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Internal Assessment Test II

<b>SUBJECT: BASIC THERMODYNAMICS</b>										<b>Code:</b>	18ME33
<b>Date:</b>	14/10/2019	<b>Duration:</b>	90 min	<b>Max. Marks:</b>	50	<b>Sem:</b>	03	<b>Branch:</b>	MECH		

Answer any 2 FULL questions. Each question carries equal marks.

Q. No.	Question	Marks	OBE M.A.P	
			CO	I.B.T
1	a Write the vander walls equation and derive the vander walls constants	[10]	CO3	I1
	b Mixture of gases comprises 30% CO, 15% CO <sub>2</sub> , and 55% H <sub>2</sub> . Find the gravimetric analysis specific gas constant and molecular weight of the mixture.	[8]	CO3	I2
	c Determine the mass of nitrogen contained in a 35m <sup>3</sup> vessel at 200 bar and 200 K by using i) the ideal gas equation ii) generalized compressibility chart.	[7]	CO3	I3
2	a Write the short notes on the flowing. i) Law of corresponding states ii) compressibility factor ii) generalized compressibility chart.	[8]	CO3	I3
	b 10 kg of carbon dioxide is enclosed in a container at a temperature of 100 <sup>0</sup> C and pressure of 1 bar calculate the volume of the container by i) ideal gas equation ii) vander walls equation iii) compressibility chart	[10]	CO3	I3
	c 1 kg of CO <sub>2</sub> has volume of 0.86 m <sup>3</sup> at 120 <sup>0</sup> C. compute the pressure using i) ideal gas equation ii) vander walls equation	[7]	CO4	I1
3	a Define Entropy and prove the clausius theorem	[9]	CO3	I4
	b A mixture of ideal gases contain 5 kg of N <sub>2</sub> and 8 kg of CO <sub>2</sub> . The partial pressure of N <sub>2</sub> in the mixture is 120 kpa. Find i) mole fraction of N <sub>2</sub> and CO <sub>2</sub> ii) partial pressure of CO <sub>2</sub> iii) Molecular weight of the mixture.	[9]	CO4	I3
	c Determine pressure exerted by CO <sub>2</sub> in a container 1.5m <sup>3</sup> capacity, when it contains 5kg at 27 <sup>0</sup> C, using i) ideal gas equation ii) vander walls equation.	[7]	CO4	I1

CI

CCI

HOD

### Degree of saturation :-

It is defined as the mass of water vapour in a unit mass of dry Air, to the mass of water vapour in a unit mass of dry Air when the Air is saturated at the same temperature.

### Adiabatic saturation temperature :-

It is the temperature at which the water (or) Ice can saturate by evaporating adiabatically into it.

### Enthalpy of Moist Air :-

It is the sum of enthalpy of dry Air and enthalpy of water vapour associated with dry Air.

19 (c) write the vanderwaals equation and derive the constants a and b. vanderwaals' equation is given by

$$\left(P + \frac{a}{v^2}\right) (v - b) = RT_c$$

$$\left(P + \frac{a}{v^2}\right) = \frac{RT_c}{v - b}$$

$$P = \frac{RT}{v - b} - \frac{a}{v^2} \rightarrow (1)$$

$$\frac{dp}{dv} = \frac{-RT_c}{(V_c - b)^2} + \frac{2a}{V_c^3} = 0 \rightarrow (2)$$

$$\frac{d^2p}{dv^2} = \frac{2RT_c}{(V_c - b)^3} - \frac{6a}{V_c^4} = 0 \rightarrow (3)$$

$$\frac{RT_c}{(V_c - b)^2} = \frac{2a}{V_c^3} \rightarrow (4)$$

$$\frac{2RT_c}{(V_c - b)^3} = \frac{6a}{V_c^4} \rightarrow (5)$$

Divide (4) by (5)

$$\frac{\frac{RT_c}{(V_c - b)^2}}{\frac{2RT_c}{(V_c - b)^3}} = \frac{\frac{2a}{V_c^3}}{\frac{6a}{V_c^4}}$$

