

Internal Assessment Test-II							
Sub:	Electromagnetic Waves	Code:	18EC55				
Date:	20/12/2021	Duration:	90 mins	Max Marks:	50	Sem:	5th
		Branch:	ECE(A,B,C,D)				
Solutions							

OBE

Marks CO RBT

[10] CO2 L2

1. Derive Maxwell's equation of electrostatics  $\nabla \cdot \mathbf{D} = \rho_V$ .

Divergence of a Vector & Divergence theorem: from Gauss's law:

Net outward flux  $\psi = \oint_S \mathbf{D} \cdot d\mathbf{s}$

$\psi = \oint_S \mathbf{D} \cdot d\mathbf{s} = Q_{enc}$

**Definition of divergence**

Divergence of  $\mathbf{D}$  is defined as the net outward flux per unit Volume as the volume shrinks to zero

$$\text{div } \mathbf{D} = \nabla \cdot \mathbf{D} = \lim_{\Delta V \rightarrow 0} \frac{\oint_S \mathbf{D} \cdot d\mathbf{s}}{\Delta V}$$

It gives the measure of how much the field diverges or emanates from that point.

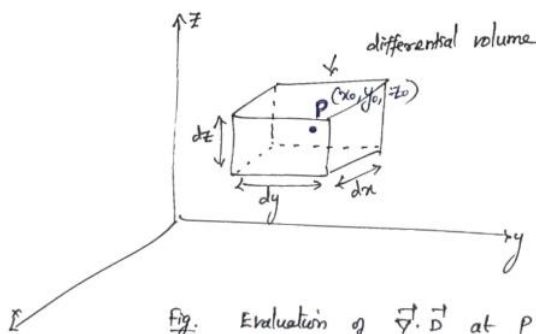


Fig: Evaluation of  $\nabla \cdot \mathbf{D}$  at  $P(x_0, y_0, z_0)$

$$\oint_S \mathbf{D} \cdot d\mathbf{s} = \left( \iint_{\text{front}} + \iint_{\text{back}} + \iint_{\text{left}} + \iint_{\text{right}} + \iint_{\text{top}} + \iint_{\text{bottom}} \right) \mathbf{D} \cdot d\mathbf{s}$$

Three dimensional Taylor series expansion of  $D_x$  at  $P$ ,

$$D_x(x, y, z) = D_x(x_0, y_0, z_0) + (x-x_0) \left. \frac{\partial D_x}{\partial x} \right|_P + (y-y_0) \left. \frac{\partial D_x}{\partial y} \right|_P + (z-z_0) \left. \frac{\partial D_x}{\partial z} \right|_P + \text{higher order terms}$$

For the front side,

$$x = x_0 + \frac{dx}{2} \quad \hat{s} = dy dz \vec{ax}$$

$$\iint_{\text{front}} \vec{D} \cdot d\vec{s} = \left[ D_x(x_0, y_0, z_0) + \frac{dx}{2} \frac{\partial D_x}{\partial x} \Big|_P \right] [dy dz] + \text{higher order terms}$$

For the back side,

$$x = x_0 - \frac{dx}{2} \quad \hat{s} = dy dz (-\vec{ax})$$

$$\iint_{\text{back}} \vec{D} \cdot d\vec{s} = \left[ D_x(x_0, y_0, z_0) - \frac{dx}{2} \frac{\partial D_x}{\partial x} \Big|_P \right] [-dy dz] + \text{higher order terms}$$

Hence, 
$$\iint_{\text{front}} \vec{D} \cdot d\vec{s} + \iint_{\text{back}} \vec{D} \cdot d\vec{s} = dx dy dz \frac{\partial D_x}{\partial x} \Big|_P + \text{higher order terms}$$

By taking similar steps,

$$\iint_{\text{left}} \vec{D} \cdot d\vec{s} + \iint_{\text{right}} \vec{D} \cdot d\vec{s} = dx dy dz \frac{\partial D_y}{\partial y} \Big|_P + \text{higher order terms}$$

and

$$\iint_{\text{top}} \vec{D} \cdot d\vec{s} + \iint_{\text{bottom}} \vec{D} \cdot d\vec{s} = dx dy dz \frac{\partial D_z}{\partial z} \Big|_P + \text{higher order terms}$$

$$\lim_{\Delta V \rightarrow 0} \frac{\oiint_S \vec{D} \cdot d\vec{s}}{\Delta V} = \left( \frac{\partial D_x}{\partial x} + \frac{\partial D_y}{\partial y} + \frac{\partial D_z}{\partial z} \right) \Big|_{\text{at } P} \quad \Delta V = dx dy dz$$

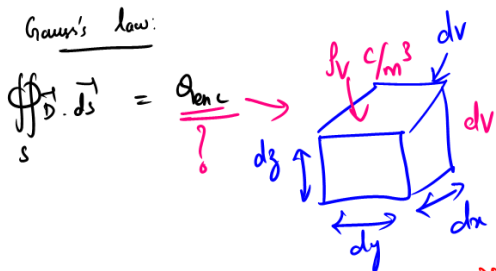
higher order terms will vanish as  $\Delta V \rightarrow 0$ .

