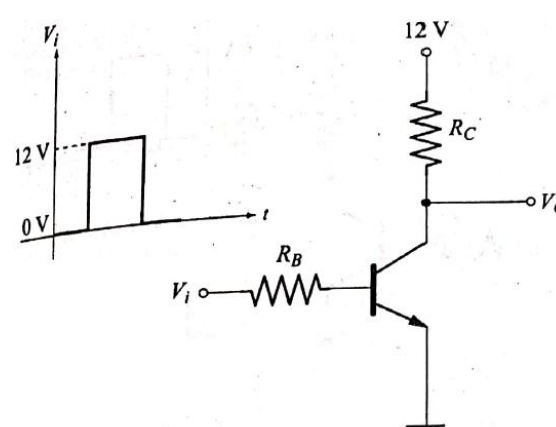


Internal Assessment Test - I

Sub:	ANALOG ELECTRONIC CIRCUITS	Code:	18EE34
Date:	17/12/2021	Duration:	90 mins
		Max Marks:	50
		Sem:	3rd
		Branch:	EEE
Answer Any FIVE FULL Questions			
			Marks
			OBE
			CO RBT
1	For Emitter Stabilized Bias circuit $V_{CC} = 10V$, $R_C = 1k\Omega$, $R_E = 500\Omega$, $R_B = 100k\Omega$, $\beta = 100$. Calculate I_B , I_C , V_{CE} , V_E and V_C .	10	CO1 L3
2	Design a Voltage Divider Bias circuit for the given conditions. $I_C = 1mA$, $S_{ICO} = 20$, $\beta = 100$, $V_E = 1V$, $V_{CE} = 6V$ and $V_{CC} = 12V$.	10	CO1 L3
3	Derive the expression for stability factor $S(I_{CO})$ and $S(V_{BE})$ for Emitter Bias configuration	10	CO1 L3
4	Determine the stability factor $S(V_{BE})$ and the change in I_C from $25^{\circ}C$ to $100^{\circ}C$ for the transistor with $V_{BE}(25^{\circ}C) = 0.65V$ and $V_{BE}(100^{\circ}C) = 0.48V$ for the following bias arrangements a) Fixed Bias with $R_B = 270k\Omega$ and $\beta = 120$ b) Voltage Divider Bias with $R_1 = 39k\Omega$, $R_2 = 10k\Omega$, $R_E = 1k\Omega$ and $\beta = 120$	10	CO1 L3
5	Derive the expression for stability factor $S(I_{CO})$, $S(V_{BE})$ and $S(\beta)$ for Fixed Bias configuration	10	CO1 L3
6	For the transistor inverter shown, determine the values of R_B and R_C . Take $I_{C(sat)} = 12mA$, $\beta = 200$ and $V_{CE(sat)} = 0V$. Also draw the output voltage waveform. <div style="text-align: center;">  </div>	10	CO1 L3
7	What is Clamping circuits? Draw the circuit and output waveforms for Negative Clamper and Positive Clamper.	10	CO1 L1

IAT 1 Solution

1.

$$I_B = \frac{V_{CC} - V_{BE}}{R_B + (1+\beta)R_E} = \frac{10V - 0.7V}{100k\Omega + (101)500\Omega} = \frac{9.3}{150.5} = \underline{\underline{0.062mA}}$$

$$I_C = \beta I_B = 100 \times 0.062 = \underline{\underline{6.2mA}}$$

$$V_{CE} = V_{CC} - I_C(R_C + R_E)$$

$$= 10 - 6.2(1 + 500\Omega) = \underline{\underline{0.7V}}$$

$$V_E = I_E R_E = 6.2 \times 500\Omega = \underline{\underline{3.1V}}$$

$$V_C = V_{CC} - I_C R_C = 10 - 6.2 \times (1) = \underline{\underline{3.8V}}$$

2.