$$\frac{RT_c}{(V_c - b)^2} \times \frac{(V_c - b)^3}{2RT_c} = \frac{2a}{V_c^3} \times \frac{V_c^4}{\frac{6a}{3}}$$

$$\frac{V_c - b}{2} = \frac{V_c}{3}$$

$$3V_c - 3b = 2V_c$$

$$3V_c - 2V_c = 3b$$

$$V_c = 3b$$

$$b = \frac{V_c}{3}$$

substitute  $b = v_c/3$  in eq ④

$$\Rightarrow \frac{RT_c}{(v_c - b)^2} = \frac{2a}{v_c^3}$$

$$\Rightarrow \frac{RT_c}{(v_c - \frac{v_c}{3})^2} = \frac{2a}{v_c^3}$$

$$\Rightarrow \frac{RT_c}{(\frac{2v_c}{3})^2} = \frac{2a}{v_c^3}$$

$$\Rightarrow \frac{RT_c}{\frac{4v_c^2}{9}} = \frac{2a}{v_c^3}$$

$$\Rightarrow RT_c v_c^3 = 2a \left[ \frac{4v_c^2}{9} \right]$$

$$\Rightarrow RT_c v_c^3 = \frac{8av_c^2}{9}$$

$$\Rightarrow R = \frac{8v_c^2 a}{9T_c v_c^3}$$

$$\Rightarrow R = \frac{8a}{9T_c v_c}$$

substitute  $b$  and  $R$  values in vanderwaals equation

$$(P_c + \frac{a}{v_c^2}) (v_c - b) = RT_c$$

$$(P_c + \frac{a}{v_c^2}) (v_c - \frac{v_c}{3}) = \frac{8a}{9T_c v_c} \cdot T_c$$

$$(P_c + \frac{a}{v_c^2}) (\frac{3v_c - v_c}{3}) = \frac{8a}{9v_c}$$



$$\Rightarrow \left( P_c + \frac{a}{v_c^2} \right) \left( \frac{2v_c}{3} \right) = \frac{8a}{9v_c}$$

$$\Rightarrow P_c + \frac{a}{v_c^2} = \frac{8a}{9v_c} \times \frac{3}{2v_c}$$

$$\Rightarrow P_c + \frac{a}{v_c^2} = \frac{24a}{18v_c^2}$$

$$\Rightarrow P_c + \frac{a}{v_c^2} = \frac{4a}{3v_c^2}$$

$$\Rightarrow P_c = \frac{4a}{3v_c^2} - \frac{a}{v_c^2}$$

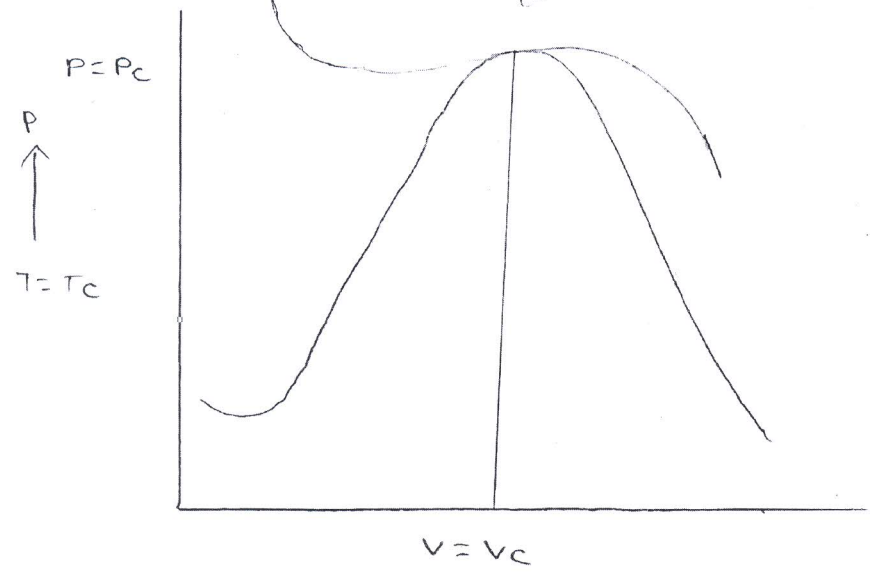
$$\Rightarrow P_c = \frac{a}{v_c^2} \left[ \frac{4}{3} - 1 \right]$$