$$\vec{\nabla} \cdot \vec{D} = \frac{\partial D_x}{\partial x} + \frac{\partial D_y}{\partial y} + \frac{\partial D_z}{\partial z} \quad (\text{Rectangular / Cartesian})$$

similar expressions can be obtained for other co-ordinate systems,

Cylindrical: 
$$\vec{\nabla} \cdot \vec{D} = \frac{1}{\rho} \frac{\partial}{\partial \rho} (\rho D_\rho) + \frac{1}{\rho} \frac{\partial D_\phi}{\partial \phi} + \frac{\partial D_z}{\partial z}$$

Spherical: 
$$\vec{\nabla} \cdot \vec{D} = \frac{1}{r^2} \frac{\partial}{\partial r} (r^2 D_r) + \frac{1}{r \sin \theta} \frac{\partial}{\partial \theta} (\sin \theta D_\theta) + \frac{1}{r \sin \theta} \frac{\partial D_\phi}{\partial \phi}$$



$$LHS = \oint_S \vec{D} \cdot d\vec{s} = dx dy dz \left[ \frac{\partial D_x}{\partial x} + \frac{\partial D_y}{\partial y} + \frac{\partial D_z}{\partial z} \right]$$

+ higher order terms

$$RHS = Q_{enc} = \iiint \rho_v dv$$

where  $\rho_v = \lim_{\Delta v \rightarrow 0} \left( \frac{\Delta Q}{\Delta V} \right)$

$$\oint_S \vec{D} \cdot d\vec{s} = Q_{enc} = \iiint \rho_v dv$$

Gauss law for a closed surface

Integral form of Gauss's law

Definition of Divergence

$$\vec{\nabla} \cdot \vec{D} = \lim_{\Delta v \rightarrow 0} \frac{\oint_S \vec{D} \cdot d\vec{s}}{\Delta V}$$

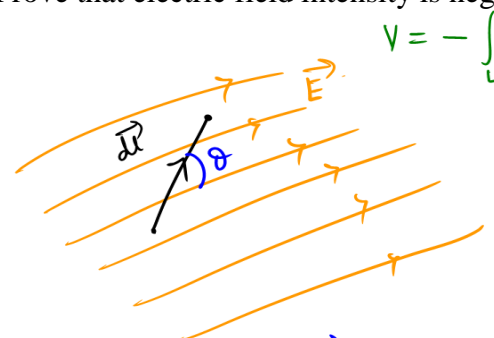
$$\lim_{\Delta v \rightarrow 0} \frac{\oint_S \vec{D} \cdot d\vec{s}}{\Delta V} = \lim_{\Delta v \rightarrow 0} \left( \frac{Q_{enc}}{\Delta V} \right)$$

$$\vec{\nabla} \cdot \vec{D} = \rho_v$$

Gauss's law at a point (Differential) form of Gauss's law

2.(a) Prove that electric field intensity is negative gradient of potential.

[04] CO3 L2



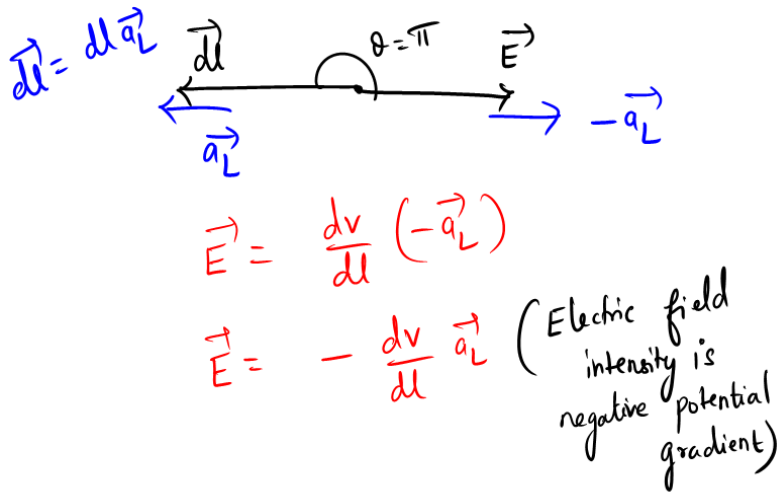
$$V = - \int_L \vec{E} \cdot d\vec{l}$$

$$dV = - \vec{E} \cdot d\vec{l}$$

$$dV = - |\vec{E}| |d\vec{l}| \cos \theta$$

$$|\vec{E}| \cos \theta = - \left| \frac{dV}{dl} \right|$$

$$|\vec{E}|_{max} = \left| \frac{dV}{dl} \right|_{max} \text{ occurs at } \theta = \pi$$



$\vec{E} = - \text{grad } V$  (m)

$\vec{E} = - \vec{\nabla} V$

2.(b) Define current and current density. Derive continuity of current equation.