$$I_C \approx I_E = \underline{\underline{1mA}}$$

$$V_E = I_E R_E \Rightarrow R_E = \frac{V_E}{I_E} = \underline{\underline{1k\Omega}}$$

$$I_B = \frac{I_C}{\beta} = 0.01mA$$

$$V_{CC} - V_{CE} - I_C(R_C + R_E) = 0$$

$$\therefore R_C = \frac{V_{CC} - V_{CE}}{I_C} - R_E = \underline{\underline{5k\Omega}}$$

$$S_{(CO)} = (1+\beta) \left[\frac{R_E + R_{TH}}{(1+\beta)R_E + R_{TH}} \right]$$

$$[(1+\beta)R_E + R_{TH}]20 = (1+\beta)(R_E + R_{TH})$$

$$2020R_E + 20R_{TH} = 101R_E + 101R_{TH}$$

$$81R_{TH} = 1919R_E$$

$$R_{TH} = 23.691k\Omega$$

$$V_{TH} = R_{TH} I_B + I_E R_E + V_{BE}$$

$$= (23.691 \times 0.01) + (1 \times 1) + 0.7$$

$$= 1.937V$$

$$V_{TH} = V_{CC} \frac{R_2}{R_1 + R_2}$$

$$V_{TH} = \frac{V_{CC}}{R_1} \frac{R_1 R_2}{(R_1 + R_2)} = \frac{V_{CC}}{R_1} R_{TH}$$

$$R_1 = \frac{V_{CC}}{V_{TH}} R_{TH} = \frac{12}{1.937} \times 23.691 = 146.769 k\Omega$$

$$\approx \underline{\underline{147 k\Omega}}$$

$$R_{TH} = R_1 || R_2 \Rightarrow \frac{1}{R_{TH}} = \frac{1}{R_1} + \frac{1}{R_2}$$

$$\frac{1}{R_2} = \frac{1}{R_{TH}} - \frac{1}{R_1} = \frac{R_1 - R_{TH}}{R_1 R_{TH}}$$

$$\therefore R_2 = \frac{R_1 R_{TH}}{R_1 - R_{TH}} = \frac{147 \times 23.691}{147 - 23.691}$$

$$= 28.243 k\Omega$$

$$\approx \underline{\underline{28 k\Omega}}$$

3.

Stability Factor $S(I_{CO})$

$$S(I_{CO}) = \frac{1 + \beta}{1 - \beta \frac{\partial I_B}{\partial I_C}}$$

$$V_{CC} = I_B R_B + V_{BE} + I_E R_E$$

But $I_E = I_B + I_C$

$$\therefore V_{CC} = I_B R_B + V_{BE} + I_B R_E + I_C R_E$$

Differentiating with respect to I_C keeping V_{BE} constant, we get

$$0 = \frac{\partial I_B}{\partial I_C} R_B + \frac{\partial I_B}{\partial I_C} R_E + R_E = \frac{\partial I_B}{\partial I_C} (R_B + R_E) + R_E$$

$$\therefore \frac{\partial I_B}{\partial I_C} = - \frac{R_E}{R_B + R_E}$$

$$S(I_{CO}) = \frac{1 + \beta}{1 - \beta \left(\frac{-R_E}{R_B + R_E} \right)} = \frac{1 + \beta}{1 + \beta \left(\frac{R_E}{R_B + R_E} \right)}$$

$$= \frac{(\beta + 1)(R_B + R_E)}{R_B + R_E + \beta R_E} = \frac{(\beta + 1)(R_B + R_E)}{(\beta + 1)R_E + R_B}$$

$$S(I_{CO}) = \frac{(\beta + 1) \left(1 + \frac{R_B}{R_E} \right)}{(\beta + 1) + \frac{R_B}{R_E}}$$

Stability Factor $S(V_{BE})$

$$S(V_{BE}) = \frac{\partial I_C}{\partial V_{BE}}$$

$$V_{CC} = I_B R_B + V_{BE} + I_B R_E + I_C R_E$$

$$\text{Substituting } I_B = \frac{I_C}{\beta}$$

$$V_{CC} = \frac{I_C}{\beta} R_B + V_{BE} + \frac{I_C}{\beta} R_E + I_C R_E$$

$$= \left[\frac{R_B}{\beta} + \frac{R_E}{\beta} + R_E \right] I_C + V_{BE}$$

$$= \left[\frac{R_B + R_E + \beta R_E}{\beta} \right] I_C + V_{BE}$$

$$V_{CC} = \left[\frac{R_B + (1 + \beta) R_E}{\beta} \right] I_C + V_{BE}$$

Differentiating with respect to I_C , keeping β constant, we get

$$0 = \frac{R_B + (1 + \beta) R_E}{\beta} + \frac{\partial V_{BE}}{\partial I_C}$$

$$\therefore \boxed{S(V_{BE}) = \frac{\partial I_C}{\partial V_{BE}} = \frac{-\beta}{R_B + (1 + \beta) R_E}}$$

