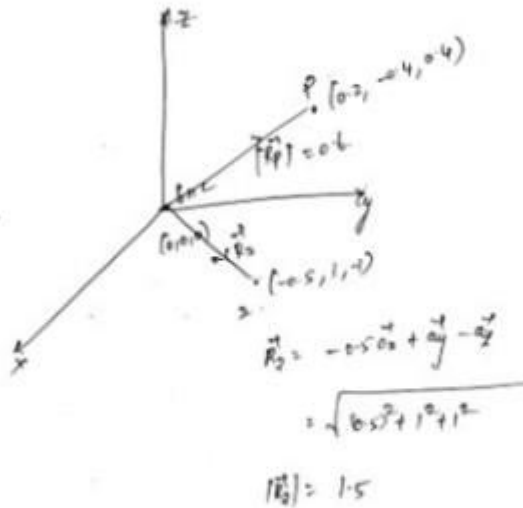
$$V_{P1} = V_P - V_1$$

$$V_P = V_{P1} + V_1$$

$$= 36 + 0$$

$$\boxed{V_P = 36V}$$

(ii)



$$V_{P2} = V_P - V_2$$

$$= \frac{q}{4\pi\epsilon_0 |\vec{r}_{P1}|} - \frac{q}{4\pi\epsilon_0 |\vec{r}_2|}$$

$$= 6 \times 10^{-9} \times 9 \times 10^9 \times \left[ \frac{1}{0.6} - \frac{1}{1.5} \right]$$

$$= 6 \times 10^9 \times \left[ \frac{10}{6} - \frac{10}{15} \right] = 6 \times 10^9 \times \left[ \frac{5-2}{3} \right] = 6 \times 10^9 \times \left[ \frac{3}{3} \right]$$

$$\boxed{V_{P2} = 54V}$$

$$V_2 = 20V$$

$$\therefore V_P = V_{P2} + V_2$$

$$\boxed{V_P = 74V}$$

4. (c)

sol.

Current through a closed surface,

$$I = \oint \vec{J} \cdot d\vec{a}$$

Outward flow of +ve charge is balance by a decrease of +ve charge within the closed surface.

Let,  $Q_1$  be the charge inside the closed surface

$$\therefore I = \oint \vec{J} \cdot d\vec{a} = -\frac{dQ_1}{dt} \rightarrow \text{reduction in charge, giving -ve sign.}$$

Using divergence theorem,

$$\oint \vec{J} \cdot d\vec{a} = \int_{\text{vol}} (\nabla \cdot \vec{J}) dV$$

$$\text{Now, } Q = \int_{\text{vol}} \rho_0 dV$$

$$\therefore \int_{\text{vol}} (\nabla \cdot \vec{J}) dV = -\frac{d}{dt} \int_{\text{vol}} \rho_0 dV$$

If the surface is constant derivative becomes a partial derivative.

$$\therefore \int_{\text{vol}} (\nabla \cdot \vec{J}) dV = \int_{\text{vol}} -\frac{\partial \rho_0}{\partial t} dV$$

This is true for any value however small.  
This is true for an incremental volume.

$$\therefore (\nabla \cdot \vec{J}) dV = -\frac{\partial \rho_0}{\partial t} dV$$

$\therefore$  Point form of continuity equation,

$$\boxed{(\nabla \cdot \vec{J}) = -\frac{\partial \rho_0}{\partial t}}$$

5.(a) Derive the expression for Poisson's and Laplace's equation.

Soln.

From Gauss's law,

$$\vec{\nabla} \cdot \vec{D} = \rho_v$$

$$\vec{D} = \epsilon \vec{E}$$

$$\text{and } \vec{E} = -\vec{\nabla} V$$

$$\therefore \vec{\nabla} \cdot \vec{D} = \vec{\nabla} \cdot (\epsilon \vec{E}) = -\vec{\nabla} \cdot (\epsilon \vec{\nabla} V) = \rho_v$$

$$\Rightarrow -\vec{\nabla} \cdot (\vec{\nabla} V) = \frac{\rho_v}{\epsilon}$$

$$\Rightarrow \vec{\nabla} \cdot (\vec{\nabla} V) = \frac{-\rho_v}{\epsilon}$$

$$\Rightarrow \nabla^2 V = \frac{-\rho_v}{\epsilon}$$

$$\boxed{\nabla^2 V = \frac{-\rho_v}{\epsilon}} \rightarrow \text{Poisson's equation}$$

$$\text{Now, } \vec{\nabla} \cdot \vec{A} = \left( \hat{a}_x \frac{\partial}{\partial x} + \hat{a}_y \frac{\partial}{\partial y} + \hat{a}_z \frac{\partial}{\partial z} \right) \cdot (A_x \hat{a}_x + A_y \hat{a}_y + A_z \hat{a}_z)$$

$$= \frac{\partial A_x}{\partial x} + \frac{\partial A_y}{\partial y} + \frac{\partial A_z}{\partial z}$$

