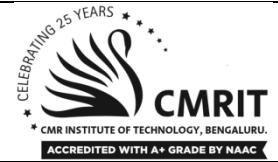


USN



Internal Assessment Test 3 – Nov. 2019

| | | | | | | | | | | |
|--|--|-----------|----------|------------|-----------|------------|---------------------------------|-------|----|-----|
| Sub: | CONTROL ENGINEERING | | | | Sub Code: | 15ME73 | Branch: | ME | | |
| Date: | 19/11/19 | Duration: | 90 min's | Max Marks: | 50 | Sem / Sec: | 7th/A & B | | | |
| Section A (Answer all questions) | | | | | | | | MARKS | CO | RBT |
| 1 | For a unity feedback system : $G(s) = \frac{K(s+1)}{s(s-1)(s+6)}$ Determine: i) Range of K for system to be stable. ii) Marginal value of K. iii) Location of roots for marginal value of K. | | | | | | [10] | CO4 | L2 | |
| 2 | $G(s)H(s) = \frac{K(s+1)}{s(s-1)(s^2+4s+16)}$ Draw root locus. Determine for damping ratio = 0.6: i) Closed loop dominant poles ii) Damped natural frequency iii) Gain K | | | | | | [20] | CO5 | L2 | |
| Section B (Answer ANY ONE question) | | | | | | | | | | |
| 3 | The open loop transfer function of a certain unity feedback system is given by $G(s) = \frac{K}{s(s+2)(s+20)}$ Construct Bode Plots and determine: i) Limiting value of K for system to be stable. ii) Value of K for gain margin to be 10dB. iii) Value of K for phase margin to be 50°. | | | | | | [20] | CO4 | L2 | |
| 4 | For a system $G(s)H(s) = \frac{242(s+5)}{s(s+1)(s^2+5s+121)}$ Sketch the Bode Plot and determine gain margin, phase margin, gain crossover frequency, phase crossover frequency. Comment on stability of the system. | | | | | | [20] | CO4 | L2 | |

CI

CCI

HOD

$$01. \quad G(s)H(s) = \frac{k(s+1)}{s(s-1)(s^2+4s+16)}$$

$$1 + G(s)H(s) = 0$$

$$1 + \frac{k(s+1)}{s(s-1)(s^2+4s+16)} = 0$$

$$s(s-1)(s^2+4s+16) + k(s+1) = 0$$

$$s^4 + 3s^3 + 12s^2 - 16s + ks + k = 0$$

$$s^4 + 3s^3 + 12s^2 + s(k-16) + k = 0$$

Routh's array.

$$\begin{array}{r|rrrr}
 s^4 & 1 & 12 & k & 0 \\
 s^3 & 3 & (k-16) & 0 & 0 \\
 s^2 & \left(\frac{52-k}{3}\right) & k & 0 & 0 \\
 s^1 & \left(\frac{52-k}{3}\right)(k-16) - 3k & 0 & 0 & 0 \\
 s^0 & k & \left(\frac{52-k}{3}\right) & 0 & 0
 \end{array}$$

or stability,

i) From s^0 row; $k > 0$

ii) From s^1 row; $\left(\frac{52-k}{3}\right)(k-16) - 3k > 0$

$$(52-k)(k-16) - 9k > 0$$

$$(52k - 832 - k^2 + 16k - 9k) > 0$$

$$k^2 - 59k + 832 < 0$$

\therefore Roots are $k > 23.315$ & $k < 35.684$

iii) From s^2 row $\frac{52-k}{3} > 0$

$$k < 52$$

$0 < k < 23.315$ - unstable

$23.315 < k < 35.685$ - stable

$k > 35.685$ - unstable

} overall marginally stable.

$$2) G(s)H(s) = \frac{K(s+1)}{s(s-1)(s^2+4s+16)}$$

open-poles at $s = 0, 1, -2 \pm 3.464i, -2 - 3.464i$

$$\therefore P = 4$$

$$Z = -1$$

$P > Z$

$P - Z = 4 - 1 = 3$ branches = N.O. of asymptotes.

