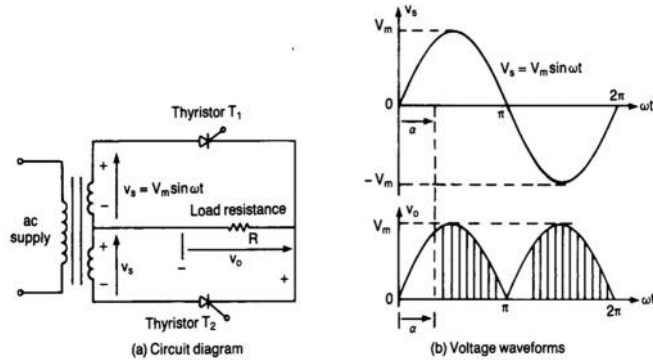




## Ac-dc converters (controlled rectifiers)

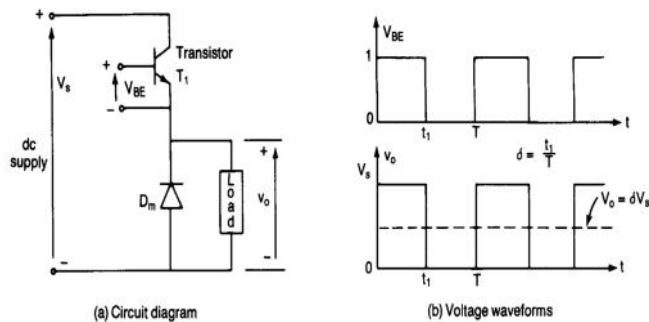
- A **single-phase** converter with two natural commutated thyristor is shown
- Average value of the output voltage can be controlled by varying the conduction time of thyristors
- This converters are also known as *controlled rectifiers*



5

## Dc-dc converters (dc choppers)

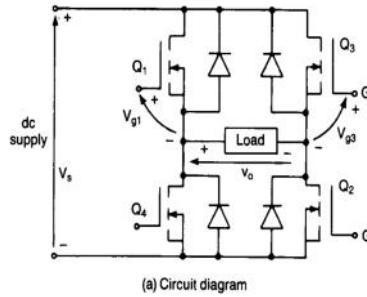
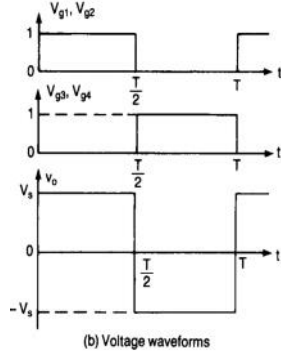
- Is also known as *Chopper or Switching Regulator*
- The average output voltage is controlled by varying the conduction of transistor,  $t_1$ .
- If  $T$  is the chopping period, then  $t_1 = \delta T$
- $\delta$  is called as the duty cycle of chopper



6

## DC-AC Converters

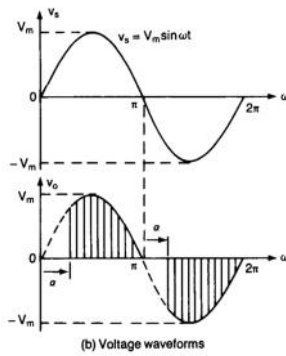
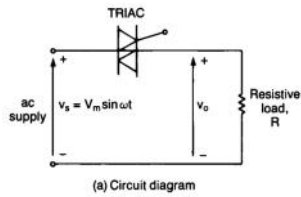
- Is also known as **Inverter**
- If transistor Q1 and Q2 conduct for one-half period and Q3 and Q4 conduct the other half, the output voltage is of alternating form
- Fixed dc voltage to variable ac voltage
- Voltage control is obtained by controlling duty cycle
- Also known as inverter



7

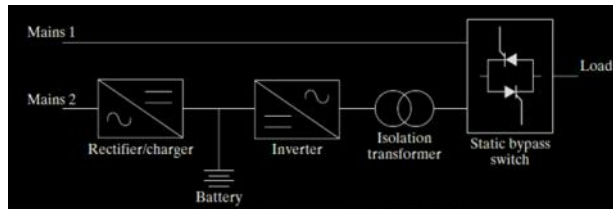
## AC-AC Converters

- AC Voltage Controller / Cyclo Converter
- **Fixed AC source into variable AC** output voltage
- a single-phase converter with a TRIAC is shown below



## Static Switches

- Power devices can be operated as static switches or contactors
- Supply to these switches could be either AC or DC
- **The switches are called as AC static switches or DC switches**
- Power electronic devices used as static switches in an UPS shown
- Mains 1 and 2 are connected to same supply
- Mains 1 supplies the load thro static bypass switch
- The rectifier charges the battery from Mains 2.
- The inverter supplies the emergency power to the load



9

1b Explain the peripheral effects of power electronic equipments.

4

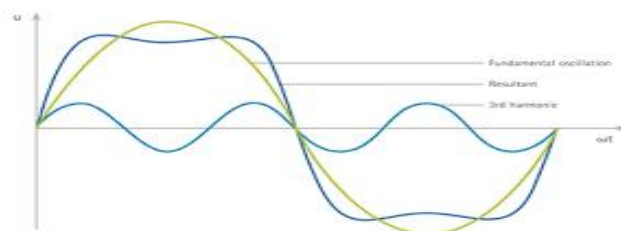
CO1

L2

## Harmonics

- **Harmonics** are unwanted higher frequencies which superimposed on the fundamental waveform (50 Hz) creating a distorted wave pattern.
- **Harmonic** is a
  - voltage or current waveforms at a multiple of the fundamental frequency of the system,
  - produced by the action of non-linear loads such as rectifiers, discharge lighting, or saturated magnetic devices.
- "harmonics" are multiples of the fundamental frequency  $f$  and can therefore be expressed as:  $2f$ ,  $3f$ ,  $4f$ , etc.