$$\vec{\nabla} V = \frac{\partial V}{\partial x} \hat{a}_x + \frac{\partial V}{\partial y} \hat{a}_y + \frac{\partial V}{\partial z} \hat{a}_z$$

$$\vec{\nabla} \cdot \vec{\nabla} V = \frac{\partial}{\partial x} \left( \frac{\partial V}{\partial x} \right) + \frac{\partial}{\partial y} \left( \frac{\partial V}{\partial y} \right) + \frac{\partial}{\partial z} \left( \frac{\partial V}{\partial z} \right)$$

$$= \frac{\partial^2 V}{\partial x^2} + \frac{\partial^2 V}{\partial y^2} + \frac{\partial^2 V}{\partial z^2}$$

$$\boxed{\nabla^2 V = \frac{\partial^2 V}{\partial x^2} + \frac{\partial^2 V}{\partial y^2} + \frac{\partial^2 V}{\partial z^2}} \rightarrow \text{rectangular co-ordinates}$$

If  $\rho_v = 0$  then  $\nabla^2 V = 0$

In cylindrical co-ordinates,

$$\nabla^2 V = \frac{1}{\rho} \frac{\partial}{\partial \rho} \left( \rho \frac{\partial V}{\partial \rho} \right) + \frac{1}{\rho^2} \left( \frac{\partial^2 V}{\partial \phi^2} \right) + \frac{\partial^2 V}{\partial z^2}$$

$$\nabla^2 V = \frac{1}{x^2} \frac{\partial}{\partial x} \left( x^2 \frac{\partial V}{\partial x} \right) + \frac{1}{x^2 \sin^2 \theta} \frac{\partial}{\partial \theta} \left( \sin \theta \frac{\partial V}{\partial \theta} \right) + \frac{1}{x^2 \sin^2 \theta} \frac{\partial^2 V}{\partial \phi^2}$$

5.(b)

$$\frac{\partial^2 V}{\partial x^2} = 0$$
$$\frac{d^2 V}{dx^2} = 0$$
$$\Rightarrow \frac{dV}{dx} = A$$
$$\Rightarrow V = Ax + B$$
$$V = V_1 \text{ at } x = x_1$$
$$V = V_2 \text{ at } x = x_2$$
$$A = \frac{V_1 - V_2}{x_1 - x_2} \quad B = \frac{V_2 x_1 - V_1 x_2}{x_1 - x_2}$$
$$V = 0 \text{ at } x = 0$$
$$V = V_0 \text{ at } x = d$$
$$\therefore A = B = 0, \quad A = \frac{V_0}{d}$$
$$\therefore V = \frac{V_0 x}{d}$$
$$\therefore \vec{E} = -\frac{V_0}{d} \hat{a}_x$$
$$\vec{D} = \epsilon \vec{E} = -\frac{\epsilon V_0}{d} \hat{a}_x$$
$$D_s = D|_{x=0} = -\frac{\epsilon V_0}{d} \hat{a}_x = \rho_s = 0 \text{ nC}$$
$$Q = -\int \frac{\epsilon V_0}{d} d\vec{s} = -\frac{\epsilon V_0 s}{d}$$
$$\Rightarrow c = \frac{|Q|}{V} = \frac{\epsilon s}{d}$$

5.(c) State and prove uniqueness theorem.

$\therefore V_{1b} = V_{2b} = V_b$   
 $\Rightarrow V_{1b} - V_{2b} = 0$   
 considering the vector identity  
 $\vec{\nabla} \cdot (V\vec{B}) = V(\vec{\nabla} \cdot \vec{B}) + \vec{B} \cdot (\vec{\nabla} V)$   
 considering a scalar to be  $(V_1 - V_2)$   
 considering the vector to be  $\vec{\nabla}(V_1 - V_2)$   
 $\vec{\nabla} \cdot [(V_1 - V_2)\vec{\nabla}(V_1 - V_2)] = (V_1 - V_2)(\vec{\nabla} \cdot \vec{\nabla}(V_1 - V_2)) + [\vec{\nabla}(V_1 - V_2) \cdot \vec{\nabla}(V_1 - V_2)]$   
 taking volume integral on both sides  
 $\int_{vol} (\vec{\nabla} \cdot [(V_1 - V_2)\vec{\nabla}(V_1 - V_2)]) dV = \int_{vol} (V_1 - V_2) \nabla^2 (V_1 - V_2) dV + \int_{vol} [\vec{\nabla}(V_1 - V_2) \cdot \vec{\nabla}(V_1 - V_2)] dV$   
 $\int_{vol} (\vec{\nabla} \cdot [(V_1 - V_2)\vec{\nabla}(V_1 - V_2)]) dV = \int_{vol} (V_1 - V_2) \nabla^2 (V_1 - V_2) dV + \int_{vol} [\vec{\nabla}(V_1 - V_2) \cdot \vec{\nabla}(V_1 - V_2)] dV$   
 $LHS = \oint_S [(V_1 - V_2)\vec{\nabla}(V_1 - V_2)] \cdot d\vec{S}$   
 $= \oint_S [(V_{1b} - V_{2b})\vec{\nabla}(V_{1b} - V_{2b})] \cdot d\vec{S}$   
 $= 0$   
 $\therefore \int_{vol} [\vec{\nabla}(V_1 - V_2)]^2 dV = 0$   
 $\Rightarrow \vec{\nabla}(V_1 - V_2) = 0$   
 $V_1 - V_2 = \text{constant}$   
 on the boundary  
 $V_1 - V_2 = V_{1b} - V_{2b} = 0$   
 $\Rightarrow V_1 - V_2 = 0$   
 $V_1 = V_2$