$$\Rightarrow P_c = \frac{a}{v_c^2} \left[ \frac{4-3}{3} \right]$$

$$\Rightarrow P_c = \frac{a}{3v_c^2}$$

$$\Rightarrow a = 3P_c v_c^2$$

*critical state*



1 > Given data

b  $x_{CO} = 0.3$      $x_{CO_2} = 0.15$      $x_{H_2} = 0.55$

$m_{fCO} = ?$      $m_{fCO_2} = ?$      $m_{fH_2} = ?$

$$M = x_{CO} M_{CO} + x_{CO_2} M_{CO_2} + x_{H_2} M_{H_2}$$
$$= 0.3 \times 28 + 0.15 \times 44 + 0.55 \times 2$$
$$= \underline{\underline{16.1 \text{ kg/kg mol}}}$$

$$R = \frac{R_u}{M} = \frac{8.314}{16.1} = \underline{\underline{0.516 \text{ kJ/kg}\cdot\text{K}}}$$

Gravimetric Composition

$$m_{fCO} = x_{CO} \times \frac{M_{CO}}{M} = 0.3 \times \frac{28}{16.1} = \underline{\underline{0.522}}$$

$$m_{fCO_2} = x_{CO_2} \times \frac{M_{CO_2}}{M} = 0.15 \times \frac{44}{16.1} = \underline{\underline{0.409}}$$

$$\underline{\underline{m_{fH_2}}} = x_{H_2} \times \frac{M_{H_2}}{M} = 0.55 \times \frac{2}{16.1} = \underline{\underline{0.068}}$$

1  
c

$$N_2, V_2 = 35 \text{ M}^3 \quad P = 200 \times 100 \text{ kPa.}$$

i) ideal gas equation.

From Thermodynamic hand book, for  $N_2$   
We get

$$M = 28, \quad R_u = 8.314 \text{ kJ/kg mol K.}$$

$$Pv = mRT = \quad R = \frac{R_u}{M} = \frac{8.314}{28} \\ = 0.2969 \text{ kJ/kg K.}$$

$$200 \times 100 \times 35 = m \times 0.2969 \times 200$$

$$m = \underline{\underline{11788.48 \text{ kg}}}$$

ii) Generalized compressibility Chart.

$$P_c = 33.94 \text{ bar} \quad T_c = 126.2^\circ \text{C}$$

$$P_r = \frac{P}{P_c} = \frac{200}{33.94} = \underline{\underline{5.89}} \quad T_r = \frac{T}{T_c} = \frac{200}{126.2} = \underline{\underline{1.58}}$$

$$Z = 0.9$$

$$Z = \frac{P_{\text{act}}}{RT} = \quad 0.9 = \frac{200 \times 100 \times V_{\text{act}}}{0.2969 \times 200} \quad V_{\text{act}} = 0.00266 \\ M = \frac{35}{0.00266} \text{ M}^3/\text{kg}$$

and WBT.

This curve also possess WBT lines, enthalpy and specific volume lines.

Q. 1

state the following

Law of corresponding states

If any two gases have equal values of reduced pressure and reduced temperature, then they have same values of reduced volume.

i.e  $v_r = \text{function of reduced temperature } T_r$  and reduced pressure  $P_r$ .  $f(T_r, P_r)$