[06] CO2 L2

Current and Current Density:

Electric charges in motion  $\rightarrow$  current (Ampere (A)).

Rate of movement of charge passing a given reference point (or crossing a reference plane).

$\downarrow$   
 1 c/s = 1 Ampere.

$I = \frac{dq}{dt}$  ← movement of positive charges

Current density  $\rightarrow$  vector  $\rightarrow \vec{J}$  A/m<sup>2</sup>

Increment of current  $\Delta I$ , crossing an incremental surface  $\Delta S$ , normal to the current density

$\Delta I = \vec{J}_N \cdot \Delta S$

If  $\vec{J}$  is not  $\perp$  to surface

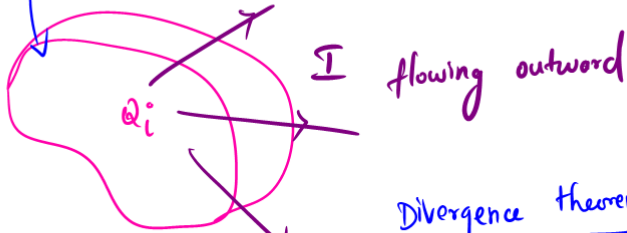
$\Delta I = \vec{J} \cdot \Delta \vec{S}$

Total current

$I = \int_S \vec{J} \cdot d\vec{S}$

Derive the equation of continuity of current  
(continuity equation of current)

$\rho_v$  C/m<sup>3</sup>



Divergence theorem:

$$\textcircled{1} \quad \oint_S \vec{J} \cdot d\vec{s} = \iiint_V \nabla \cdot \vec{J} \, dv$$

$$I = \oint_S \vec{J} \cdot d\vec{s} = \iiint_V (\nabla \cdot \vec{J}) \, dv \rightarrow \textcircled{2}$$

$$Q_i = \iiint_V \rho_v \, dv \rightarrow \textcircled{3}$$

Sub  $\textcircled{2}$  &  $\textcircled{3}$  in  $\textcircled{1}$

$$\iiint_V (\nabla \cdot \vec{J}) \, dv = - \frac{d}{dt} \left[ \iiint_V \rho_v \, dv \right]$$

$\rho_v(x, y, z, t)$

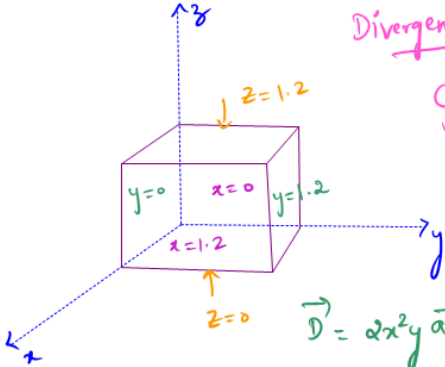
$$\iiint_V (\nabla \cdot \vec{J}) \, dv = - \iiint_V \left( \frac{\partial \rho_v}{\partial t} \right) \, dv$$

$$\textcircled{-X} \quad \boxed{\nabla \cdot \vec{J} = - \frac{\partial \rho_v}{\partial t}} \quad \text{continuity eqn. of current}$$

3. Evaluate both sides of the divergence theorem for the field  $\mathbf{D} = 2x^2y \mathbf{a}_x + 3x^2y^2 \mathbf{a}_y$  C/m<sup>2</sup> and the cube formed by the planes  $x = 0$  and  $1.2$ ,  $y = 0$  and  $1.2$ , and  $z = 0$  and  $1.2$ .

[10] CO2 L3

Divergence theorem:

$$\oiint_S \vec{D} \cdot d\vec{s} = \iiint_V \nabla \cdot \vec{D} \, dv$$


$\vec{D} = 2x^2y \mathbf{a}_x + 3x^2y^2 \mathbf{a}_y$  C/m<sup>2</sup>

LHS:

$$\oiint_S \vec{D} \cdot d\vec{s} = \iint_{\text{top}} \vec{D} \cdot d\vec{s}_z + \iint_{\text{bottom}} \vec{D} \cdot d\vec{s}_z + \iint_{\text{left}} \vec{D} \cdot d\vec{s}_y + \iint_{\text{right}} \vec{D} \cdot d\vec{s}_y + \iint_{\text{front}} \vec{D} \cdot d\vec{s}_x + \iint_{\text{back}} \vec{D} \cdot d\vec{s}_x$$

$$\oiint_S \vec{D} \cdot d\vec{s} = - \iint_{z=0} 3x^2y^2 dx dz + \iint_{z=1.2} 3x^2y^2 dx dz + \iint_{y=0} 2x^2y dy dz - \iint_{y=1.2} 2x^2y dy dz + \iint_{x=1.2} 2x^2y dy dz - \iint_{x=0} 2x^2y dy dz$$