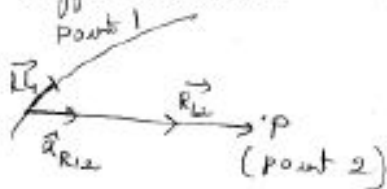
[Note: an integral may be zero if either the integrand is everywhere zero, or the integrand is +ve in some regions and -ve in other regions, and the contributions cancel algebraically. In this case the 1st reason holds good as  $[\vec{\nabla}(V_1 - V_2)]^2$  can not be -ve.]

6.(a) State and explain Biot-Savart's law.

(\*) Biot-Savart's law :-

It is considered a differential current element as a vanishingly small section of a current-carrying filamentary conductor, where a filamentary conductor is the limiting case of a cylindrical conductor of circular cross-section as the radius approaches zero.

We assume a current  $I$  flowing in a differential vector length of the filament  $d\vec{l}$ . The Biot-Savart's law then states that, at any point  $P$  the mag. of the mag. field intensity produced by the differential element is proportional to the product of the current, the mag. of the differential length and the sine of the angle lying b/w the filament and a line connecting the filament to the point  $P$  at which the field is desired. Also, the magnitude of the mag. field intensity is inversely proportional to the square of the distance from the differential element to point  $P$ .

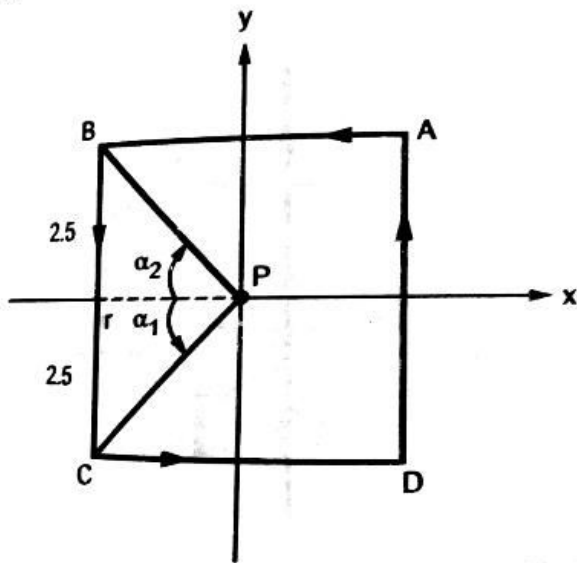


$$d\vec{H}_2 = \frac{I d\vec{l} \times \hat{a}_{r_{12}}}{4\pi r_{12}^2}$$

where  $d\vec{H}_2 \rightarrow$  mag. field intensity produced by a differential current element  $I d\vec{l}$ . The direction of  $d\vec{H}_2$  is into the page.



6.(b)



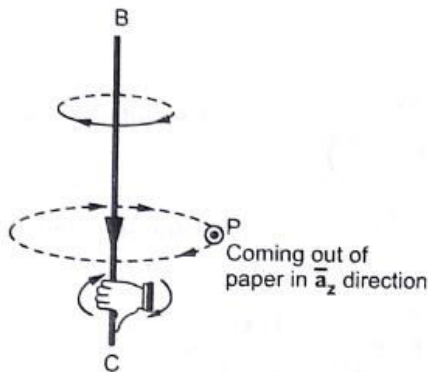
**Alternative method :** Consider one side of a square as shown in the Fig. 7.20, in xy plane. Consider segment BC, which is finite length of the conductor. As B is above P,  $\alpha_1$  is negative and  $\alpha_2$  is positive.

$$\alpha_1 = \tan^{-1} \frac{2.5}{2.5} = 45^\circ, \text{ but}$$

$$\alpha_1 = -45^\circ$$

$$\alpha_2 = +45^\circ$$

$$\therefore |\vec{H}| = \frac{I}{4\pi r} \sin \alpha_2 - \sin \alpha_1 = \frac{10}{4\pi \times 2.5} [\sin(45^\circ) - \sin(-45^\circ)] = 0.4501 \text{ A/m}$$



**Important note :** As BC segment is not along z axis while using formula derived earlier do not use direction as  $\vec{a}_\phi$ . Remember that  $\vec{H}$  direction is normal to the plane containing the source. In this case, square is in xy plane normal to which is  $\vec{a}_z$  hence direction of  $\vec{H}$  is  $\vec{a}_z$ , as shown in the Fig. 7.21 by right handed screw rule.

