18CV54 - BASIC GEOTECHNICAL ENGINEERING



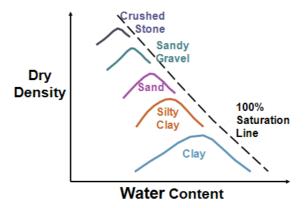
1 (a) Explain the factors affecting compaction.	[06]
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Any 4 factor with sketches - 4

The factors which affect the degree of compaction are given below.

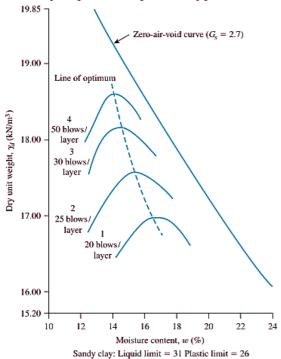
1. Type of soil

Normally, heavy clays, clays & silts offer higher resistance to compaction where as sandy soils and coarse grained or gravelly soils are amenable for easy compaction.



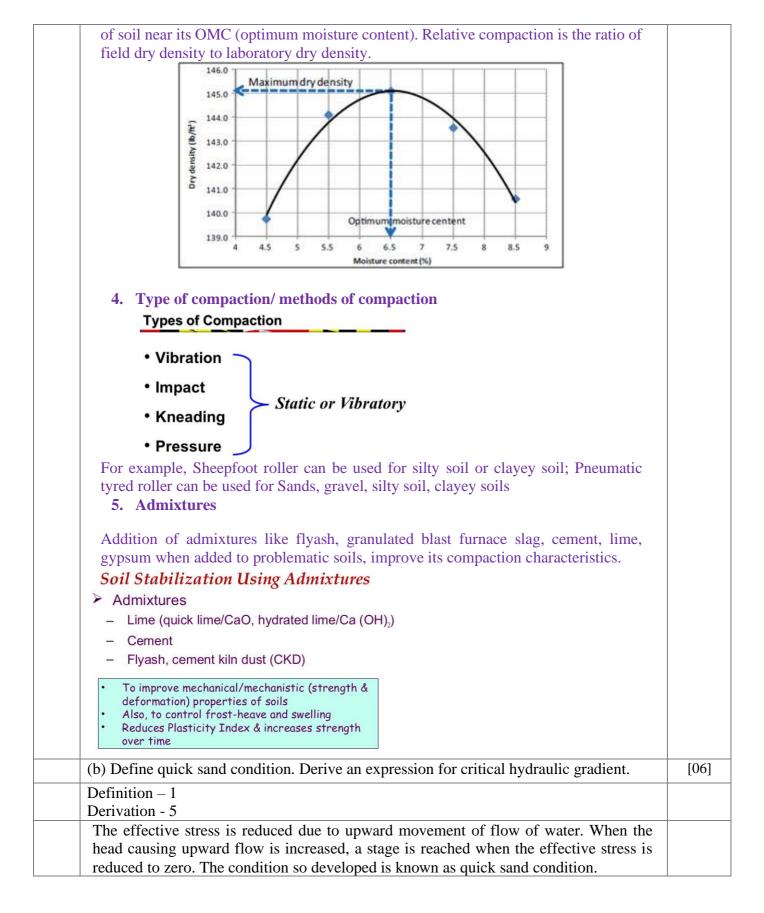
2. Amount of compaction

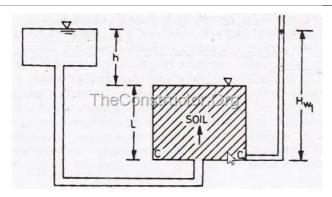
This is dependent on the type of compacting equipment, layer thickness, layer lifts, roller passes etc. Greater the compactive effort, greater will be the compaction energy, greater will be the extent of compaction. Type of compaction equipment to be used is mainly dependent upon the type of soil to be compacted.



3. Moisture content/ water content

Proper control of moisture content in soil is necessary for achieving desired density. Maximum density with minimum compacting effort can be achieved by compaction





From the above figure

$$\sigma' = \sigma - u$$

$$\sigma' = \gamma_{sat} L - \gamma_w H_{w1}$$

$$\sigma' = \gamma_{sat} L - \gamma_w h - \gamma_w L$$

$$\sigma' = \gamma_{sub} L - \gamma_{w} h$$

When effective stress becomes equal to 0, $\sigma' = \gamma_{sub} L - \gamma_{wh}$ or

$$h/L = \gamma_{sub} / \gamma_{w}$$
 (1)

$$\gamma_{\text{sub}} = \gamma_{\text{sat}} - \gamma_{\text{w}} \tag{2}$$

But
$$\gamma_{sat} = \frac{\gamma_w(G+eS)}{1+e} = \frac{\gamma_w(G+e)}{1+e}$$

Therefore, $\gamma_{\text{sub}} = \gamma_{\text{sat}} - \gamma_{\text{w}}$

$$\gamma_{\text{sub}} = \frac{\gamma_w(G+e)}{1+e} - \gamma_w = \frac{\gamma_w[G+e-1-e]}{1+e} = \frac{\gamma_w(G-1)}{1+e}$$
 (3)

Substituting (3) in (1)
$$\frac{h}{L} = \frac{\gamma_{sub}}{\gamma_w} = \frac{\gamma_w(G-1)}{1+e} \times \frac{1}{\gamma_w} = \frac{(G-1)}{1+e} = i_c$$

This ic is called as critical hydraulic gradient

(c) List the merits of triaxial shear test over direct shear test.