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**Need for Filter**

## Effects of Harmonics

The operations of the power converters are based mainly on the switching of power semiconductor devices

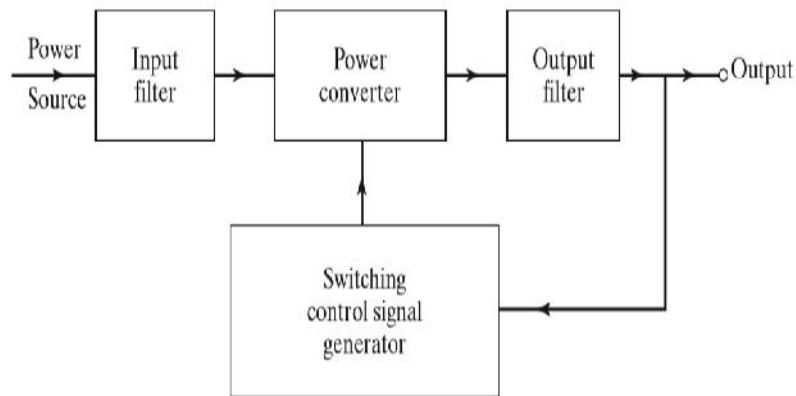
- As a result the converters **introduce current and voltage harmonics into the supply system and on the output of the converters**. These can cause
  - Problems of distortion of the output voltage and current
  - harmonic generation into the supply system
  - Interference with the communication and signalling circuits.
  - Harmonic frequencies in the power grid are a frequent cause of **power quality problems**.
  - Increased heating in the equipment and conductors
  - Misfiring in variable speed drives
  - Torque pulsations in motors.

13

### Need for filter

- It is normally necessary to introduce filters on the input and output of a converter system to reduce the harmonic level to an acceptable magnitude.

### Generalized Power Converter System



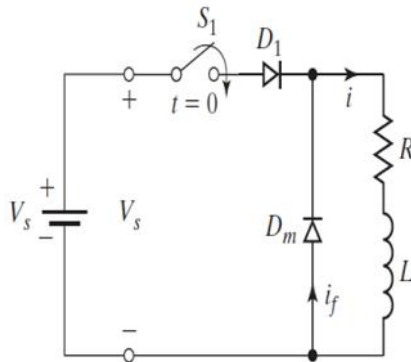
2 Explain the function of a freewheeling diode in a switched RL load with the help of circuit diagram and waveforms.

10

CO1

L2

## Freewheeling diodes with RL Load

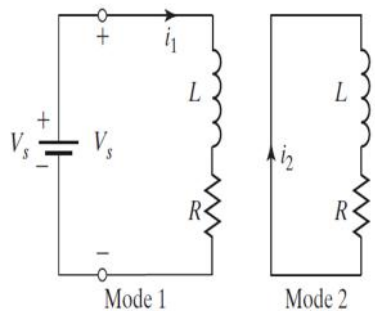


(a) Circuit diagram

D1 – Normal Diode

Dm – Freewheeling Diode

- If switch  $S_1$  is closed for time  $t_1$ , a current is established through the load;
- If the switch is opened, a path must be provided for the current in the inductive load.
- Otherwise, the inductive energy induces a very high voltage and this energy is dissipated as heat across the switch as sparks.
- This is normally done by connecting a diode  $D_m$  as shown in Figure, and this diode is usually called a *freewheeling diode*.
- Diode  $D_m$  is needed to provide a path for the inductive load current.
- Diode  $D_1$  is connected in series with the switch and it will prevent any negative current flow through the switch if there is an ac input supply voltage.
- But for dc supply, there is no need for  $D_1$ .



(b) Equivalent circuits

- The circuit operation can be divided into **Two modes**.
- Mode 1 begins when the switch is closed at  $t = 0$
- Mode 2 begins when the switch is opened.
- The equivalent circuits for the modes are shown in Figure.
- Variables  $i_1$  and  $i_2$  are defined as the instantaneous currents for mode 1 and mode 2, respectively;
- $t_1$  and  $t_2$  are the corresponding durations of these modes.

## Mode 1

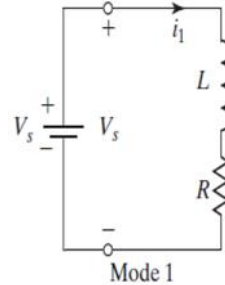
- Diode current  $i_1$

$$i_1(t) = \frac{V_s}{R} (1 - e^{-tR/L})$$

- When the switch is opened at  $t = t_1$  (at the end of this mode),
- Diode current  $i_1$  at  $t = t_1$  becomes

$$I_1 = i_1(t = t_1) = \frac{V_s}{R} (1 - e^{-t_1 R/L})$$

- If the time  $t_1$  is sufficiently long, the current practically reaches a **steady-state current** of  $I_s = V_s/R$  flows through the load.