Angle of asymptotes $\theta_A = \frac{(2q+1)180^\circ}{P-Z}$

$$\theta_{A_1} = 60^\circ, \theta_{A_2} = 180^\circ, \theta_{A_3} = 300^\circ$$

Centroid $\sigma_A = \frac{\sum R.P. \text{ of poles} - \sum R.P. \text{ of zeros}}{P-Z}$

$$\sigma_A = \frac{0 + 1 - 2 - 2 - (-1)}{3} = -0.6$$

1. For σ_1 between 0 & 1 ; $P_1 + Z_1 = 1 + 0 = 1$ (odd) RL ✓
2. For σ_2 between -1 & 0 ; $P_2 + Z_2 = 2 + 0 = 2$ (even) RL X
3. For σ_3 between $-\infty$ to -1 ; $P_3 + Z_3 = 2 + 1 = 3$ (odd) RL ✓.

Characteristic equation of system

$$1 + G(s)H(s) = 0$$

$$1 + \frac{K(s+1)}{s(s-1)(s^2+4s+16)} = 0$$

$$s^4 + 3s^3 + 12s^2 - 16s + K(s+1) = 0$$

$$K = -\frac{(s^4 + 3s^3 + 12s^2 - 16s)}{(s+1)}$$

$$\frac{dK}{ds} = \frac{(s+1)(-1)(4s^3 + 9s^2 + 24s - 16) + (s^4 + 3s^3 + 12s^2 - 16s)}{(s+1)^2} = 0$$

$$3s^4 + 10s^3 + 21s^2 + 24s - 16$$

$$s = 0.448, -2.26, -0.76 + 2.16i, -0.76 - 2.16i$$

$$\text{Valid points } s = 0.448, -2.26$$

Characteristic equation.

$$s^4 + 3s^3 + 12s^2 - 16s + k = 0$$

Routh's array.

| | | | |
|-------|---------------------------------|--------|-----|
| s^4 | 1 | 12 | k |
| s^3 | 3 | $k-16$ | 0 |
| s^2 | $\frac{52-k}{3}$ | k | 0 |
| s^1 | $\frac{-k^2 + 59k - 832}{52-k}$ | 0 | 0 |
| s^0 | k | 0 | 0 |