$$\oiint_S \vec{D} \cdot d\vec{s} = 3x(1.2)^2 \times \int_0^{1.2} \int_0^{1.2} x^2 dx dz + 2x(1.2)^2 \times \int_0^{1.2} \int_0^{1.2} y dy dz$$

$$= 3 \times (1.2)^2 \times \left[ \frac{x^3}{3} \right]_0^{1.2} \times [z]_0^{1.2} + 2 \times (1.2)^2 \times \left[ \frac{y^2}{2} \right]_0^{1.2} \times [z]_0^{1.2}$$

$$= (1.2)^5 \times 1.2 + (1.2)^4 \times 1.2$$

$$\oiint_S \vec{D} \cdot d\vec{s} = 5.474304 \text{ C}$$

RHS:  $\iiint_V \nabla \cdot \vec{D} \, dv = ? \quad \vec{D} = 2x^2y \vec{a}_x + 3x^2y^2 \vec{a}_y \text{ C/m}^2$

$$\nabla \cdot \vec{D} = \frac{\partial}{\partial x}(2x^2y) + \frac{\partial}{\partial y}(3x^2y^2) + \frac{\partial}{\partial z}(0)$$

$$\nabla \cdot \vec{D} = 4xy + 6x^2y \text{ C/m}^3$$

$$\iiint_V (4xy + 6x^2y) \, dx \, dy \, dz = \iiint_V 4xy \, dx \, dy \, dz + \iiint_V 6x^2y \, dx \, dy \, dz$$

$$= 4 \left[ \frac{x^2}{2} \right]_0^{1.2} \times \left[ \frac{y^2}{2} \right]_0^{1.2} \times [z]_0^{1.2} + 6 \left[ \frac{x^3}{3} \right]_0^{1.2} \times \left[ \frac{y^2}{2} \right]_0^{1.2} \times [z]_0^{1.2}$$

$$= (1.2)^2 \times (1.2)^2 \times (1.2) + (1.2)^3 \times (1.2)^2 \times (1.2)$$

$$\iiint_V (\nabla \cdot \vec{D}) \, dv = 5.474304 \text{ C}$$

4.(a) Derive Poisson's and Laplace's equations in free space.

[04] CO3 L2

Poisson's & Laplace's equations:

Point form of Gauss's law,  $\nabla \cdot \vec{D} = \rho_v$

$$\text{or } \vec{D} = \epsilon \vec{E}$$

$$\vec{E} = -\nabla V$$

$$\nabla \cdot \vec{D} = \nabla \cdot \epsilon \vec{E} = \epsilon \nabla \cdot (-\nabla V) = \rho_v$$

In homogeneous region,  
 $\epsilon$  is constant

$$\Rightarrow \boxed{\nabla \cdot \nabla V = -\frac{\rho_v}{\epsilon}}$$

If  $\rho_v = 0$  (zero volume charge density)

but point charges, line charges & surface charge density exist at singular locations as source of field

$$\Rightarrow \boxed{\nabla^2 V = 0} \text{ Laplace's equation}$$

$$\nabla^2 v = \frac{\partial^2 v}{\partial x^2} + \frac{\partial^2 v}{\partial y^2} + \frac{\partial^2 v}{\partial z^2} = -\frac{\rho v}{\epsilon} \quad \text{Poisson's equation}$$

$$\nabla^2 v = \frac{\partial^2 v}{\partial x^2} + \frac{\partial^2 v}{\partial y^2} + \frac{\partial^2 v}{\partial z^2} = 0 \quad \text{Laplace's equation}$$

Poisson's eqn.

$$\nabla^2 v = \frac{1}{\rho} \frac{\partial}{\partial \rho} \left( \rho \frac{\partial v}{\partial \rho} \right) + \frac{1}{\rho^2} \frac{\partial^2 v}{\partial \phi^2} + \frac{\partial^2 v}{\partial z^2} = -\frac{\rho v}{\epsilon}$$

Laplace's eqn.

$$\nabla^2 v = \frac{1}{\rho} \frac{\partial}{\partial \rho} \left( \rho \frac{\partial v}{\partial \rho} \right) + \frac{1}{\rho^2} \frac{\partial^2 v}{\partial \phi^2} + \frac{\partial^2 v}{\partial z^2} = 0$$

Poisson's equation

$$\nabla^2 v = \frac{1}{r^2} \frac{\partial}{\partial r} \left( r^2 \frac{\partial v}{\partial r} \right) + \frac{1}{r^2 \sin \theta} \frac{\partial}{\partial \theta} \left( \sin \theta \frac{\partial v}{\partial \theta} \right) + \frac{1}{r^2 \sin^2 \theta} \frac{\partial^2 v}{\partial \phi^2} = -\frac{\rho v}{\epsilon}$$

Laplace's equation

$$\nabla^2 v = \frac{1}{r^2} \frac{\partial}{\partial r} \left( r^2 \frac{\partial v}{\partial r} \right) + \frac{1}{r^2 \sin \theta} \frac{\partial}{\partial \theta} \left( \sin \theta \frac{\partial v}{\partial \theta} \right) + \frac{1}{r^2 \sin^2 \theta} \frac{\partial^2 v}{\partial \phi^2} = 0$$



# UNIQUENESS THEOREM

This is the **uniqueness theorem**: If a solution to Laplace's equation can be found that satisfies the boundary conditions, then the solution is unique.

