| USN |  |  |  |  |  |
|-----|--|--|--|--|--|

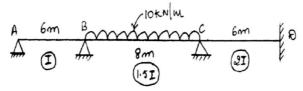


## Internal Assessment Test 1 – Nov. 2021

| Sub:  | Analysis of Indeterminate Structures |           |          |            |  | Sub Code:  | 18CV52 | Branch: | Civil |
|-------|--------------------------------------|-----------|----------|------------|--|------------|--------|---------|-------|
| Date: | 11/11/2021                           | Duration: | 90 min's | Max Marks: |  | Sem / Sec: | 5A     |         | OBE   |

## **Answer TWO FULL Questions**

Analyze the continuous beam shown in fig 1. using the slope deflection method. Sketch BMD and SFD. support B and C settles by 8mm and 5mm respectively,  $EI=20000kN/m^2$ 



1.

| Step 1 % Fixed end Moments   |
|--|
| MFAB = OKNM MFBC = -53.34 KNM<br>MFBA = OKNM MFCB = 53.34 KNM  |
| MFCD = 0 KNM A 6M B WC 6M ED  MFDC = 0 KNM (I) M 8m M (II)   |
| Step 2 : Slope deflection egn; 8 = 8×10-3  |
|  |
| MAB = 0.667 EIOA + 0.334 EIOB - 1.334 X 10 EI-   |
| $MBA = MFBA + 2EI \left[20_B + 0_A - \frac{38}{1}\right]$  |
| $= 0 + 2EI \left[ 20_B + 8_A - 3(8 \times 10^{-3}) \right]$  |
| $MBA = 0.669 EIBB + 0.334 EIBA - 1.334 X10 EI$ $L \bigcirc $ $FOR Span BC$                               |
| $MBC = MFBC + 2EI \left[20B + 0c - \frac{38}{2}\right]$  |
| $= -53.33 + 2E(1.5I) (208+0c-3(-3×10-3))$ $8$ $M_{BC} = -53.33 + 0.75EID_{B} + 0.395EID_{c} + 4.21×10-4$ |
|  |

MCB = MFCB + 2EI 20c+0B-38 53.33 + DE (1.51) [20c +0B-3(-3X163) 53.33 + 0.75EIOc + 0.375EI OB+ 4.218×10-4  $M_{CD} = 1.334 EIO_{c} + 1.667 \times 10^{-3}$ MFDC + DEI (200+0c-38  $0 + 2E(2I) \left[ 0_{c} - 3(-5x)^{-3} \right]$ 0.667 EIOC+ 1.667 × 103 EI 0.667EIOB+ 0.334 EIOA-1.334 X 10-3EI -53.33 + 0.95 EIOB + 0.375 EIOC + 4.218 X 104 EI

m

| -71.574 + 0.334 EIOA + 1.417EIOB + 0.375EIOC  |
|---|
| @ Joint "C", MCB + MCB =0   |
| $53.33 + 0.75 EID_C + 0.375 EID_B + 4.218 \times 10^{-4} + 1.834 EID_C + 1.667 \times 10^{-3} EI = 0$ |
| 95.09 + 2.084 EIOC + 0.375 EIOB - 8   |
| @ Joint "D", MDC = 0  |
| 0.667EIOC+ 1.667 X103 EI = 0  |
| 0.667 EIOc + 33.34 - 9  |
| $ \Theta_{A} = 167.7 $ $ \Theta_{B} = 24.21 $ $ \Theta_{C} = -49.98 $ $ EI$                           |
| Step 4: Final Moments   |
| MAB = 93.26 KN·m Mcb = -33.36 KN m  |
| MBA = 45.47 KN.M MDC = 0 KNM<br>MBC = -45.47 KNM  |
| McB = 33.36 KNm   |