$$\therefore \vec{H} = 0.4501 \vec{a}_z \text{ A/m}$$

$$\therefore \vec{H}_{\text{total}} = 4\vec{H} = 1.8 \vec{a}_z \text{ A/m}$$



6.(c)

Soln.

$$A_x = 4x + 3y + 2z$$

$$A_y = 5x + 6y + 3z$$

$$A_z = 2x + 3y + 5z$$

$$\begin{aligned} \therefore \vec{\nabla} \times \vec{A} &= \begin{vmatrix} \hat{a}_x & \hat{a}_y & \hat{a}_z \\ \frac{\partial}{\partial x} & \frac{\partial}{\partial y} & \frac{\partial}{\partial z} \\ (4x+3y+2z) & (5x+6y+3z) & (2x+3y+5z) \end{vmatrix} \\ &= \hat{a}_x (3-3) + \hat{a}_y (2-2) + \hat{a}_z (5-3) \\ &= 2 \hat{a}_z \text{ Wb/m}^2 = \vec{B} \end{aligned}$$

7.(a)

Consider the case of current carrying conductors

• convection current density,

$$\boxed{\vec{J} = \rho_v \vec{v}}$$

$$d\vec{a} = \rho_v d\vec{v}$$

$$\therefore d\vec{F} = \rho_v d\vec{v} \vec{v} \times \vec{B}$$

$$\Rightarrow \boxed{d\vec{F} = \vec{J} \times \vec{B} d\vec{v}} \quad [\because \vec{J} = \rho_v \vec{v}]$$

$$\vec{J} d\vec{v} = \vec{K} d\vec{s} = I d\vec{L}$$

$$\therefore d\vec{F} = I \vec{K} \times \vec{B} d\vec{s}$$

$$d\vec{F} = I d\vec{L} \times \vec{B}$$

Integrating,

$$\vec{F} = \int_{\text{vol}} \vec{J} \times \vec{B} d\vec{v}$$

$$\vec{F} = \int \vec{K} \times \vec{B} d\vec{s}$$

$$\vec{F} = \oint I d\vec{L} \times \vec{B} = -I \oint \vec{B} \times d\vec{L}$$

$$\begin{aligned} \vec{J} &= \rho_v \vec{v} \\ d\vec{F} &= \rho_v d\vec{v} \vec{v} \times \vec{B} \\ &= \vec{J} \times \vec{B} d\vec{v} \\ &= I d\vec{L} \times \vec{B} \\ &= -I \vec{B} \times d\vec{L} \end{aligned}$$

$$\vec{F} = Q \vec{E}$$

direction same as electric field intensity.

A charge  $Q$  in motion in a magnetic field with flux-density  $\vec{B}$ .  
velocity of charge =  $\vec{v}$ .

$$\vec{F} = Q \vec{v} \times \vec{B}$$

For a force which is applied in a direction  $\perp$  to the direction of motion can't change magnitude of particle velocity.

i.e. steady magnetic field can not do any energy transfer to the moving charge.

Force on a moving particle due to combined effects of electric and magnetic fields.

$$\vec{F} = Q (\vec{E} + \vec{v} \times \vec{B})$$

7.(b) Derive an expression for force on a differential current element placed in a magnetic field.

Force b/w differential current elements  
 Using Biot-Savart's law, the field at point 2 due to a current element at point 1 is,  

$$d\vec{H}_2 = \frac{I_1 d\vec{L}_1 \times \hat{a}_{R_{12}}}{4\pi R_{12}^2}$$

Differential force on a differential current element is,  $d\vec{F} = (I d\vec{L} \times \vec{B})$ .

Here, in place of  $\vec{B}$ , we use  $d\vec{B}_2$ .  
 $d\vec{B}_2$  is the differential flux density at point 2 caused by current element 1.

One more current element  $I_2 d\vec{L}_2$ .

~~Force~~ differential force on element 2  $d(d\vec{F}_2)$ .

$$\begin{aligned} \therefore d(d\vec{F}_2) &= I_2 d\vec{L}_2 \times d\vec{B}_2 \\ &= I_2 d\vec{L}_2 \times \mu_0 d\vec{H}_2 \\ &= \mu_0 I_2 d\vec{L}_2 \times \frac{I_1 d\vec{L}_1 \times \hat{a}_{R_{12}}}{4\pi R_{12}^2} \\ &= \frac{\mu_0 I_1 I_2}{4\pi R_{12}^2} d\vec{L}_2 \times (d\vec{L}_1 \times \hat{a}_{R_{12}}) \end{aligned}$$

$\therefore$  The total force b/w two filamentary circuits is obtained by integrating twice.

$$\begin{aligned} \vec{F}_2 &= \frac{\mu_0 I_1 I_2}{4\pi} \oint [d\vec{L}_2 \times \oint \frac{d\vec{L}_1 \times \hat{a}_{R_{12}}}{R_{12}^2}] \\ &= \frac{\mu_0 I_1 I_2}{4\pi} \oint [ \oint \frac{\hat{a}_{R_{12}} \times d\vec{L}_1}{R_{12}^2} ] \end{aligned}$$