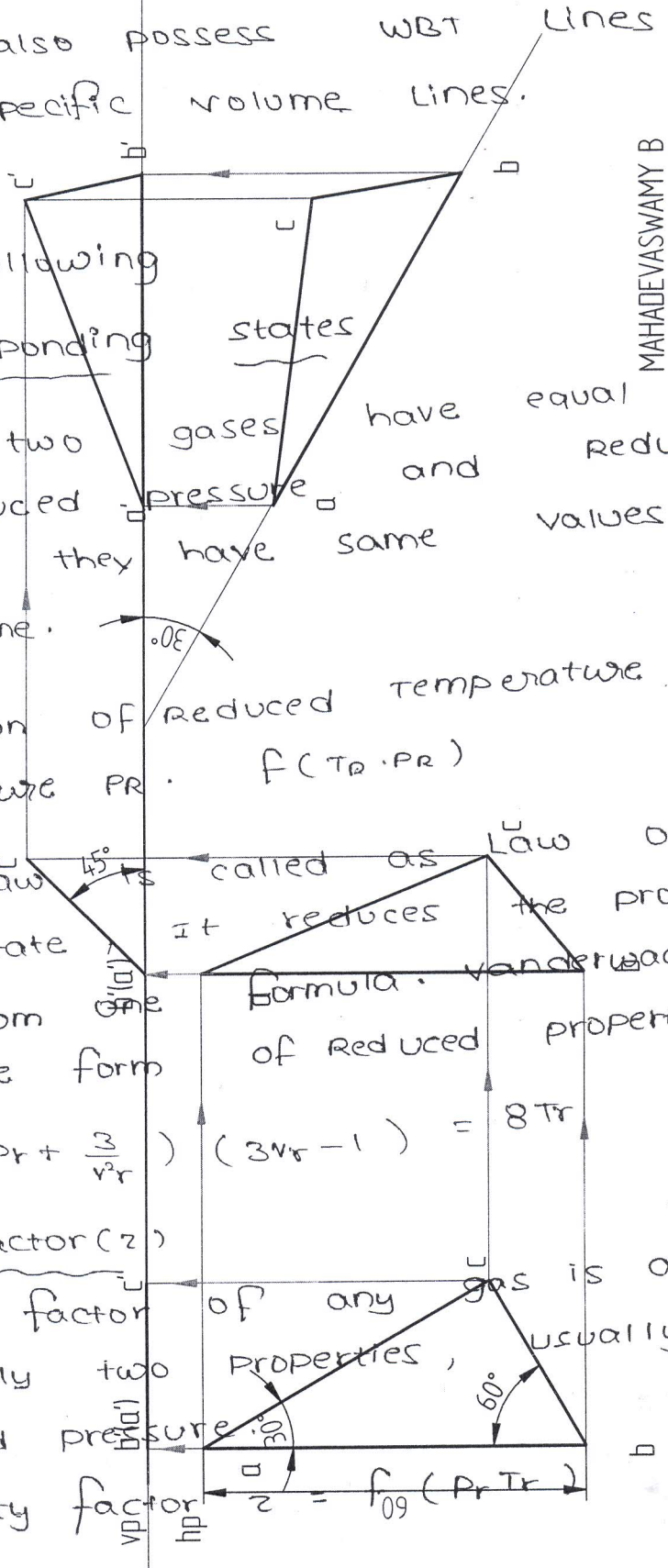
The above law is called as Law of corresponding state. It reduces the property of all gases from one equation in the form of reduced properties

is given by  $(P_r + \frac{3}{v_r}) (3v_r - 1) = 8T_r$

Compressibility Factor (z)

compressibility factor of any gas is a function of only two properties, usually temperature and pressure

i.e compressibility factor  $z = f_09(P_r, T_r)$



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It also defined as the ratio of the actual volume to the, volume predicted by the ideal gas law at a given pressure and temperature.