## Mode 2

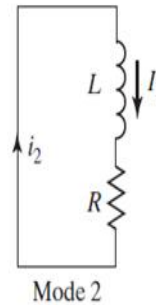
- This mode begins when the **switch is opened and the load current starts to flow through the freewheeling diode  $D_m$** .
- Redefining the time origin at the beginning of this mode, the **freewheeling diode** is found f

$$0 = L \frac{di_2}{dt} + Ri_2$$

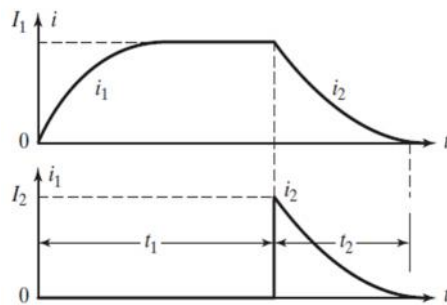
- with initial condition  $i_2(t = t_1) = I_1$ .
- the free  $i_2$  is given by

$$i_2(t) = I_1 e^{-tR/L}$$

- at  $t = t_2$  this current decays exponentially to practically zero provided that  $t_2 > L/R$ .



## Waveforms of Currents



(c) Waveforms

## Steady-State Characteristics

- The MOSFETs are **voltage-controlled devices** and have a very **high input impedance**.
- The gate draws a very small leakage current, on the order of nano amperes.
- The **current gain**, which is the **ratio of drain current  $I_D$  to input gate current  $I_G$** , is typically on the order of  $10^9$ .
- The **transconductance**, which is the **ratio of drain current to gate voltage**, defines the transfer characteristics and is a very important parameter.  $g_m = \Delta I_D / \Delta V_{GS}$ , when  $V_{DS}$  is constant.
- Drain current is calculated as

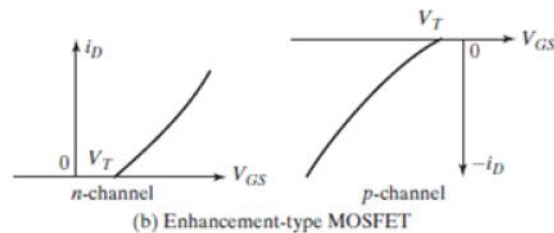
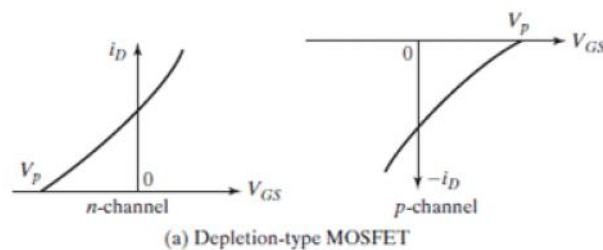
$$i_D = K_n (v_{GS} - V_T)^2 \text{ for } v_{GS} > V_T \text{ and } v_{DS} \geq (v_{GS} - V_T)$$

where  $K_n$  is the MOS constant,  $A/V^2$

$v_{GS}$  is the gate-to-source voltage, V

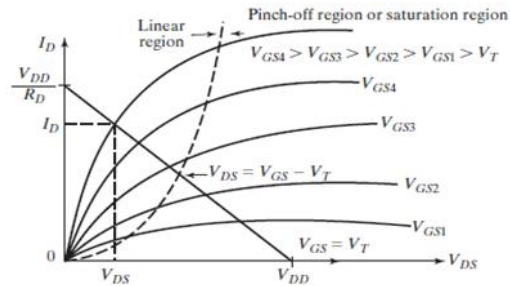
$V_T$  is the threshold voltage, V

## Transfer characteristics of MOSFETs





## Output characteristics - Enhancement-type MOSFET



There are three regions of operation: (1) cutoff region, where  $V_{GS} \leq V_T$ ; (2) pinch-off or saturation region, where  $V_{DS} \geq V_{GS} - V_T$ ; and (3) linear region, where  $V_{DS} \leq V_{GS} - V_T$ . The pinch-off occurs at  $V_{DS} = V_{GS} - V_T$ .

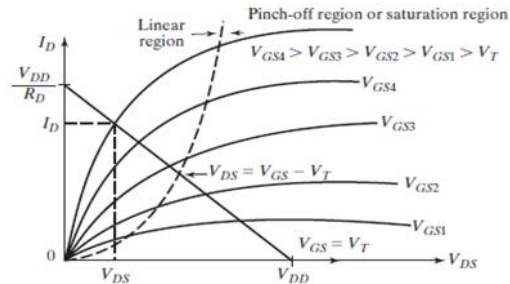
The load line of a MOSFET with a load resistance  $R_D$  can be described by

$$i_D = \frac{V_{DD} - v_{DS}}{R_D}$$

where  $i_D = V_{DD}/R_D$  at  $v_{DS} = 0$  and  $v_{DS} = V_{DD}$  at  $i_D = 0$

In order to keep the value of  $V_{DS}$  low, the gate-source voltage  $V_{GS}$  must be higher so that the transistor operates in the linear region.

## Output characteristics - Enhancement-type MOSFET



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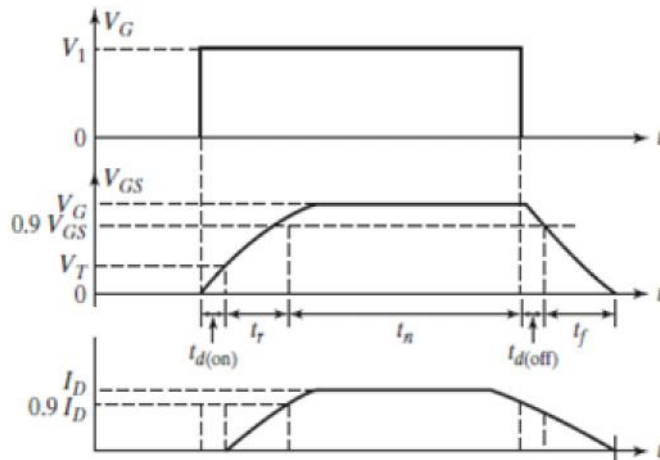
In order to keep the value of  $V_{DS}$  low, the gate-source voltage  $V_{GS}$  must be higher so that the transistor operates in the linear region.