*only one solution*

The theorem applies to any solution of Poisson's or Laplace's equation in a given region or closed surface.

The theorem is proved by contradiction. We assume that there are two solutions  $V_1$  and  $V_2$  of Laplace's equation both of which satisfy the prescribed boundary conditions.

Laplace's eqn	$V_1(x, y, z)$	Poisson's eqn
$\nabla^2 V = 0$	$V_2(x, y, z)$	$\nabla^2 V = -\frac{\rho}{\epsilon}$
$\nabla^2 V_1 = 0 \rightarrow (1)$		$\nabla^2 V_1 = -\frac{\rho}{\epsilon} \rightarrow (3)$
$\nabla^2 V_2 = 0 \rightarrow (2)$		$\nabla^2 V_2 = -\frac{\rho}{\epsilon} \rightarrow (4)$
$(1) - (2) \Rightarrow \nabla^2 V_1 - \nabla^2 V_2 = 0$		$(3) - (4) \Rightarrow \nabla^2 V_1 - \nabla^2 V_2 = 0$
$\nabla^2 (V_1 - V_2) = 0$		
$V_1 - V_2 = V_d$		
	$\nabla^2 V_d = 0 \rightarrow (5)$	
	$\nabla^2 V_d = 0 \rightarrow (6)$	

At a given boundary (at least one conductor surface),

Boundary conditions

$V_{1b} = V_{2b} \rightarrow (7)$	$V_1(x, y, z)$	$V_2(x, y, z)$
$V_{db} = V_{1b} - V_{2b} = 0 \rightarrow (8)$	$V_{1b} = V_{2b}$	

$$V_d = V_1 - V_2$$

where  
 $V_1(x, y, z)$   
 $V_2(x, y, z)$

$$\vec{A} = V_d \vec{\nabla} V_d$$

From the divergence theorem. ✓

$$\int_V \nabla \cdot \vec{A} \, dv = \oint_S \vec{A} \cdot d\vec{S} \quad \rightarrow (9)$$

$$\iiint_V (\nabla \cdot V_d \vec{\nabla} V_d) \, dv = \oint_S V_d \vec{\nabla} V_d \cdot d\vec{S} \quad \rightarrow (10)$$

We let  $\vec{A} = V_d \nabla V_d$  and use a vector identity ✓  $\rightarrow (11)$

$$\nabla \cdot \vec{A} = \nabla \cdot (V_d \nabla V_d) = V_d \nabla^2 V_d + \nabla V_d \cdot \nabla V_d$$

But  $\nabla^2 V_d = 0$  from (6)

$$\vec{\nabla} V_d \cdot \vec{\nabla} V_d = |\vec{\nabla} V_d|^2$$

$$\nabla \cdot \vec{A} = \nabla V_d \cdot \nabla V_d = |\vec{\nabla} V_d|^2$$

$$(10) \Rightarrow \iiint_V |\vec{\nabla} V_d|^2 \, dv = \oint_S V_d \vec{\nabla} V_d \cdot d\vec{S} \quad \rightarrow (12)$$

Apply the boundary condition,

$$V_d = 0 \text{ in } (12)$$

(12)  $\Rightarrow$

$$\iiint_V |\nabla V_d|^2 dV = 0$$

$$|\nabla V_d|^2 = 0$$

$\int_a^b f(x) dx = 0$   
 i)  $f(x)$  is odd in  $[a, b]$   
 ii)  $f(x) = 0$

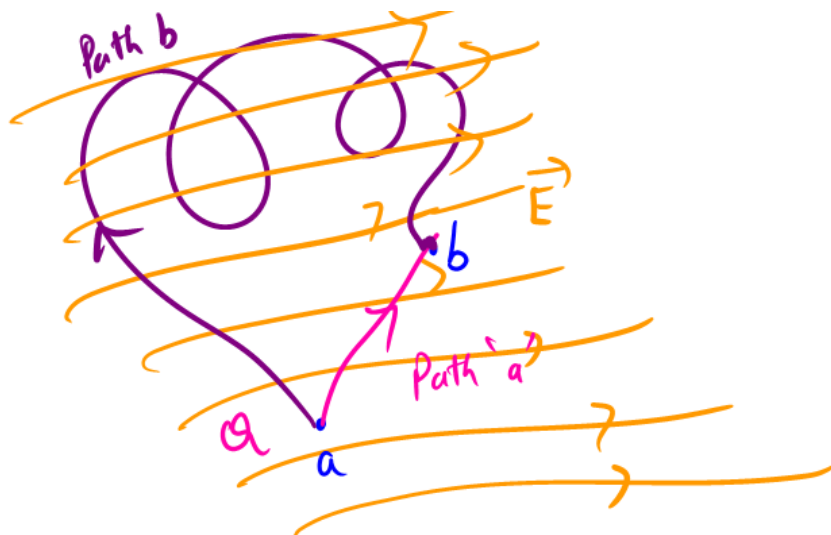
$\nabla V_d = 0 \Rightarrow V_d = \text{constant} = 0$   
 Gradient of  $V_d$  is zero only if  $V_d$  is constant  
 The constant is zero according to boundary condition