$$Z = \frac{\text{actual volume}}{\text{Volume Predicted by ideal gas law}}$$

$$Z = \frac{V_{act}}{\frac{RT}{P}} = \frac{P \cdot V_{act}}{RT}$$

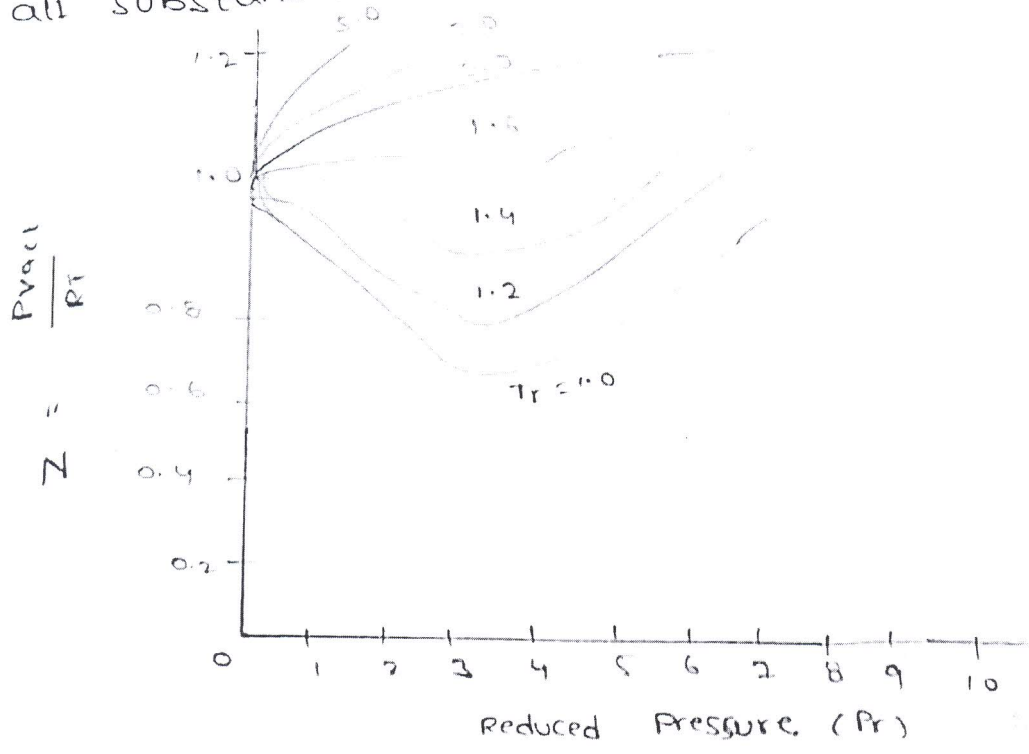
If the gas behaves like an ideal gas, then  $Z = 1$  at all temperatures and pressures. Thus to quantify the deviation of real gas behaviour from the ideal gas behaviour compressibility factor is used.

Generalized compressibility chart

- \* The General compressibility chart is plotted with  $Z$  versus  $P_r$  for values of  $T_r$ .
- \* This is constructed by plotting the known data of one or more gases and can be used for any gas.
- \* This chart provides one of the best means of expressing deviation from ideal behaviour and gives result with an accuracy of with in 5%.

The following observations can be made from the generalized chart

- (1) At all temperatures  $Z = 1$   
 $P_r = 0$
- (2) At the temperature is equal to twice the critical temperature ( $T_r = 2$ ) and above  $Z = 1$  over a wide range of pressure up to 5 times the critical pressure.
- (3) The compressibility factor at the critical point  $Z_c = \frac{P_{vc}}{RT}$  is called critical compressibility and is found to be equal to 0.275 for all substances.



2

b.

$$m = 10 \text{ kg} \quad T = 100 + 273 = 373 \text{ K} \quad P = 1 \text{ bar} = 100 \text{ kPa}$$

$$V = ?$$

From Thermodynamic data book for

$$\text{CO}_2 = M = 44.$$

$$a = 362850 \text{ N/m}^4 / (\text{kg mol})^2 \quad b = 0.0423 \text{ m}^3 / (\text{kg mol})$$

i. ideal gas equation,

$$PV = mRT$$

$$R = \frac{R_u}{M} = \frac{8.314}{44}$$

$$= 0.189 \text{ kJ/kg}\cdot\text{K}$$

$$V = \frac{mRT}{P} = \frac{100 \times 0.189 \times 373}{1 \times 100} = 7.048 \text{ m}^3.$$