4.

$$4. a) \Delta V_{BE} = V_{BE}(100^\circ\text{C}) - V_{BE}(25^\circ\text{C}) = \underline{\underline{-0.17V}}$$

$$S_{V_{BE}} = \frac{-\beta}{R_B} = -0.44 \times 10^{-3}$$

$$\Delta I_C = S_{V_{BE}} \times \Delta V_{BE} = \underline{\underline{74.8 \mu\text{A}}}$$

$$b) \Delta V_{BE} = -0.17V$$

$$S(V_{BE}) = \frac{-\beta}{R_{TH} + (1 + \beta) R_E}$$

$$R_{TH} = R_1 \parallel R_2 = 7.95 \text{ k}\Omega$$

$$\therefore S(V_{BE}) = -0.93 \times 10^{-3}$$

$$\Delta I_C = S(V_{BE}) \times \Delta V_{BE} = \underline{\underline{158.1 \mu\text{A}}}$$

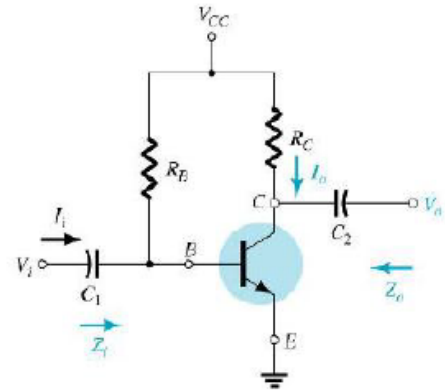
5.

Stability Factor $S(I_{CO})$

$S(I_{CO})$ or $S = \frac{\partial I_C}{\partial I_{CBO}}$ at constant V_{BE} and β

From circuit diagram

$$I_B = \frac{V_{CC} - V_{BE}}{R_B}$$



$$V_{CC} \gg V_{BE}$$

$$I_B \simeq \frac{V_{CC}}{R_B} \quad \text{which is constant}$$

Differentiating with respect to I_C ,

$$\frac{\partial I_B}{\partial I_C} = 0$$

Substitute in equation A,

$$\boxed{S(I_{CO}) = 1 + \beta}$$

Stability Factor $S(V_{BE})$

$$S(V_{BE}) \equiv \frac{\partial I_C}{\partial V_{BE}}$$

$$V_{CC} = I_B R_B + V_{BE}$$

$$\therefore V_{BE} = V_{CC} - I_B R_B$$

$$\text{But } I_B \approx \frac{I_C}{\beta}$$

$$\therefore V_{BE} = V_{CC} - \frac{I_C}{\beta} R_B$$

Differentiating with respect to V_{BE} , keeping β constant, we get

$$1 = 0 - \frac{R_B}{\beta} \frac{\partial I_C}{\partial V_{BE}}$$

$$S(V_{BE}) = -\frac{\beta}{R_B}$$

6.

Solution To find R_C , $I_C(\text{sat}) = \frac{V_{CC} - V_{CE}(\text{sat})}{R_C}$

$$\therefore R_C = \frac{V_{CC}}{I_C(\text{sat})} = \frac{12V}{12\text{mA}} = 1\text{K}\Omega$$

To find R_B , $I_B(\text{max}) = \frac{I_C(\text{sat})}{\beta_{DC}} = \frac{12\text{mA}}{200} = 60\mu\text{A}$.

Let $I_B = 150\%$ of $I_B(\text{max})$ [to ensure saturation]
 $= 1.5 (60\mu\text{A}) = 90\mu\text{A}$.

$$\therefore R_B = \frac{V_i - V_{BE}}{I_B} = \frac{12V - 0.7V}{90\mu\text{A}} = 125.55\text{K}\Omega$$

7.

- A clamping circuit is a circuit that shifts an AC waveform (up or down) to a different DC level.
- Also known as a level shifter.
- The input and output waveforms have identical shapes, only the DC level is different.