7.(c)

A conductor 4 m long lies along the y-axis with a current of 10 A in  $\hat{a}_y$  direction. Find the force on the conductor if the field in the region is  $\vec{B} = 0.005 \hat{a}_x$  T.

$$\vec{F} = I d\vec{L} \times \vec{B}$$

$$d\vec{L} = 4 \hat{a}_y$$

$$\vec{B} = 0.005 \hat{a}_x$$

$$I = 10 \text{ A}$$

$$\vec{F} = 10 \times 4 \hat{a}_y \times 0.005 \hat{a}_x$$

$$\vec{F} = -0.2 \hat{a}_z \text{ N}$$

8.(a)

∴ Magnetization  $M$  is the magnetic dipole moment per unit volume,  

$$M = \lim_{\Delta v \rightarrow 0} \frac{1}{\Delta v} \sum_{i=1}^{n \text{ or } \infty} m_i \quad \text{A/m.}$$

Permeability: A quantity measuring the influence of a substance on the magnetic flux in the region it occupies.

8.(b)

(i)  $\mu = 1.8 \times 10^{-5} \text{ H/m} = \mu_0 \mu_r$  &  $H = 120 \text{ A/m.}$

$$\mu_0 = 4\pi \times 10^{-7}$$

$$\mu_r = \frac{\mu}{\mu_0} = \frac{1.8 \times 10^{-5}}{4\pi \times 10^{-7}} = 14.3239$$

$$\chi_m = 13.3239, \quad \vec{M} = \chi_m \vec{H}$$

$$\vec{M} = 1598.873 \text{ A/m}$$

(ii)  $B = 300 \mu\text{T}$

$$\vec{H} = \frac{\vec{B}}{\mu} \quad \mu_r = H \chi_m$$

$$\mu = \mu_0 \mu_r = \mu_0 \times 16$$

$$\vec{M} = \chi_m \vec{H}$$

$$= 15 \times \frac{300 \times 10^{-6}}{\mu_0 \times 16}$$

$$\vec{M} = 223.811 \text{ A/m}$$

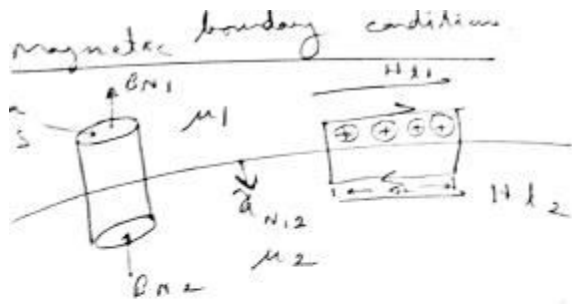
(ii) Magnetization is total magnetic dipole moment per unit volume

$$m_i = 4.5 \times 10^{-27} \text{ A m}^2 \quad (\text{dipole moment for each atom})$$

$$n = 8.3 \times 10^{28} \text{ atoms/m}^3 \quad (\text{total no. of atoms})$$

$$\vec{M} = n \times m_i = 373.5 \frac{\text{A m}^2}{\text{m}^3} \quad \vec{M} = 373.5 \text{ A/m}$$

8.(c) Discuss the boundary conditions at the interface between two media of different permeabilities.



Gauss's law of mag.

$$\oint \vec{B} \cdot d\vec{s} = 0$$

$$B_{N1} \Delta s - B_{N2} \Delta s = 0$$

$$\Rightarrow \boxed{B_{N1} = B_{N2}}$$

$$\therefore H_{N2} = \frac{\mu_1}{\mu_2} H_{N1}$$

Normal comp. of  $B$  is continuous.  
Tangential comp. of  $H$  is discontinuous by

factor  $\left(\frac{\mu_1}{\mu_2}\right)$ .

$$M_{N2} = \chi_{m2} \left(\frac{\mu_1}{\mu_2} H_{N1}\right)$$

$$= \frac{\chi_{m2} \mu_1}{\chi_{m1} \mu_2} M_{N1} \quad [M = \chi_m H]$$

$$H_{N1} = \frac{M_{N1}}{\chi_{m1}}$$

$$\therefore \oint \vec{H} \cdot d\vec{l} = I$$

Small closed path in a plane normal to the boundary surface.

$$H_{t1} \Delta l - H_{t2} \Delta l = K \Delta l$$

Surface current  $\vec{K}$   $\rightarrow$  comp. normal to the plane of closed path  $\rightarrow K$ .