# Switching Characteristics of MOSFETs

## Parasitic model of enhancement of MOSFETs

- Without any gate signal, the enhancement-type MOSFET may be considered as **two diodes connected back to back** (*np and pn diodes*) or as an **NPN-transistor**.
- The gate structure has **parasitic capacitances to the source,  $C_{gs}$ , and to the drain,  $C_{gd}$** .
- The NPN-transistor has a **reverse-bias junction from the drain to the source** and offers a capacitance,  $C_{ds}$ .
- Hence, a MOSFET may be considered as having an internal diode and the parasitic capacitances are dependent on their respective voltages.

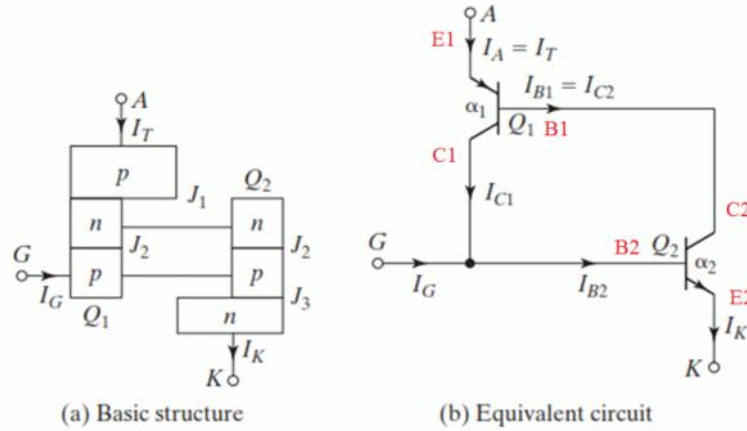
## Switching waveforms and times



	<p style="text-align: center;"><b>Definitions</b></p> <ul style="list-style-type: none"> <li>• <i>Delay time <math>t_{d(on)}</math> / Turn on Delay time</i> is the time that is required to charge the input capacitance to threshold voltage level.</li> <li>• <i>It is time taken by the VGS increases from 0 to VT (Threshold voltage)</i></li> <li>• <i>Rise time <math>t_r</math></i> is the gate-charging time from the threshold level to the full-gate voltage <math>V_{GSP}</math>, which is required to drive the transistor into the linear region.</li> <li>• <i>It is time taken by ID to increase from 0 to 90% &amp; VGS increase from VT to VGSp (Full gate voltage)</i></li> <li>• <i>Turn-off delay time <math>t_{d(off)}</math> / storage time</i> is the time required for the input capacitance to discharge from the overdrive gate voltage <math>V_1</math> to the pinch-off region.</li> <li>• <i>It is time taken by ID to decrease from 100% to 90% &amp; VGS decrease from VGS to VGSp (Full gate voltage)</i></li> <li>• <i>Fall time <math>t_f</math></i> is the time that is required for the input capacitance to discharge from the pinch-off region to threshold voltage.</li> <li>• <i>It is time taken by ID to decrease from 90% to 0 &amp; VGS decrease from VGSp to 0.</i></li> <li>• <i>If <math>V_{GS} \leq V_T</math>, transistor turns off.</i></li> </ul>			
4	<p>Explain the two-transistor analogy, and derive an expression for the anode current of thyristor.</p> <p style="text-align: center;"><b>Two-transistor Model of Thyristor</b></p> <ul style="list-style-type: none"> <li>• The regenerative or latching action due to a positive feedback can be demonstrated by using a two-transistor model of thyristor.</li> <li>• A thyristor can be considered as two complementary transistors</li> <li>• one PNP-transistor, Q1, and other NPN-transistor, Q2.</li> </ul>	10	CO3	L2

## Two-transistor Model of Thyristor

Two-transistor model of thyristor.



(a) Basic structure

(b) Equivalent circuit

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The collector current  $I_C$  of a thyristor is related, in general, to the emitter current  $I_E$  and the leakage current of the collector-base junction,  $I_{CBO}$ , as

$$I_C = \alpha I_E + I_{CBO} \quad (9.1)$$

and the *common-base current gain* is defined as  $\alpha \approx I_C/I_E$ . For transistor  $Q_1$ , the emitter current is the anode current  $I_A$ , and the collector current  $I_{C1}$  can be found from Eq. (9.1):

$$I_{C1} = \alpha_1 I_A + I_{CBO1} \quad (9.2)$$

where  $\alpha_1$  is the current gain and  $I_{CBO1}$  is the leakage current for  $Q_1$ . Similarly, for transistor  $Q_2$ , the collector current  $I_{C2}$  is

$$I_{C2} = \alpha_2 I_K + I_{CBO2} \quad (9.3)$$

where  $\alpha_2$  is the current gain and  $I_{CBO2}$  is the leakage current for  $Q_2$ . By combining  $I_{C1}$  and  $I_{C2}$ , we get