Hence,  $V_d = 0$  or  $V_1 = V_2$  everywhere,

showing that  $V_1$  and  $V_2$  cannot be different solutions of the same problem.

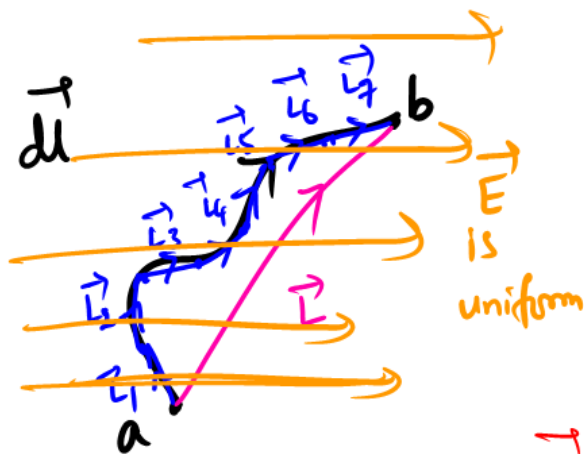
5.(a) Derive an expression for the work done in moving a point charge  $Q$  in the presence of an electric field  $\mathbf{E}$ .

[05] CO3 L2



$$dW = \vec{F} \cdot d\vec{l}$$

$$dW = -q \vec{E} \cdot d\vec{l}$$



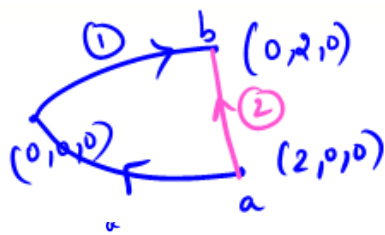
$$dW = -q (\vec{E} \cdot d\vec{l}_1 + \vec{E} \cdot d\vec{l}_2 + \dots + \vec{E} \cdot d\vec{l}_N)$$

$$= -q \vec{E} \cdot (d\vec{l}_1 + d\vec{l}_2 + \dots + d\vec{l}_N)$$

$$dW = -q \vec{E} \cdot d\vec{l} \quad \left[ W = -q \int_a^b \vec{E} \cdot d\vec{l} \right] =$$

Work done is same irrespective of path chosen

- 5.(b) Given the electric field intensity  $\vec{E} = 2x \mathbf{a}_x - 4y \mathbf{a}_y$  V/m. Find the work done in moving a point charge of 2 C from (2,0,0) to (0,0,0) and then from (0,0,0) to (0,2,0). [05] CO3 L3



Work done is  
same  
irrespective  
of the  
path chosen

path ①  $W = -q \int_a^b \vec{E} \cdot d\vec{l}$

$$W = -2x \left[ \int_{x=2}^0 2x dx - \int_{y=0}^2 4y dy \right]$$

$$W = -2x \left[ 2 \left( \frac{x^2}{2} \right) \Big|_2^0 - 4 \left( \frac{y^2}{2} \right) \Big|_0^2 \right]$$

$$W = -2 \left[ (0-4) - 2(4-0) \right]$$

$$W = -2 \left[ -4 - 8 \right]$$

$$W = 24 \text{ J}$$

path ②

$$W = -2x \left[ \int_{x=2}^0 2x dx - \int_{y=0}^0 4y dy \right] + \left\{ -2x \left[ \int_{x=0}^0 2x dx - \int_{y=0}^2 4y dy \right] \right\}$$

$$W = -2 \left\{ \int_2^0 2x dx - \int_0^2 4y dy \right\}$$

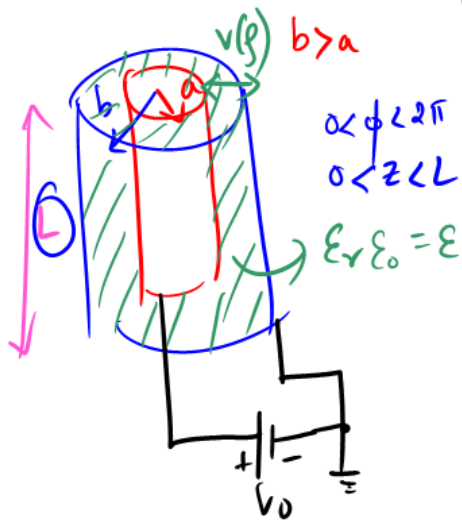
$$W = -2 \left\{ 2 \left( \frac{x^2}{2} \right) \Big|_2^0 - 4 \left( \frac{y^2}{2} \right) \Big|_0^2 \right\}$$