$$\therefore \boxed{H_{t1} - H_{t2} = K}$$

$\Rightarrow (\vec{H}_1 - \vec{H}_2) \times \hat{a}_{N12} = \vec{K}$   
 $\hat{a}_{N12} \rightarrow$  unit normal at the boundary directed from region 1 to region 2

$$(\vec{H}_{t1} - \vec{H}_{t2}) = \hat{a}_{N12} \times \vec{K}$$

$$\frac{B_{t1}}{\mu_1} - \frac{B_{t2}}{\mu_2} = K$$

$$\left( \frac{B_{t2}}{\mu_2} = \frac{\chi_{m2}}{\chi_{m1}} M_{t1} - \chi_{m2} K \right)$$

$$H_{t1} - H_{t2} = k$$

$$\Rightarrow \frac{M_{t1}}{x_{m1}} - \frac{M_{t2}}{x_{m2}} = k$$

$$\Rightarrow M_{t1} x_{m2} - M_{t2} x_{m1} = k x_{m1} x_{m2}$$

$$\Rightarrow M_{t2} x_{m1} = -k x_{m1} x_{m2} + M_{t1} x_{m2}$$

$$\Rightarrow \boxed{M_{t2} = \frac{x_{m2}}{x_{m1}} M_{t1} - k x_{m2}}$$


9. (a)

- Two separate windings on an iron toroid and placed a galvanometer in one ckt. and battery on the other.

- closing the battery ckt, momentary deflection of the galvanometer.

- A similar deflection in the opposite direction occurred when the battery was disconnected.

- either a moving mag. field or a moving coil could also produce a galvanometer deflection.



- Time varying mag. field produces an emf which may establish a current in a suitable closed ckt.

Faraday's law:  $e \propto -\frac{d\phi}{dt}$   $\Rightarrow e = -k \frac{d\phi}{dt}$   $k = \frac{d\phi}{dI}$   $(k=1)$

$e = -\frac{d\phi}{dt}$  conducting loop, not

~~side note~~ we consider a closed path, the mag. flux is that flux that passes through any and every surface whose perimeter is the closed path.

and  $\frac{d\phi}{dt} \rightarrow$  time rate of change of flux

A non-zero value of  $\frac{d\phi}{dt}$  occurs when:

- Time-changing flux linking a closed path.
- Relative motion b/w a steady flux and a closed path.
- A combination of the two.

The minus sign is an indication that the emf is in a direction as to produce a current whose

- If the closed path is that taken by  $N$  thin filamentary conductors, it is sufficiently accurate to consider the turns as coincident and let,

$$\text{emf} = -N \frac{d\phi}{dt}$$

where,  $\phi \rightarrow$  flux passing through any one of the  $N$  coincident paths.

e.m.f is defined as

$\text{emf} = \oint \vec{E} \cdot d\vec{l} \rightarrow$  voltage about a specific closed path

for electrostatic  $\oint \vec{E} \cdot d\vec{l} = 0$

$$\text{e.m.f} = \oint \vec{E} \cdot d\vec{l} = - \frac{d\phi}{dt} = - \frac{d}{dt} \int \vec{B} \cdot d\vec{S}$$

fingers of our right hand indicate the direction of the closed path. thumb indicates the direction of  $d\vec{S}$ .

- A flux-density  $\vec{B}$  in the direction of  $d\vec{S}$  and increasing with time thus produces an average value of  $\vec{E}$  which is opposite to the +ve direction about the path.

Stationary path.

magnetic flux  $\rightarrow$  time varying quantity.

$$\therefore \text{emf} = \oint \vec{E} \cdot d\vec{l} = - \int \frac{\partial \vec{B}}{\partial t} \cdot d\vec{l}$$

Applying Stokes's theorem

$$\int (\vec{\nabla} \times \vec{E}) \cdot d\vec{S} = - \int \frac{\partial \vec{B}}{\partial t} \cdot d\vec{S}$$

Surface integrals taken over identical generic surfaces.

$$\therefore (\vec{\nabla} \times \vec{E}) \cdot d\vec{S} = - \frac{\partial \vec{B}}{\partial t} \cdot d\vec{S}$$

$$\Rightarrow \boxed{(\vec{\nabla} \times \vec{E}) = - \frac{\partial \vec{B}}{\partial t}} \rightarrow \text{differential or point form}$$

$$\boxed{\oint \vec{E} \cdot d\vec{l} = - \int \frac{\partial \vec{B}}{\partial t} \cdot d\vec{S}} \rightarrow \text{voltage}$$



9.(b)

$$|\sigma \vec{E}| = |j\omega \epsilon \vec{E}|$$

$$\frac{\sigma}{\omega \epsilon} = 1$$

$$\text{or } \sigma = \omega \epsilon$$

$$\omega = \frac{\sigma}{\epsilon} = \frac{2 \times 10^{-4}}{8.854 \times 10^{-12} \times 81} = \frac{2 \times 10^{-4} \times 4}{81 \times 81 \pi \times 10^{-9}}$$

$$= \frac{8\pi \times 10^5}{9}$$

$$\boxed{\omega = 2.679 \times 10^8 \text{ rad/s}}$$

$$f = \frac{\omega}{2\pi} = \frac{8\pi \times 10^5}{2\pi \times 9}$$

$$f = 4.44 \times 10^6 \text{ Hz}$$

$$\boxed{f = 4.44 \text{ MHz}}$$

9.(c)