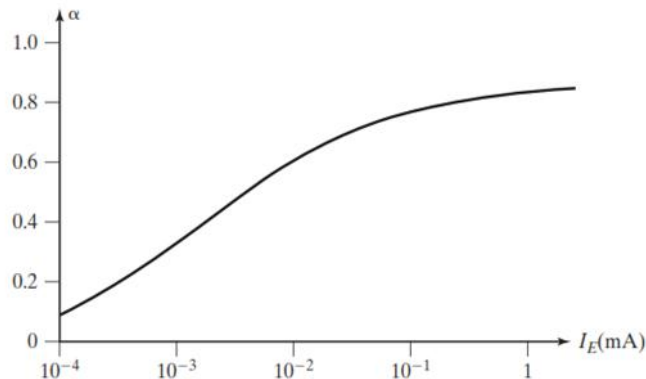
$$I_A = I_{C1} + I_{C2} = \alpha_1 I_A + I_{CBO1} + \alpha_2 I_K + I_{CBO2} \quad (9.4)$$

For a gating current of  $I_G, I_K = I_A + I_G$  and solving Eq. (9.4) for  $I_A$  gives

$$I_A = \frac{\alpha_2 I_G + I_{CBO1} + I_{CBO2}}{1 - (\alpha_1 + \alpha_2)} \quad (9.5)$$

### Derivation of Anode Current

### Variation of Current Gain with Emitter Current



Typical variation of current gain with emitter current.

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The current gain  $\alpha_1$  varies with the emitter current  $I_A = I_E$ ;  
 and  $\alpha_2$  varies with  $I_K = I_A + I_G$ .

If the gate current  $I_G$  is suddenly increased, say from 0 to 1 mA, this immediately increases anode current  $I_A$ , which would further increase  $\alpha_1$  and  $\alpha_2$ .  
 Current gain  $\alpha_2$  depends on  $I_A$  and  $I_G$ .

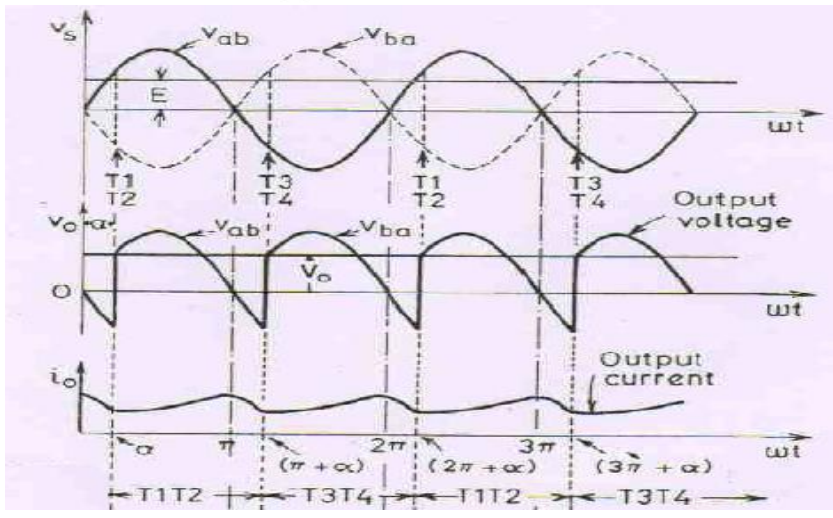
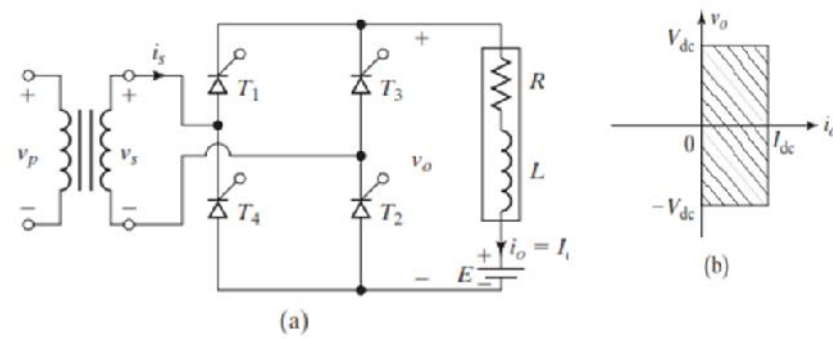
The increase in the values of  $\alpha_1$  and  $\alpha_2$  further increases  $I_A$ .

Therefore, there is a regenerative or positive feedback effect.

If  $(\alpha_1 + \alpha_2)$  tends to be unity,  
 the denominator of Eq.  $I_A = \frac{\alpha_2 I_G + I_{CBO1} + I_{CBO2}}{1 - (\alpha_1 + \alpha_2)}$  approaches zero,  
 resulting in a large value of anode current  $I_A$ ,  
 and the thyristor turns on with a small gate current.

5 Explain single phase fully controlled converter with RLE load with neat diagram and waveform and derive the expression for average and RMS voltage.

10 CO4 L2



- During the positive half-cycle**
- The fully controlled bridge converter consists of four thyristors  $T1$ ,  $T2$ ,  $T3$  and  $T4$  connected in the form of full wave bridge configuration.
  - Each thyristor is controlled and turned on by its gating signal and naturally

turns off when a reverse voltage appears across it (Line commutation or Natural commutation).