$$\frac{-k^2 + 59k - 832}{52-k} = 0 \quad k = 35.68 \quad \& \quad 23.21$$

at $k = 35.68$,

$$s = \pm 2.56j$$

$k = 23.21$,

$$s = \pm 1.56i$$

$$\phi_{P_1} = 180^\circ - \tan^{-1} \frac{3.464}{3} = 130.89^\circ$$

$$\phi_{P_2} = 180^\circ - \tan^{-1} \frac{3.464}{2} = 120^\circ$$

$$\phi_{P_3} = 90^\circ$$

$$\phi_{Z_1} = 106.11^\circ$$

$$\phi = 234.78^\circ$$

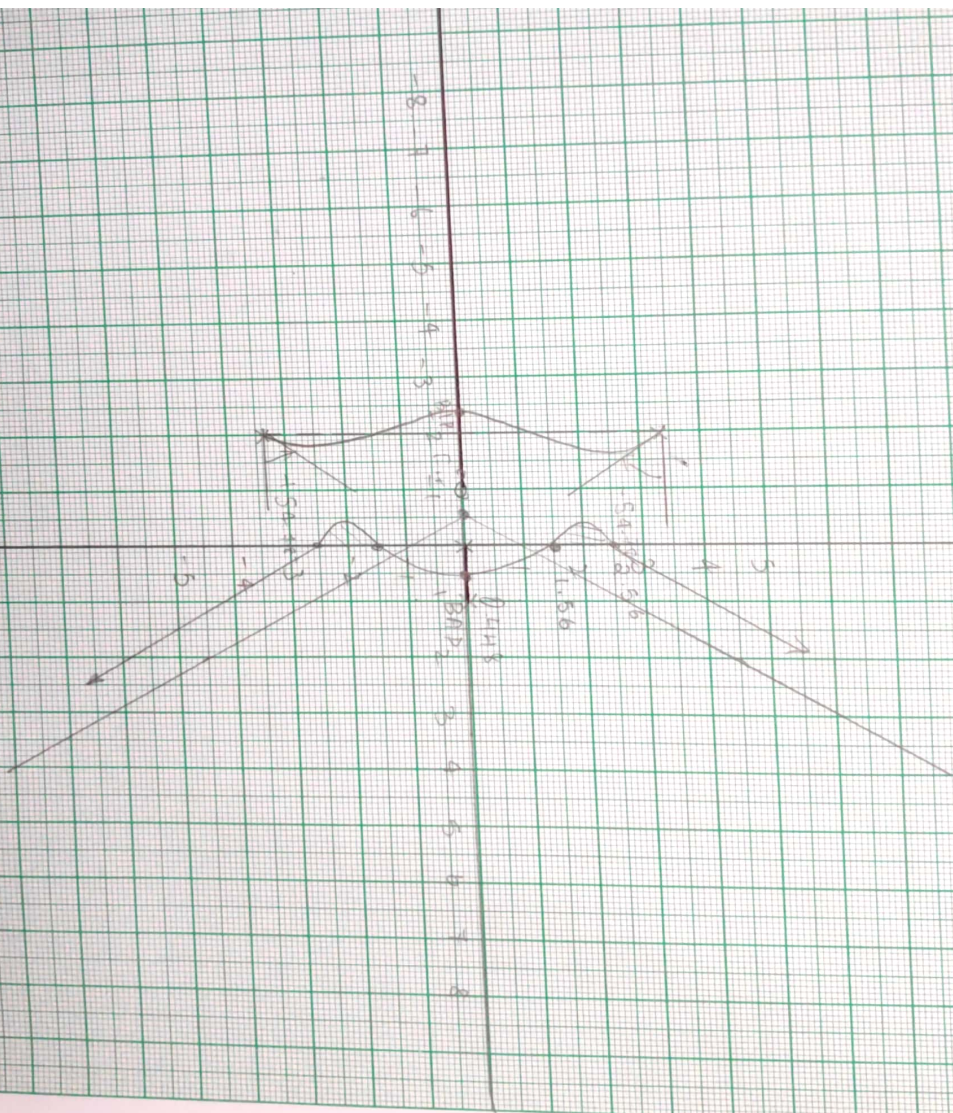
$$\sum \phi_p = 340.89^\circ$$

Angle of departure: $180 - 234.78$

$$\sum Z = 106.11^\circ$$

$$= -54.78 \text{ at } -2 + 3.464i$$

$$+ 54.78 \text{ at } -2 - 3.464i$$



$$G(s) = \frac{k}{s(s+a)(s+a)}$$

From standard form $G(s)H(s) = \frac{k}{s(s+a)(s+a)}$

Here $H(s) = 1$.

$$G(s)H(s) = \frac{k}{40s(1+\frac{1}{20}s)(1+\frac{1}{20}s)} = \frac{k}{40s(1+0.05s)(1+0.05s)}$$

$$G(i\omega)H(i\omega) = \frac{A}{i\omega(1+0.05i\omega)(1+0.05i\omega)} \quad \text{where } \frac{k}{40} = A$$

$$20 \log |G(i\omega)H(i\omega)| = 20 \log A - 20 \log \sqrt{1+(0.05\omega)^2} - 20 \log \sqrt{1+(0.05\omega)^2}$$

$$\omega_{c1} = \frac{1}{0.05} = 2 \text{ rad/s} \quad \omega_{c2} = \frac{1}{0.05} = 20 \text{ rad/s}$$

| Range | Slope in (dB/decade) |
|---------|----------------------|
| 0.1 - 2 | -20 |
| 2 - 20 | -40 |
| 20 - ∞ | -60 |