- Maxwell's eqn. in point form:

$$\vec{\nabla} \cdot \vec{D} = \rho_v$$

$$\vec{\nabla} \cdot \vec{B} = 0$$

$$\vec{\nabla} \times \vec{E} = -\frac{\partial \vec{B}}{\partial t}$$

$$\vec{\nabla} \times \vec{H} = \vec{J} + \frac{\partial \vec{D}}{\partial t}$$

Maxwell's eqn. in Integral form:

$$\oint \vec{D} \cdot d\vec{s} = Q$$

$$\oint \vec{B} \cdot d\vec{s} = 0$$

$$\oint \vec{E} \cdot d\vec{l} = -\frac{d}{dt} \int \vec{B} \cdot d\vec{s}$$

$$\oint \vec{H} \cdot d\vec{l} = I + \int \frac{\partial \vec{D}}{\partial t} \cdot d\vec{s}$$



10.(a)

Solution of wave equation (Uniform Plane Waves)

(iii)

$$\nabla^2 \vec{E}_s = -j^2 \vec{E}_s$$

$$\vec{E}_x(z,t) = E_{xs}(z) e^{j\omega t}$$

$$\vec{H}_y(z,t) = H_{ys}(z) e^{j\omega t}$$

$$\nabla^2 E_{xs} = -j^2 E_{xs}$$

$$\frac{\partial^2 E_{xs}}{\partial x^2} + \frac{\partial^2 E_{xs}}{\partial y^2} + \frac{\partial^2 E_{xs}}{\partial z^2} = -j^2 E_{xs}$$

$$\vec{E}_s = E_{xs} \vec{a}_x$$

$$\vec{H}_s = H_{ys} \vec{a}_y$$

$$\frac{d^2 E_{xs}}{dz^2} = -j^2 E_{xs}$$

Solution of the above equation is

$$E_{xs}(z) = E_{x0} e^{-jz} + E_{x0} e^{jz}$$

↑ Forward travelling wave
 ↑ Backward travelling wave

$$\vec{E}_x(z,t) = \vec{E}_{xs}(z) e^{j\omega t}$$

$$\vec{E}_x(z,t) = (E_{x0} e^{-jz} + E_{x0} e^{jz}) e^{j\omega t} \vec{a}_x$$

$$\vec{E}_x(z,t) = \left[ E_{x0} e^{-\alpha z - j\beta z} e^{j\omega t} + E_{x0} e^{\alpha z + j\beta z} e^{j\omega t} \right] \vec{a}_x$$

↑ Forward travelling wave
 ↑ Backward travelling wave

From the Maxwell's equation

$$\nabla \times \vec{E}_s = -j\omega \mu \vec{H}_s$$

$$\nabla \times \vec{E}_s = \begin{vmatrix} \vec{a}_x & \vec{a}_y & \vec{a}_z \\ \frac{\partial}{\partial x} & \frac{\partial}{\partial y} & \frac{\partial}{\partial z} \\ E_{xs} & 0 & 0 \end{vmatrix} = \vec{a}_x (0-0) - \vec{a}_y (0 - \frac{\partial E_{xs}}{\partial z}) + \vec{a}_z (0-0)$$

$$\nabla \times \vec{E}_s = \frac{\partial E_{xs}}{\partial z} \vec{a}_y$$

$$\Rightarrow \frac{\partial E_{xs}}{\partial z} \hat{a}_y = -j\omega\mu H_{ys} \hat{a}_y$$

$$H_{ys} = -\frac{1}{j\omega\mu} \cdot \frac{\partial}{\partial z} \left[ E_{x0} e^{-j\gamma z} + E_{x0}' e^{j\gamma z} \right]$$

$$H_{ys} = E_{x0} \cdot \frac{e^{-j\gamma z} \cdot (-j\gamma)}{(-j\omega\mu)} + E_{x0}' \frac{e^{j\gamma z} (j\gamma)}{(-j\omega\mu)}$$

$$H_{ys} = \frac{E_{x0} \cdot e^{-j\gamma z}}{\left(\frac{j\omega\mu}{\gamma}\right)} + \frac{E_{x0}' \cdot e^{j\gamma z}}{-\left(\frac{j\omega\mu}{\gamma}\right)}$$

$\eta = \text{Intrinsic impedance}$

$$\frac{E_{x0}}{\eta} = H_{y0}$$

$$\frac{E_{x0}'}{-\eta} = H_{y0}'$$

$$H_{ys} = H_{y0} e^{-j\gamma z} + H_{y0}' e^{j\gamma z} \quad \eta = \frac{j\omega\mu}{\gamma}$$

Intrinsic Impedance,

$$\eta = \frac{j\omega\mu}{j\gamma} = \frac{j\omega\mu}{\sqrt{j\omega\mu(\sigma + j\omega\epsilon)}} = \sqrt{\frac{j\omega\mu}{\sigma + j\omega\epsilon}}$$

$$\vec{H}_y(z,t) = \left[ \frac{E_{x0}}{\eta} e^{-\alpha z} e^{-j\beta z} e^{j\omega t} + \frac{E_{x0}'}{\eta} e^{\alpha z} e^{j\beta z} e^{j\omega t} \right] \hat{a}_y$$

10.(b)

Poynting's theorem :-

Poynting's theorem states that the net power flowing out of a given volume  $V$  is equal to the time-rate of decrease in the energy stored within  $V$  minus the ohmic losses.