SHIP

recurana. H

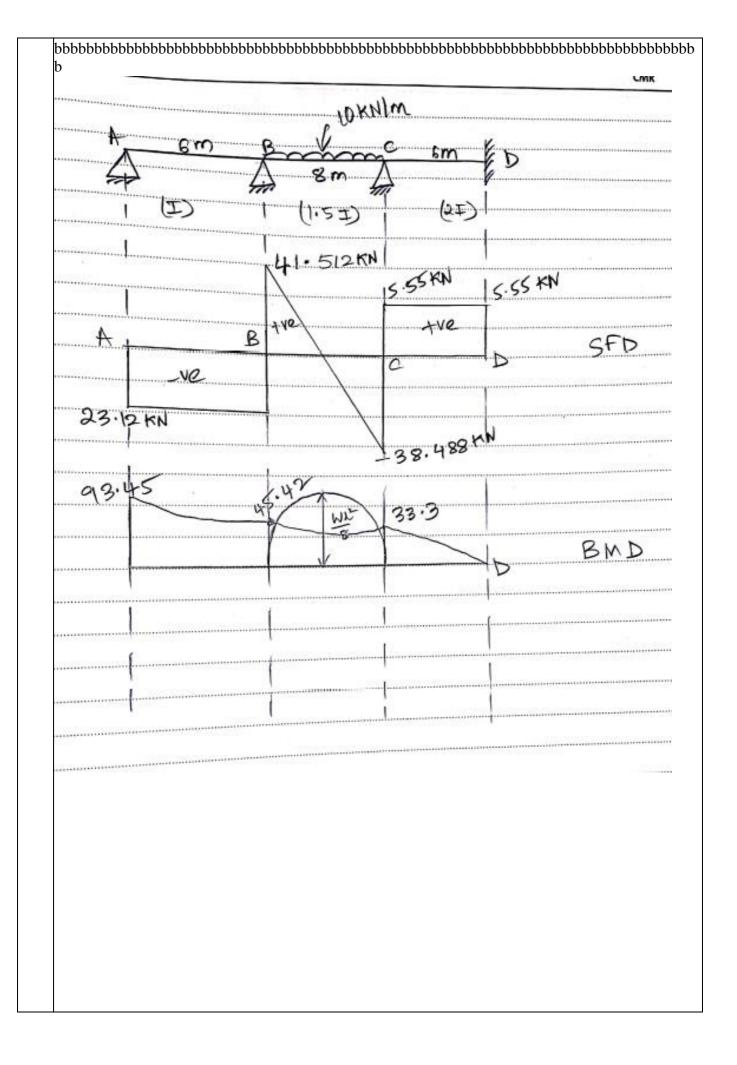
Step 5: SFD & BMD

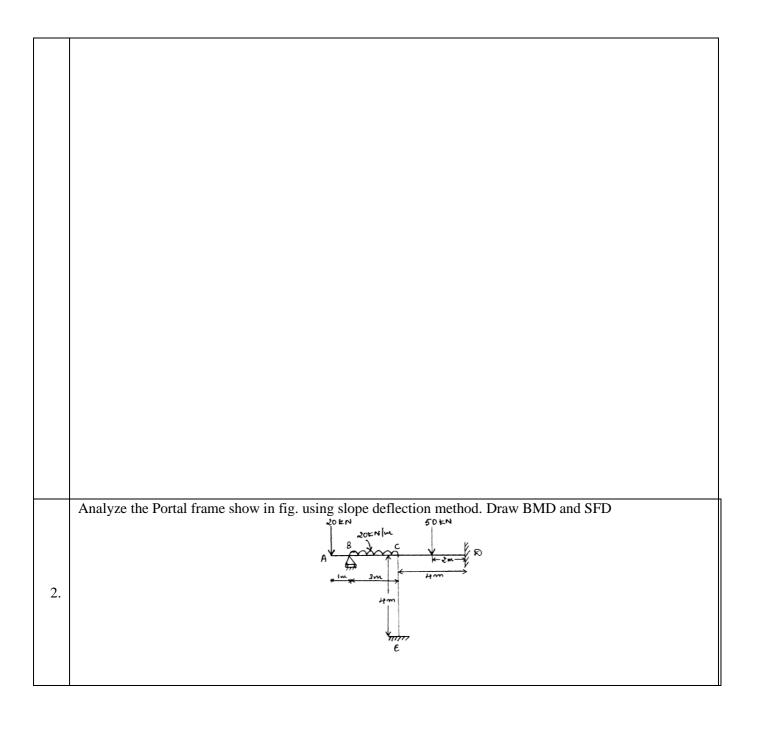
V4 + VB + VC + VD = 80 KN

VAX6 +93-266+45-47

-VD X 6-33.35 = 0 Vb = 5.55 KN

VAX14-10X8X4+93.262+33.35+VBX8





| (1) TREATE   | reerthana. H  |
|--|---|
| Step 2: Slope 1.10 F   | CMR   |
| aefrection equa  | ten grande so. I                                      |
| Step 2: Slope deflection equa  | 1000 1000 1747  |
| For span OBC, L=3m   |   |
| $\lambda = 3 \text{ m}$  | 1 77M M   |
|  | 0   |
| MBC = MFBC + 2EI (20B+0C-  |   |
| 208 TOC -  | 38 ) 3 7 7 1  |
| 2 - 15   | / [ ]   |
| $= -15 + 2EI \left[ 20_3 + 0_2 \right)$  | 1.4   |
| 3 (208100)   | DATM - CAN  |
| Maa  |   |
| MBC = -15 + 0.667 EID + 192  | CTA A   |
| MBC = -15 + 0.667 EIDc + 1.33  | EIUB -U   |
| Mag Ma   | 20  |
| 11CB = MIFCB + 2EI (20+00.   | -38   |
| McB = MFCB + 2EI (20c+0B.  | 1   |
| - 15 + 05 F COO 107  |   |
| = 15 + 2EI [20c+0B]  |   |
| Maria Maria Maria Maria Fore   | 1: 8 8 ext - 1111                                     |
| MCB = 15 + 1.330 EE + 0.000  | 1 ET 0 - (D)  |
| MCB = 15 + 1.330CEI + 0.665  | TELOB — E   |
| - The state of the | 7911 + 471  |
| For span CD, l = 4m  |   |