Phase table.

| ω | $\frac{1}{i\omega}$ | $\frac{1}{(1+0.05i\omega)}$ | $\frac{1}{(1+0.05i\omega)}$ | $\sum \theta_R$ |
|----------|---|---|---|-----------------|
| 0.2 | $-\tan^{-1}\left(\frac{\omega}{0}\right)$ | $-\tan^{-1}\left(\frac{0.05\omega}{1}\right)$ | $-\tan^{-1}\left(\frac{0.05\omega}{1}\right)$ | -96.28 |
| 0.8 | -90 | -5.71 | -0.57 | -114.09 |
| 2 | -90 | -21.8 | -2.29 | -140.71 |
| 10 | -90 | -45 | -5.71 | -195.25 |
| 20 | -90 | -78.69 | -26.56 | -219.28 |
| 100 | -90 | -84.28 | -45 | -257.54 |
| ∞ | -90 | -88.85 | -78.69 | -270 |

$$i) 20 \log A < 28$$

$$\log A < 1.4$$

$$A < 10^{1.4}$$

$$A < 25.11$$

$$K < 25.11 \times 40 = \underline{1004.75^\circ}$$

(ii) For gain margin to be 10dB

$$28\text{dB} - 10 = 18\text{dB}$$

$$20 \log A < 18$$

$$A < 7.943$$

$$K < \underline{317.79^\circ}$$

For phase margin to be 50°

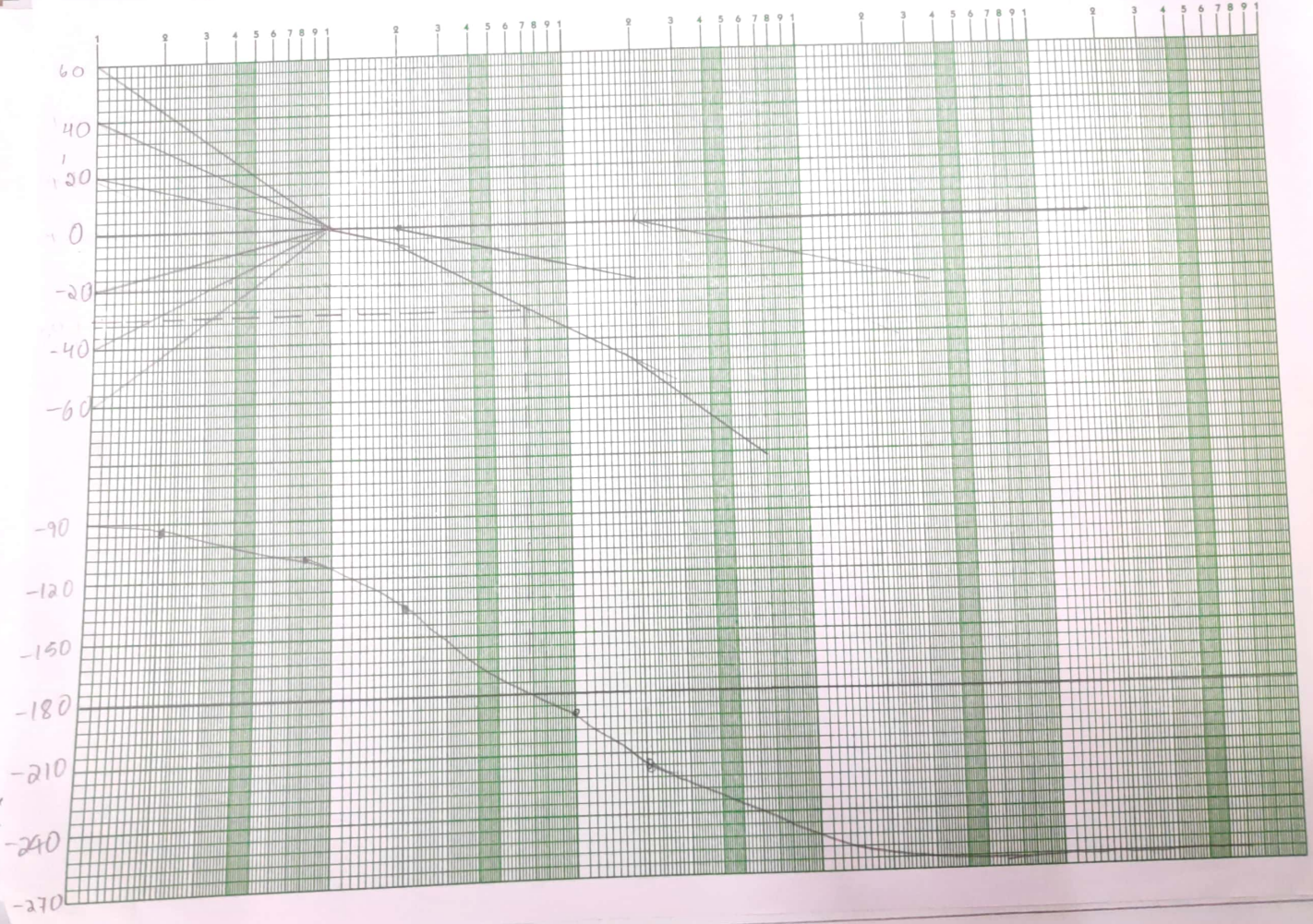
$$20 \log A < 6$$

$$A < 1.995$$

$$K < \underline{79.81^\circ}$$

2)

SEMI-LOG PAPER (5 CYCLES x 1/10)



$$(s)H(s) = \frac{48.4(1+0.2iw)}{i\omega(1+i\omega)(1+0.04i\omega - 8.26 \times 10^{-3}\omega^2)}$$

$$20 \log |G(i\omega)| = 20 \log 48.4 + 20 \log \sqrt{1+(0.2\omega)^2} - 20 \log \omega - 20 \log \sqrt{1-8.26 \times 10^{-3}\omega^2 + (0.04\omega)^2}$$

Corner frequencies $\omega_c = \frac{1}{0.2} = 5 \text{ rad/s}$

$\omega_{c2} = \frac{1}{0.04} = 25 \text{ rad/s}$ $\omega_{c3} = 16 \text{ rad/s}$
 phase margin = -30