If the medium is conductive, Maxwell's equation becomes,

$$\vec{\nabla} \times \vec{H} = \vec{J} + \frac{\partial \vec{B}}{\partial t} \quad \dots (1)$$

Taking scalar product of both sides with  $\vec{E}$ ,

$$\vec{E} \cdot (\vec{\nabla} \times \vec{H}) = \vec{E} \cdot \vec{J} + \vec{E} \cdot \frac{\partial \vec{B}}{\partial t} \quad \dots (2)$$

Consider the vector identity

$$\vec{\nabla} \cdot (\vec{E} \times \vec{H}) = -\vec{E} \cdot (\vec{\nabla} \times \vec{H}) + \vec{H} \cdot (\vec{\nabla} \times \vec{E})$$

$$\Rightarrow \vec{E} \cdot (\vec{\nabla} \times \vec{H}) = \vec{H} \cdot (\vec{\nabla} \times \vec{E}) - \vec{\nabla} \cdot (\vec{E} \times \vec{H}) \quad \dots (3)$$

Using this result in eqn. (2),

$$\vec{H} \cdot (\vec{\nabla} \times \vec{E}) - \vec{\nabla} \cdot (\vec{E} \times \vec{H}) = \vec{E} \cdot \vec{J} + \vec{E} \cdot \frac{\partial \vec{B}}{\partial t}$$

$$\Rightarrow \vec{H} \cdot \left( -\frac{\partial \vec{B}}{\partial t} \right) - \vec{\nabla} \cdot (\vec{E} \times \vec{H}) = \vec{J} \cdot \vec{E} + \vec{E} \cdot \frac{\partial \vec{B}}{\partial t}$$

$$\Rightarrow -\vec{\nabla} \cdot (\vec{E} \times \vec{H}) = \vec{J} \cdot \vec{E} + \epsilon \vec{E} \cdot \frac{\partial \vec{E}}{\partial t} + \mu \vec{H} \cdot \left( \frac{\partial \vec{H}}{\partial t} \right) \quad \dots (4)$$

$$\text{Now, } \epsilon \vec{E} \cdot \frac{\partial \vec{E}}{\partial t} = \frac{\partial}{\partial t} (\frac{1}{2} \vec{B} \cdot \vec{E})$$

$$\text{and } \mu \vec{H} \cdot \frac{\partial \vec{H}}{\partial t} = \frac{\partial}{\partial t} (\frac{1}{2} \vec{B} \cdot \vec{H}) \quad \dots \quad \nabla$$

Eqn. (3) becomes,

$$-\nabla \cdot (\vec{E} \times \vec{H}) = \vec{J} \cdot \vec{E} + \frac{\partial}{\partial t} \left( \frac{1}{2} \vec{D} \cdot \vec{E} \right) + \frac{\partial}{\partial t} \left( \frac{1}{2} \vec{B} \cdot \vec{H} \right)$$

Integrating over a volume,

$$-\int_{\text{vol}} \nabla \cdot (\vec{E} \times \vec{H}) dV = \int_{\text{vol}} \vec{J} \cdot \vec{E} dV + \int_{\text{vol}} \frac{\partial}{\partial t} \left( \frac{1}{2} \vec{D} \cdot \vec{E} \right) dV + \int_{\text{vol}} \frac{\partial}{\partial t} \left( \frac{1}{2} \vec{B} \cdot \vec{H} \right) dV$$

$$\Rightarrow -\oint_{\text{area}} (\vec{E} \times \vec{H}) \cdot d\vec{S} = \text{R.H.S}$$

∴ R.H.S,

1st term = ohmic power dissipated within the volume  
 2nd term = total energy stored in the electric field  
 3rd term = " " " " " magnetic field

R.H.S = total power flowing into the volume.

∴ The total power flowing out of the volume is

$$\oint_{\text{area}} (\vec{E} \times \vec{H}) \cdot d\vec{S} \text{ W}$$

The cross-product,  $(\vec{E} \times \vec{H}) = \vec{S}$  Poynting's vector.

Direction of power flow normal to both  $\vec{E}$  &  $\vec{H}$  vectors

10.(c)

Given:  $\delta = 0.1 \text{ m}$  (depth of penetration).

$$f = 1 \text{ MHz}$$

To find:  $\sigma = ?$

$$\delta = \frac{1}{\sqrt{\pi f \mu \sigma}} \Rightarrow$$

$$\delta^2 = \frac{1}{\pi f \mu \sigma}$$

$$\sigma = \frac{1}{\pi f \mu \delta^2} = \frac{1}{\pi \times 1 \times 10^6 \times \mu_0 \times (0.1)^2}$$

$$\sigma = \frac{1}{\pi \times 10^6 \times 4\pi \times 10^{-7} \times (0.1)^2} = 25.33$$

$$\sigma = 25.33 \text{ S/m}$$