| Mark the state of  | 2 0   |
| McD = Mfcb + 2EI (202+0)   | 26X   |
| 111CD -1 ZEI (20c+0)   | - 38)   |
|  | $\left[\begin{array}{c} O_{D} = 0 \end{array}\right]$ |
| = -25"+2EI (20c)   | 10 N 4- 11  |
| 4  |   |
| Marie G  | 7   |
| MCD - 1-25 + 6 E1 - 3  | )   |
| 20   | 20  |
| MAG MOG + DET 10AL+A.  | - 381   |
| 1110C = 11+DC - ZET (29D 100   | - <del>/L</del> )                                     |
| OI - C OI -   | 2/ 57 OF 31 1   |
| = 25 + 2EI(0c)   |   |
| 14 1 L   | Vilale Nallocal I                                     |
|  | $-\omega$   |
| $MDC = 25 + 0.5 EI \theta_c$   | — ( <del>+)</del>                                     |
| 28 S 4 S 1 1 1 1 S C 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2   | - 1   |
|  |   |

For span CE, l= 4m MCE = MFCE + 2EF (20c+06-38)  $MCE = 0 + EIO_C - G$ MFEC + 2EI (20E+Oc-38) 0+ 2EI (Oc) 0.5 EIOc -6 11) Step 3: Toint Equilibrium Condition MBA + MBC = 0 @ Joint B 20+ (-15)+0.669EIOc+ 1.33EIOp=0 1.33 EIOB + 0.669 EIOC = -5 -(7) MCB + MCD + MCE @ Joint C 15 + 1.33 EIOC + 0.66 FEIOB - 25 + EIOC + EIOc = O 0.667EIOB + 3.33EIOc = 10 - (8) : By Solving eq (7) & (8), we get  $\theta_{R} = -5.833$   $\theta_{C} = 4.167$