- Thyristors  $T1$  and  $T2$  are forward biased (0 to  $\pi$ );
- when these two thyristors are turned on simultaneously at  $t = \alpha$ , the load is connected to the input supply through  $T1$  and  $T2$ .
- Due to the inductive load, thyristors  $T1$  and  $T2$  continue to conduct beyond  $t = \pi$ , even though the input voltage is already negative.
- $T1$  and  $T2$  conduct from  $t = \alpha$  to  $\pi + \alpha$
- The output voltage across the load follows the input voltage  $v_o = v_m \sin t$

**During the negative half-cycle of the input voltage**

- Thyristors  $T3$  and  $T4$  are forward biased ( $\pi$  to  $2\pi$ );
- Turning on of thyristors  $T3$  and  $T4$  applies the supply voltage across thyristors  $T1$  and  $T2$  as reverse blocking voltage.
- $T3$  &  $T4$  are triggered at  $t = \pi + \alpha$
- $T1$  and  $T2$  are turned off due to *line* or *natural commutation*.
- The output voltage across the load follows the input voltage  $v_o = -v_m \sin t$
- Load current is transferred from  $T1$  and  $T2$  to  $T3$  and  $T4$ .
- $T3$  and  $T4$  conduct from  $t = \pi + \alpha$  to  $2\pi + \alpha$
- During next half cycle  $T3$  and  $T4$  are turned off

**During Period from  $\alpha$  to  $\pi - \alpha$  - Rectification mode**

- The input voltage  $v_s$  and input current  $i_s$  are positive,
- Power flows from the supply to the load.
- The converter is said to be operated in **rectification mode**.

**During Period from  $\pi + \alpha$  to  $2\pi - \alpha$  - Inversion mode**

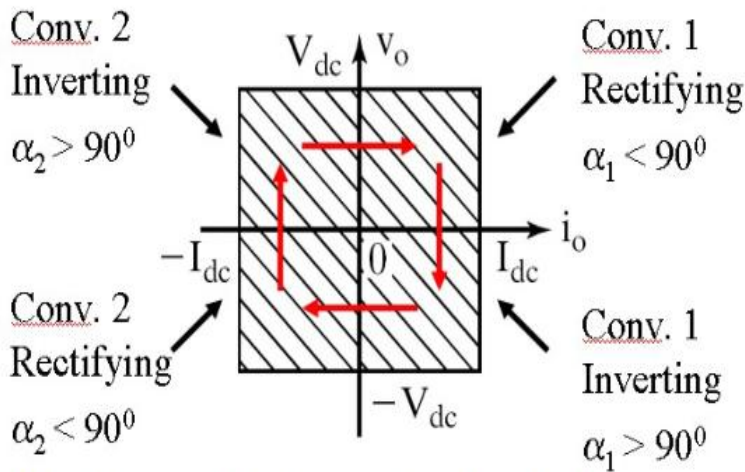
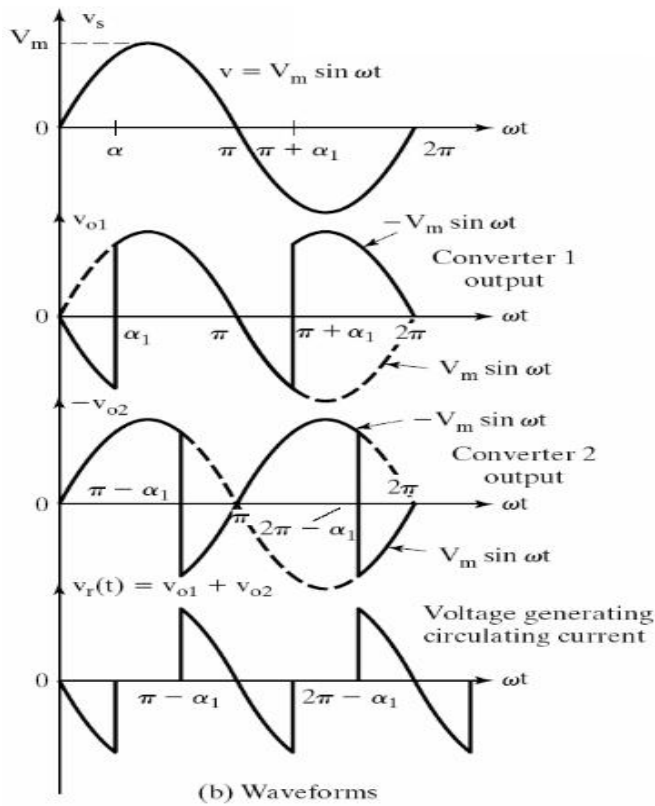
- The input voltage  $v_s$  is negative and the input current  $i_s$  is positive,
- Reverse power flows from the load to the supply.
- The converter is said to be operated in inversion mode.
- This converter is extensively used in industrial applications up to 15 kW.
- Depending on the value of  $\alpha$ , the average output voltage could be either positive or negative and it provides two-quadrant operation.