$$W = -2 \left\{ -4 - 8 \right\}$$

$$W = 24 \text{ J}$$

- 6.(a) Derive the expression for capacitance of coaxial cable using Laplace's equation. [08] CO3 L2  
Consider radius of inner conductor 'a' and outer conductor 'b'. Potential at radius 'a' is maintained at  $V_0$  and the outside surface is grounded.

ii) Cylindrical Capacitor:



Boundary conditions

- i) At  $\rho = a, V = V_0$
- ii) At  $\rho = b, V = 0$

Laplace's eqn

$$\nabla^2 V = 0$$

$$V(\rho)$$

$$\frac{1}{\rho} \frac{\partial}{\partial \rho} \left( \rho \frac{\partial V}{\partial \rho} \right) + \frac{1}{\rho^2} \frac{\partial^2 V}{\partial \phi^2} + \frac{\partial^2 V}{\partial z^2} = 0$$

$$\frac{1}{\rho} \frac{d}{d\rho} \left( \rho \frac{dV}{d\rho} \right) = 0$$

$$\frac{d}{d\rho} \left( \rho \frac{dV}{d\rho} \right) = 0$$

$\int \text{wrt } \rho$

$$\rho \frac{dV}{d\rho} = c_1$$

$$\frac{dV}{d\rho} = \frac{c_1}{\rho}$$

$\int \text{wrt } \rho$

$$V = \int \frac{c_1}{\rho} d\rho = c_1 \ln \rho + c_2$$

$$= c_1 \ln \rho + c_2$$

$$V = c_1 \ln \rho + c_2$$

(i)  $\rightarrow V_0 = c_1 \ln a + c_2$   $b > a$   
 (ii)  $\rightarrow 0 = c_1 \ln b + c_2$   $c_1 \ln(b/a) = -V_0$

$$c_1 = \frac{-V_0}{\ln(b/a)}$$

$$c_2 = -c_1 \ln b$$

$$c_2 = \frac{V_0}{\ln(b/a)} \ln b$$

$$V(\rho) = \frac{-V_0}{\ln(b/a)} \ln \rho + \frac{V_0}{\ln(b/a)} \ln b$$

$$\vec{E} = -\vec{\nabla} V = - \left[ \frac{\partial V}{\partial \rho} \vec{a}_\rho + \frac{1}{\rho} \frac{\partial V}{\partial \phi} \vec{a}_\phi + \frac{\partial V}{\partial z} \vec{a}_z \right]$$

$$\vec{E} = - \left[ \frac{-V_0}{\ln(b/a)} \frac{1}{\rho} \vec{a}_\rho \right]$$

$$\vec{E} = \frac{V_0}{\rho \ln(b/a)} \vec{a}_\rho \quad V/m$$

$$\vec{D} = \epsilon \vec{E}$$

$$\vec{D} = \frac{\epsilon V_0}{\rho \ln(b/a)} \vec{a}_\rho$$

$$Q = \iint_S \vec{D} \cdot d\vec{s}_\rho$$

$$d\vec{s}_\rho = \rho d\phi dz \vec{a}_\rho$$

$$= \int_{z=0}^L \int_{\phi=0}^{2\pi} \frac{\epsilon V_0}{\rho \ln(b/a)} \cdot \rho d\phi dz$$

$$Q = \frac{\epsilon V_0}{\ln(b/a)} \times 2\pi L$$

$$V_d = V_0 - 0 = V_0$$

$$C = \frac{|Q|}{V_d} = \frac{2\pi \epsilon L}{\ln(b/a)}$$

6.(b) Verify if the given field satisfies Laplace's equation:  $V = 2x^2 - 3y^2 + z^2$  V.

[02] CO3 L3

$$\nabla^2 V = 0 \quad (\text{Laplace's equation})$$

$$\frac{\partial^2 V}{\partial x^2} + \frac{\partial^2 V}{\partial y^2} + \frac{\partial^2 V}{\partial z^2} = 0$$

$$\frac{\partial^2}{\partial x^2} (2x^2 - 3y^2 + z^2) + \frac{\partial^2}{\partial y^2} (2x^2 - 3y^2 + z^2) + \frac{\partial^2}{\partial z^2} (2x^2 - 3y^2 + z^2) = 0$$

$$\frac{\partial(4x)}{\partial x} + \frac{\partial(-6y)}{\partial y} + \frac{\partial(2z)}{\partial z} = 0$$

$$4 - 6 + 2 = 0$$

$$0 = 0$$

$\Rightarrow \nabla^2 V = 0$   
The given potential function  $V$  satisfies Laplace's equation

7.(a) Electric potential at an arbitrary point in free space is given as  $V = (x+1)^2 + (y+2)^2 + (z+3)^2$  Volts. Find  $V$ ,  $\mathbf{E}$ ,  $\mathbf{D}$ ,  $\rho_V$  at  $P(2,1,0)$ .