[80]

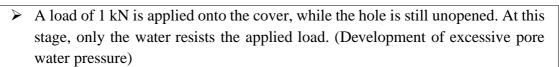
Any 5 points @ 1.5 marks/each

Direct shear tests are generally suitable for cohesionless soils except fine sands and silts whereas triaxial tests are suitable for all types of soils and tests.

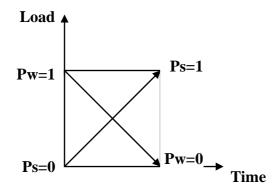
Advantages of triaxial test over direct shear test

- The stress distribution across the soil sample is more uniform in a triaxial test as compared to a direct shear test.
- Measurement of volume changes are accurate in triaxial test.complete state of stress condition is known only at failure. The conditions prior to failure are indeterminate and, therefore, the mohr circle cannot be drawn.
- Complete state of stress is known at all stages during the triaxial test, whereas stresses at failure are known in direct shear test.
- In case of triaxial shear, the sample fails along a plane on which the combination of normal and shear stress gives the maximum angle of obliquinity of the resultant with the normal, whereas in the case of direct shearm the sample is sheared only on one horizontal plane which may not be the actual failure plane.
- Control on the drainage conditions is very difficult in direct shear test whereas it is easy in triaxial test.
- The measurement of pore water pressure is not possible in direct shear test whereas it is possible in triaxial test.

	The side walls of the shear box cause lateral restraint on the specimen and do not	
	allow it to deform laterally. But in triaxial tests, the latex membrane makes the	
	specimen flexible in lateral directions too.	
2	(a) Considering soil as a three-phase system, derive the relationship,	[06]
	$\gamma_{\rm d} = \frac{G\gamma_{\rm w}}{1+e}$	
	Figure -2	
	Derivation - 4	
	$e = \frac{V_{\nu}}{V_{\rm S}}$	
	Assume $V_s=1$, then, $e=\frac{V_v}{1}$ or $V_v=e$ Volume Weight	
	Therefore, $V=V_v+V_s=e+1$ $V_v V_a Air V_a O$ $W_a=0$	
	$\rho_b = \frac{M}{V} = \frac{M_s + M_w}{1 + e} = \frac{G\rho_w V_s + \rho_w V_w}{1 + e} \qquad \qquad V \qquad \bigvee_{w} \qquad \bigvee$	
	$S = rac{V_w}{V_v} = rac{e_w}{e}$ Solid W_s	
	$\operatorname{Or} V_{w} = e_{w} = eS$	
	Since $Vs=1$ and $V_w = eS$,	
	$\rho_b = \frac{M}{V} = \frac{M_s + M_w}{1 + e} = \frac{G\rho_w + \rho_w eS}{1 + e}$	
	For an oven dried soil, S=0	
	Hence dry density, ρ_d can be obtained as	
	$\rho_d = \frac{G\rho_W}{1+e}$	
	In SI units, when ρ_d becomes γ_d and ρ_w becomes γ_w	
	Therefore $\rho_d = \frac{G\rho_w}{1+e}$ becomes $\gamma_d = \frac{G\gamma_w}{1+e}$	
	(b) Explain mass spring analogy of consolidation of soils.	[06]
	Spring analogy – Fig – 2	
	Explanation - 4 The consolidation process is often explained with an idealized system composed of a	
	spring, a container with a hole in its cover, and water.	
	1 2 3 4	
	In this system, the spring represents the compressibility or the structure itself of the soil, and the water which fills the container represents the pore water in the soil. The container is completely filled with water, and the hole is closed. (Fully saturated soil)	



- As soon as the hole is opened, water starts to drain out through the hole and the spring shortens. (Drainage of excessive pore water)
- After some time, the drainage of water no longer occurs. Now, the spring alone resists the applied load. (Full dissipation of excessive pore water pressure. End of consolidation)



(c) Derive expression for average permeability of stratified soils when flow is parallel and perpendicular to the direction of stratification.

[08]

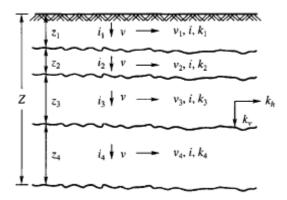
Flow parallel – 4

Flow perpendicular - 4

When a soil deposit consists of a number of horizontal layers having different permeabilities, the average value of permeability can be obtained separately for both vertical flow and horizontal flow, as \mathbf{k}_{V} and \mathbf{k}_{H} respectively.