**Average Output Voltage  $V_{dc}$**

	$V_{O(dc)} = V_{dc} = \frac{2}{2\pi} \left[ \int_{\alpha}^{\pi+\alpha} V_m \sin \omega t . d(\omega t) \right]$ $V_{O(dc)} = V_{dc} = \frac{1}{\pi} \left[ \int_{\alpha}^{\pi+\alpha} V_m \sin \omega t . d(\omega t) \right]$ $V_{O(dc)} = V_{dc} = \frac{V_m}{\pi} \left[ \int_{\alpha}^{\pi+\alpha} \sin \omega t . d(\omega t) \right]$ $V_{O(dc)} = V_{dc} = \frac{V_m}{\pi} \left[ -\cos \omega t \right]_{\alpha}^{\pi+\alpha}$ <p><b>RMS Output Voltage Vrms</b></p> <p>The rms value of the output voltage is given by</p> $V_{rms} = \left[ \frac{2}{2\pi} \int_{\alpha}^{\pi+\alpha} V_m^2 \sin^2 \omega t d(\omega t) \right]^{1/2}$ $= \left[ \frac{V_m^2}{2\pi} \int_{\alpha}^{\pi+\alpha} (1 - \cos 2\omega t) d(\omega t) \right]^{1/2}$ $= \frac{V_m}{\sqrt{2}} = V_s$ <p>With a purely resistive load, thyristors <math>T_1</math> and <math>T_2</math> can conduct from <math>\alpha</math> to <math>\pi</math>, and thyristors <math>T_3</math> and <math>T_4</math> can conduct from <math>\alpha + \pi</math> to <math>2\pi</math>.</p>			
6	<p>Illustrate the single-phase dual converter with neat diagram and waveform and also explain the significance of circulating current in dual converter.</p> <ul style="list-style-type: none"> <li>• Dual converter- the name itself indicates that it has two converters in it.</li> <li>• The dual converter system will provide four quadrant operation</li> <li>• Normally used in high power industrial variable speed drives.</li> <li>• In the case of a single phase full converter with inductive loads, the converter can operate in two different quadrants in the <math>V_{dc}</math> versus <math>I_{dc}</math> operating diagram.</li> <li>• If two single phase full converters are connected in parallel and in opposite direction (connected in back to back) across a common load four quadrant operation is possible.</li> </ul> <p>Such a converter is called as a dual converter.</p>	10	CO4	L2







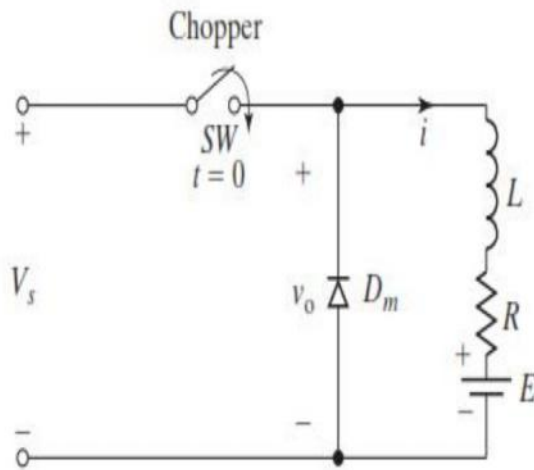
**Fig.: Four quadrant operation of a dual converter**

### CIRCULATING CURRENT

- In this mode of operation both the converters 1 and 2 are switched on and operated simultaneously and both the converters are in a state of conduction.
- If converter 1 is operated as a controlled rectifier by adjusting the trigger angle  $\alpha_1$  between 0 to  $90^\circ$  ( $0 < \alpha_1 < 90^\circ$ )
- The second converter 2 is operated as a line commutated inverter by increasing its trigger angle  $\alpha_2$  above 90 ( $90^\circ < \alpha_2 < 180^\circ$ ).

	<ul style="list-style-type: none"> <li>• The trigger angles <math>\alpha_1</math> and <math>\alpha_2</math> are adjusted such that they produce the same average dc output voltage across the load terminals.</li> <li>• Instantaneous output voltages of two converters are out of phase, this voltage difference causes circulating current between two converters.</li> <li>• This cannot flow through the load, and it is limited by limiting reactor.</li> <li>• In the circulating current mode a current builds up between the two converters even when the load current falls to zero.</li> <li>• In order to limit the circulating current flowing between the two converters, we have to include current limiting reactors in series between the output terminals of the two converters.</li> </ul> <p><b>Significance of circulating current</b></p> <ul style="list-style-type: none"> <li>• We can have faster reversal of load current as the two converters are in a state of conduction simultaneously.</li> <li>• This greatly improves the dynamic response of the output giving a faster dynamic response.</li> <li>• The output voltage and the load current can be linearly varied by adjusting the trigger angles <math>\alpha_1</math> and <math>\alpha_2</math> to obtain a smooth and linear output control.</li> <li>• The control circuit becomes relatively simple.</li> <li>• Output response is very fast.</li> <li>• The load current is free to flow in either direction at any time.</li> </ul> <p>The reversal of the load current can be done in a faster and smoother way.</p>			
7a	Explain working of step-down chopper. Draw the relevant waveform. Derive an expression for average and output rms voltage.	5	CO5	L2

# Step-down Chopper with RL Load



➤ A dc-dc converter with an  $RL$  load is shown in Figure.

➤ The operation of the converter can be divided into two modes.

➤ During mode 1, the converter is switched on and the current flows from the supply to the load.