ii. van der Waals's equation,

$$\left( 1 \times 10^5 + \frac{362850}{V_m^2} \right) (V_m - 0.0423) = 8.314 \times 373$$

$$V_m = 30.75 \text{ m}^3 / (\text{kg mol})$$

$$n = \frac{m}{M} = \frac{10}{44} = 0.227 \text{ mol}$$

$$\text{Volume of CO}_2 = V = nV_m = 0.227 \times 30.75 = 6.98 \text{ m}^3$$

## Compressibility factor

From Thermodynamic data book critical Properties for  $\text{CO}_2$

$$T_c = 304.2 \quad P_c = 73.85$$

$$T_r = \frac{T}{T_c} = \frac{373}{304.2} = 1.23 \quad P_r = \frac{P}{P_c} = \frac{1}{73.85} = 0.0135$$

From Compressibility Chart  $T_r = 1.23$  &  $P_r = 0.0135$

We get  $z = 0.98$

$$z = \frac{Pv}{RT} = 0.98 = \frac{100 \times V}{0.189 \times 373} = 0.701 \text{ m}^3/\text{kg}$$

For mass of 10 kg

$$V = 10 \times 0.701 = 7.01 \text{ m}^3$$

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$$\frac{2}{c.} \quad a = 365.6 \frac{\text{kJm}^4}{(\text{kgmol})^2} \quad b = 0.0423 \frac{\text{m}^3}{\text{kgmol}}$$

$$V = 1 \text{ m}^3 \quad T = 120 + 273 = 393 \text{ K}$$

$$\text{CO}_2 \quad n = \frac{m}{M} = \frac{1}{44}$$

i> using ideal gas equation

$$P_{vm} = R_u T \quad R_u = 8.314 \text{ kJ/kgmol}$$

$$P = \frac{R_u T}{V_m} \quad V_m = \frac{V}{n} = \frac{0.86}{\frac{1}{44}} = 37.84 \text{ m}^3/\text{kgmol}$$

$$= \frac{8.314 \times 393}{37.84} = 86.35 \text{ kN/m}^2$$

ii> vander waal's equation

$$\left( P + \frac{a}{V_m^2} \right) (V_m - b) = R_u T$$

$$\left( P + \frac{365.6}{37.84^2} \right) (37.84 - 0.0423) = 8.314 \times 393$$

$$P = \underline{\underline{86.18 \text{ kN/m}^2}}$$

3b.

$$x_{N_2} = \frac{n_{N_2}}{n_{N_2} + n_{CO_2}} = \frac{0.17}{0.17 + 0.182} = 0.483.$$

$$n_{N_2} = \frac{m_{N_2}}{M_{N_2}} = \frac{5}{28} = 0.17 \text{ kg mol}$$

$$n_{CO_2} = \frac{m_{CO_2}}{M_{CO_2}} = \frac{8}{44} = 0.182 \text{ kg mol}$$

$$x_{CO_2} = \frac{n_{CO_2}}{n_{N_2} + n_{CO_2}} = \frac{0.182}{0.17 + 0.182} = 0.517$$