Consider a stratified soil having 3 horizontal layers of thickness z_1 , z_2 , z_3 and z_3 with coefficients of permeability k_1 , k_2 , k_3 and k_4 .

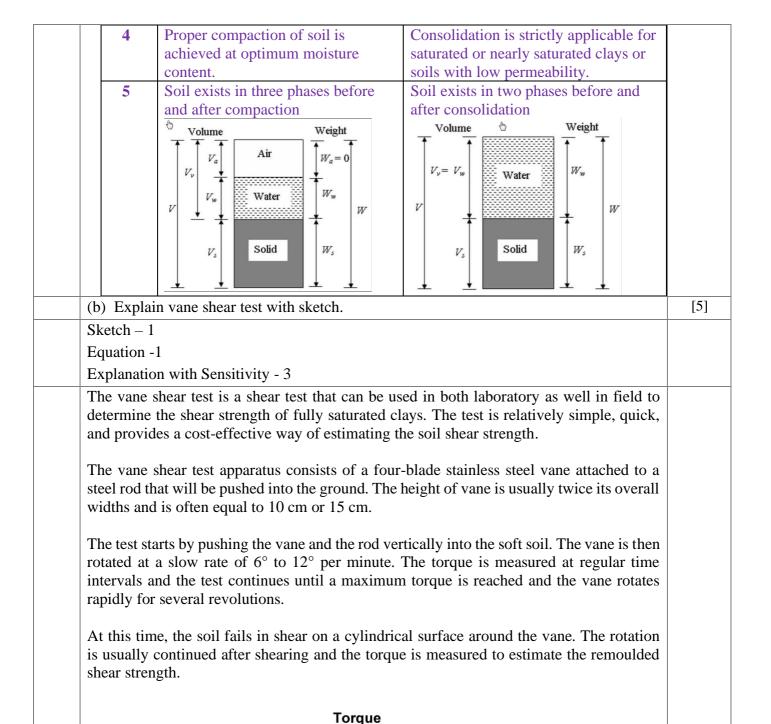
Flow parallel to bedding planes



In this case discharge $kiA = Q = Q_1 + Q_2 + Q_3 + Q_4$

But head causing flow remains same; i.e., hydraulic gradient remains same.

 $k_H \times i \times Z \times 1$ $=k_1\times i\times z_1\times 1+k_2\times i\times z_2\times 1+k_3\times i\times z_3\times 1+k_4\times i\times z_4\times 1$ Or $k_H \times Z = k_1 \times z_1 + k_2 \times z_2 + k_3 \times z_3 + k_4 \times z_4$ Or $k_{H} = \frac{k_{1} \times z_{1} + k_{2} \times z_{2} + k_{3} \times z_{3} + k_{4} \times z_{4}}{7}$ Flow perpendicular to bedding planes In this case $Q = Q_1 = Q_2 = Q_3 = Q_4$ $or v = v_1 = v_2 = v_3 = v_4$ $k_{v} \times i = k_{1} \times i_{1} = k_{2} \times i_{2} = k_{3} \times i_{3} = k_{4} \times i_{4}$ or $i_1 = \frac{k_v \times i}{k_1}$; $i_2 = \frac{k_v \times i}{k_2}$; $i_3 = \frac{k_v \times i}{k_2}$; $i_4 = \frac{k_v \times i}{k_4}$; or Total head loss = sum of head loss in each layer $h = i \times z$ $h = h_1 + h_2 + h_3 + h_4$ or $i \times Z = \frac{k_v \times i}{k_1} \times z_1 + \frac{k_v \times i}{k_2} \times z_2 + \frac{k_v \times i}{k_3} \times z_3 + \frac{k_v \times i}{k_4} \times z_4$ $Z = k_v \left[\frac{Z_1}{k_1} + \frac{Z_2}{k_2} + \frac{Z_3}{k_3} + \frac{Z_4}{k_4} \right]$ $Or k_v = \frac{Z}{\left[\frac{Z_1}{k_1} + \frac{Z_2}{k_2} + \frac{Z_3}{k_3} + \frac{Z_4}{k_4}\right]}$ 3 (a) Differentiate between compaction and consolidation. [5] 5 differences with sketch - 5 **Compaction Consolidation** SI No Compaction is the process by 1 Consolidation is the process by which which solid soil particles are soil particles are packed more closely together under the application of static packed more closely together by mechanical means. loading It is achieved through reduction of It is achieved through gradual 2 air voids. drainage of water from soil pores. It is a rapid and artificial process. It is a gradual and natural process. In 3 Applicable to cohesive and some soils it takes many years. cohesionless soils. Applicable to cohesive soils



Vane

Shear surface

Undrained shear strength,
$$c_u = \frac{T}{\pi d^2 \left[\frac{H}{2} + \frac{d}{6} \right]}$$

Where T is the torque in kgcm
D is the overall diameter of the vane in cm
H is the height of vane in cm

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