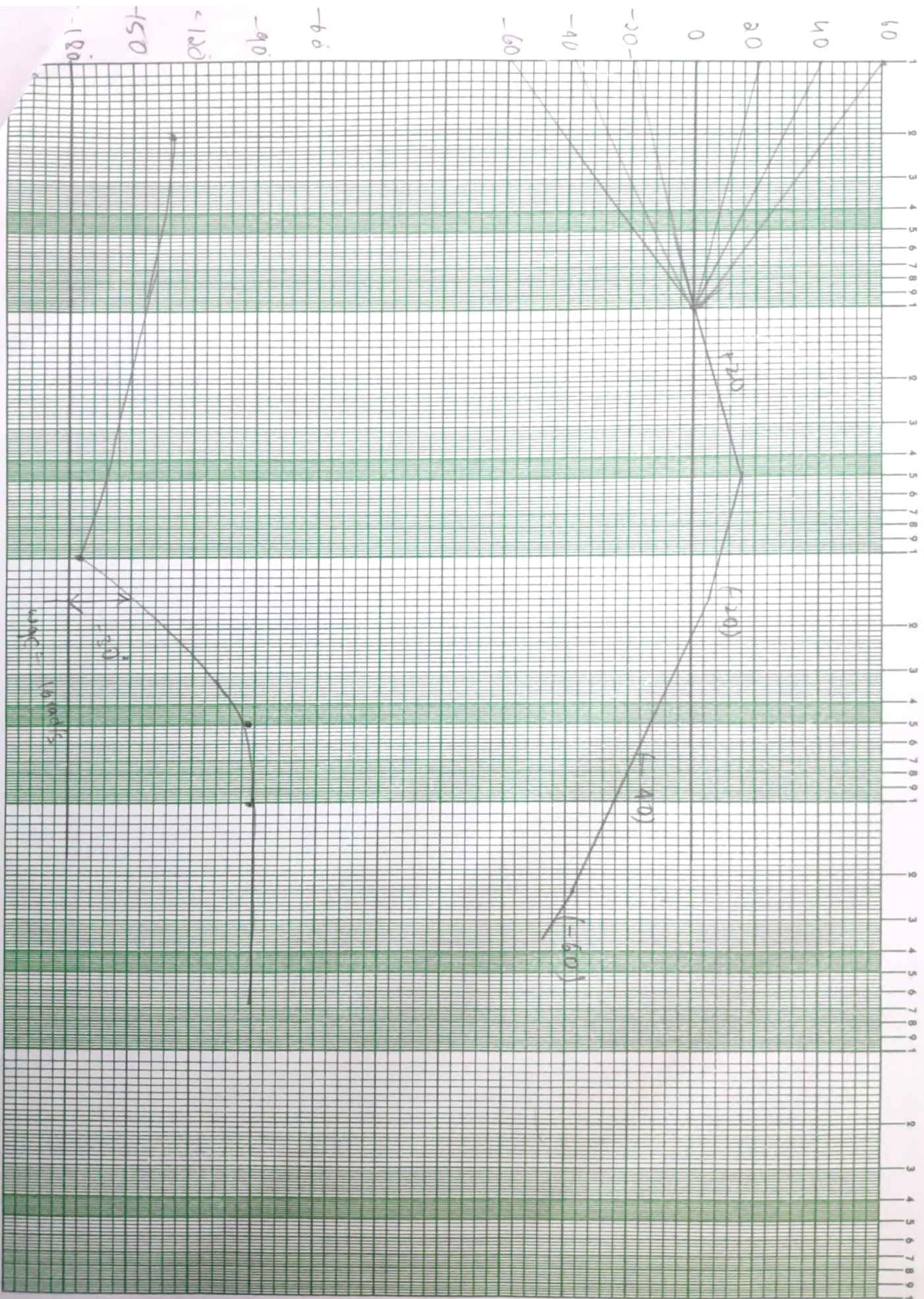
Now, $\frac{1}{\omega_n^2} = 8.26 \times 10^{-3}$

$\omega_n = 11 \text{ rad/s} = \omega_{c3}$
 Slope (dB/dec)

| | |
|-------|-----|
| 0-5 | 20 |
| 5-11 | -20 |
| 11-25 | -40 |
| 25-∞ | -60 |

$$\phi = \tan^{-1} \left[\frac{2\xi\omega}{1 - \left(\frac{\omega}{\omega_n}\right)^2} \right]$$

| ω | $\frac{1}{i\omega}$ | $\tan^{-1} \left(\frac{\omega}{0} \right)$ | $+\tan^{-1} \left(\frac{0.2\omega}{1} \right)$ | $-\tan^{-1} \left(\frac{\omega}{1} \right)$ | $-\tan^{-1} \left(\frac{0.04\omega}{1 - \left(\frac{\omega}{16}\right)^2} \right)$ | ϕ_R |
|----------|---------------------|---|---|--|---|----------|
| 0.2 | -90 | | 2.29 | -11.303° | -0.45° | -99.9 |
| 10 | -90 | | 63.43 | -84.28° | -66.54° | -177 |
| 50 | -90 | | 84.28 | -88.85° | 5.8° | -88 |
| 100 | -90 | | 87.137 | -89.427° | 2.8° | -89.99 |
| ∞ | -90 | | 90 | -90 | 0 | -90 |



SEMI-LOG PAPER (5 CYCLES x 1/10)