$$(ii) \quad x_{CO_2} = \frac{P_{CO_2}}{P} = 0.517 = \frac{P_{CO_2}}{P}$$

$$P_{CO_2} = 0.517 P.$$

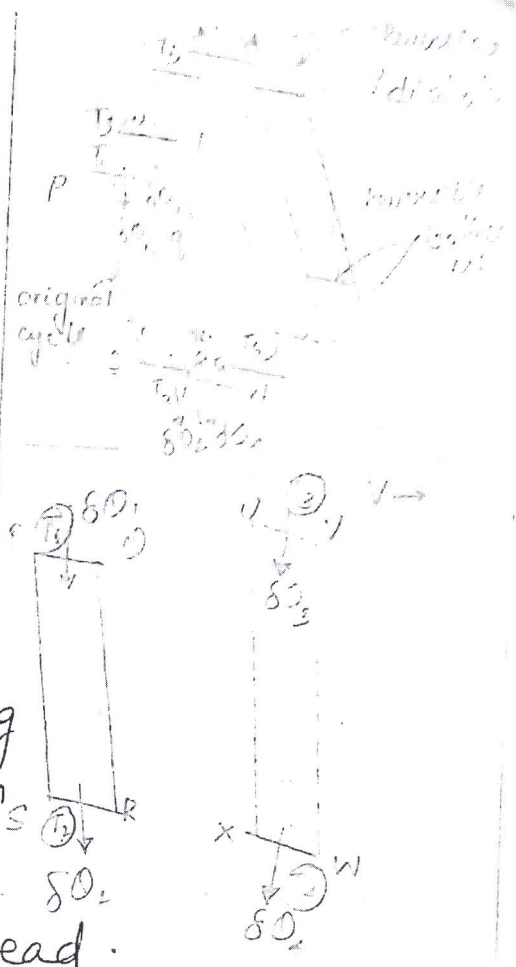
$$x_{N_2} = \frac{P_{N_2}}{P} \quad P = \frac{P_{N_2}}{x_{N_2}} = \frac{120}{0.483} = 248.45 \text{ kPa}$$

$$P_{CO_2} = 128.47 \text{ kPa}.$$

3  
a

### Clausius Theorem

Consider a smooth, closed curve which represents a reversible cycle. A number of reversible adiabatic(s) can be drawn as shown in the above fig. so that the closed cycle can be split into large no. of small strips, each of which may be closed by drawing reversible isotherms at top & bottom so that the original cycle (circle) is replaced a no. of Carnot Cycles instead.



For the elemental cycle PQRS, ' $\delta Q_1$ ' is the heat absorbed reversibly at temp  $T_1$  & ' $\delta Q_2$ ' is the heat rejected reversibly at temp  $T_2$ . WKT,

$$\frac{Q_1}{Q_2} = \frac{T_1}{T_2} \Rightarrow \frac{\delta Q_1}{\delta Q_2} = \frac{T_1}{T_2}$$

i.e.,  $\frac{\delta Q_1}{T_1} = \overset{\text{rejected}}{-\frac{\delta Q_2}{T_2}} \Rightarrow \frac{\delta Q_1}{T_1} + \frac{\delta Q_2}{T_2} = 0$

We consider heat supplied to & rejected by the system is considered +ve & -ve respectively.

Similarly, for elemental cycle UVWX,  $\frac{\delta Q_3}{T_3} = \frac{\delta Q_4}{T_4}$

i.e.,  $\frac{\delta Q_3}{T_3} + \frac{\delta Q_4}{T_4} = 0$

3  
a.

• Similarly, similar/identical equations can be written for all elemental Carnot cycles.

∴ for the whole original cycle,

$$\frac{\delta Q_1}{T_1} + \frac{\delta Q_2}{T_2} + \frac{\delta Q_3}{T_3} + \dots + \frac{\delta Q_n}{T_n} = 0$$

$$\left( \frac{\delta Q}{T} \right)_R = 0$$



3

c.

i ideal gas equation

$$R = \frac{R_u}{M} = \frac{8.314}{44} = 188.95 \text{ J/kg}\cdot\text{K}$$

$$Pv = mRT \quad P = \frac{mRT}{V} = \frac{5 \times 188.95 \times 300}{1.5}$$

$$188.95 \text{ kPa}$$

$$1.88 \text{ bar}$$

ii) using van der Waals equation

$$\left(P + \frac{a}{V_m^2}\right)(V_m - b) = R_u T$$

$$V_m = \frac{V \times M}{m} = \frac{1.5 \times 44}{5} = 13.2 \text{ m}^3/\text{kg-mol}$$

$$\left(P + \frac{364.3}{13.2^2}\right)(13.2 - 0.0427) = 8.314 \times 300$$

$$P = 128.9 \text{ kPa}$$

$$= 1.289 \text{ bar}$$