[07] CO2 L3

(i)  $V$  at  $P(2,1,0)$   $V = (x+1)^2 + (y+2)^2 + (z+3)^2$  V

$$V = (2+1)^2 + (1+2)^2 + (0+3)^2$$

$$= 3^2 + 3^2 + 3^2$$

$$V = 27 \text{ V}$$

(ii)  $\vec{E} = -\vec{\nabla}V$

$$= - \left[ \frac{\partial V}{\partial x} \vec{a}_x + \frac{\partial V}{\partial y} \vec{a}_y + \frac{\partial V}{\partial z} \vec{a}_z \right]$$

$$\vec{E} = - \left[ 2(x+1) \vec{a}_x + 2(y+2) \vec{a}_y + 2(z+3) \vec{a}_z \right] \text{ V/m}$$



$$\vec{E} \text{ at } (2,1,0) = - \left[ 2(2+1)\vec{a}_x + 2(1+2)\vec{a}_y + 2(0+3)\vec{a}_z \right]$$

$$= - \left[ 2 \times 3 \vec{a}_x + 2 \times 3 \vec{a}_y + 2 \times 3 \vec{a}_z \right]$$

$$\vec{E} = -6\vec{a}_x - 6\vec{a}_y - 6\vec{a}_z \text{ V/m}$$

$$(iii) \vec{D} = \epsilon \vec{E} = -2\epsilon_0 \left[ (x+1)\vec{a}_x + (y+2)\vec{a}_y + (z+3)\vec{a}_z \right] \text{ C/m}^2$$

$$\vec{D} \text{ at } (2,1,0) = 8.854 \times 10^{-12} \times \left[ -6\vec{a}_x - 6\vec{a}_y - 6\vec{a}_z \right] \text{ C/m}^2$$

$$\vec{D} = (-53.124 \vec{a}_x - 53.124 \vec{a}_y - 53.124 \vec{a}_z) \text{ pC/m}^2$$

$$(v) \rho_v = \nabla \cdot \vec{D}$$

$$\rho_v = -2\epsilon_0 \left[ \frac{\partial}{\partial x}(x+1) + \frac{\partial}{\partial y}(y+2) + \frac{\partial}{\partial z}(z+3) \right]$$

$$\rho_v = -2\epsilon_0 [1+1+1]$$

$$\rho_v = -6\epsilon_0$$

$$\rho_v = -53.124 \text{ pC/m}^3$$

7.(b)

$$V = \frac{\cos 2\phi}{\rho}$$

Given  $\rho$  in free space. Find the volume charge density at the point A(0.5, 60°, 1).

[03] CO3 L3

$$\rho_v = ?$$

$$\nabla^2 V = -\frac{\rho_v}{\epsilon} \Rightarrow \rho_v = -\epsilon \nabla^2 V$$

$$\rho_v = -\epsilon \left[ \frac{1}{\rho} \frac{\partial}{\partial \rho} \left( \rho \frac{\partial V}{\partial \rho} \right) + \frac{1}{\rho^2} \frac{\partial^2 V}{\partial \phi^2} + \frac{\partial^2 V}{\partial z^2} \right]$$

$$\rho_v = -\epsilon \left[ \frac{1}{\rho} \frac{\partial}{\partial \rho} \left( \rho \frac{\partial}{\partial \rho} \left[ \frac{\cos 2\phi}{\rho} \right] \right) + \frac{1}{\rho^2} \frac{\partial^2}{\partial \phi^2} \left( \frac{\cos 2\phi}{\rho} \right) + \frac{\partial^2}{\partial z^2} \left( \frac{\cos 2\phi}{\rho} \right) \right]$$

$$\rho_v = -\epsilon \left\{ \cos 2\phi \frac{1}{\rho} \frac{\partial}{\partial \rho} \left( \rho \cdot \left( -\frac{1}{\rho^2} \right) \right) + \frac{1}{\rho^2} \cdot \frac{1}{\rho} \frac{\partial^2}{\partial \phi^2} \left[ (-\sin 2\phi) (2) \right] \right\}$$

$$\rho_v = -\epsilon \left\{ \frac{\cos 2\phi}{\rho^3} - \frac{4 \cos 2\phi}{\rho^3} \right\}$$

$$\rho_v = \epsilon \frac{3 \cos 2\phi}{\rho^3} \quad \text{C/m}^3$$

$$\rho_v = 8.854 \times 10^{-12} \times \frac{3 \times \cos(120^\circ)}{(0.5)^3}$$

$$\rho_v = -106.248 \text{ p C/m}^3$$