➤ During mode 2, the converter is switched off and the load current continues to flow through freewheeling diode  $D$

## Modes of Operation

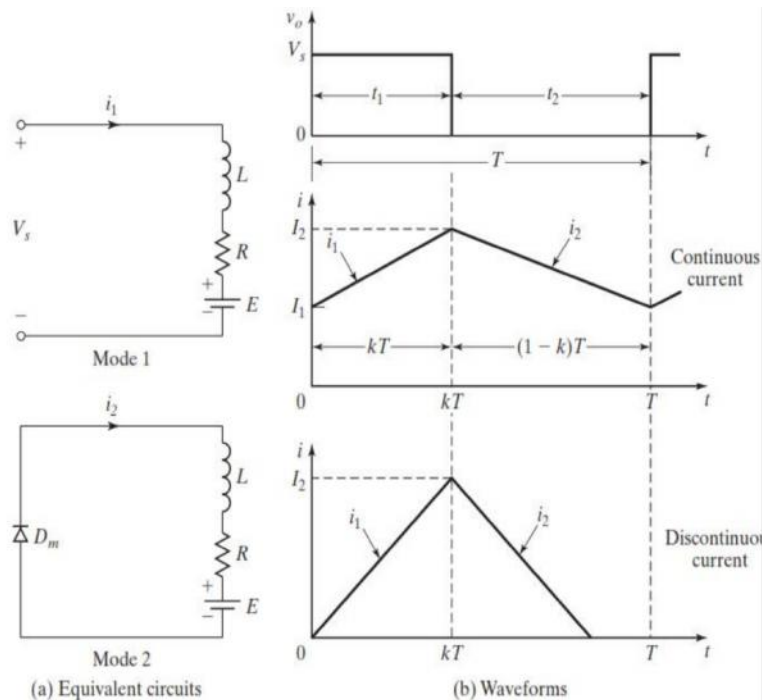
Current may be

- Continuous
- Discontinuous

### Assumption

load current rises linearly.

However, the current flowing through an  $RL$  load rises or falls exponentially with a time constant.



(a) Equivalent circuits

(b) Waveforms

The load time constant ( $\tau = L/R$ )

The load current for mode 1 can be found from

$$V_s = Ri_1 + L \frac{di_1}{dt} + E$$

which with initial current  $i_1(t=0) = I_1$  gives the load current as

$$i_1(t) = I_1 e^{-t/RL} + \frac{V_s - E}{R} (1 - e^{-t/RL}) \quad (5.19)$$

This mode is valid  $0 \leq t \leq t_1 (=kT)$ ; and at the end of this mode, the load current becomes

$$i_1(t = t_1 = kT) = I_2 \quad (5.20)$$

The load current for mode 2 can be found from

$$0 = Ri_2 + L \frac{di_2}{dt} + E$$

With initial current  $i_2(t=0) = I_2$  and redefining the time origin (i.e.,  $t = 0$ ) at the beginning of mode 2, we have

$$i_2(t) = I_2 e^{-t/RL} - \frac{E}{R} (1 - e^{-t/RL}) \quad (5.21)$$

This mode is valid for  $0 \leq t \leq t_2 [(1-k)T]$ . At the end of this mode, the load current becomes

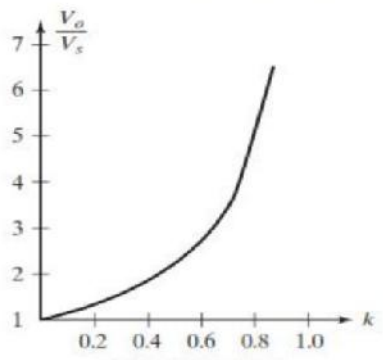
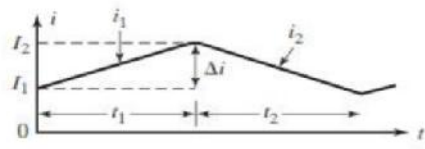
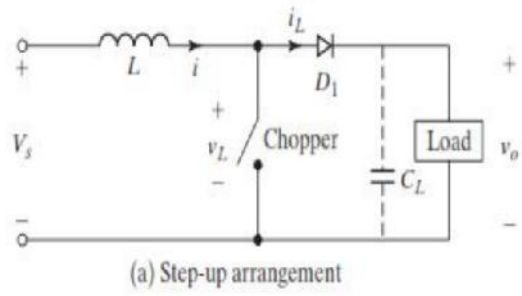
$$i_2(t = t_2) = I_3 \quad I_3 = I_1 \quad (5.22)$$

7b Explain the operation of step-up chopper. Draw the relevant waveform. Derive an expression for average output voltage.

5 CO5 L2

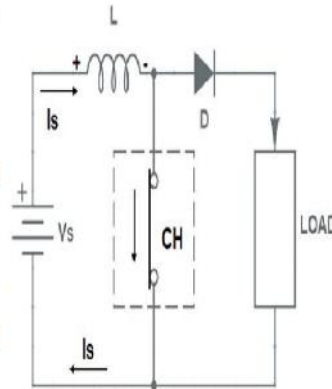
- Step-up chopper is a static device whose average output DC voltage is greater than its input DC voltage.
- A converter can be used to step-up a dc voltage and an arrangement for step-up operation. When switch SW is closed for time t, the inductor current rises and energy is stored in the inductor L.
- If the switch is opened for time t1, the energy stored in the inductor is transferred to load through diode D and the inductor current falls

### Step-up Chopper



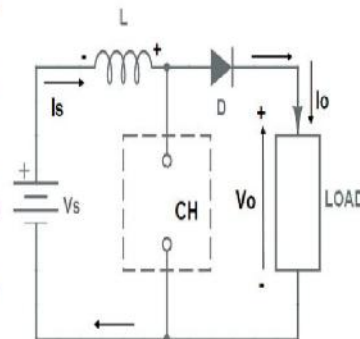
## Mode 1: Switch is ON

- When chopper (CH) is switched ON, the current will flow through the closed path formed by supply source  $V_s$ , inductor L and chopper CH.
- During this period, no current will flow through the load.
- Only source current  $i_s$  will flow and the value of load current  $i_o$  will be ZERO during the ON period.
- Also, during the  $T_{ON}$  period, energy is stored in the inductor L.
- This energy storage in L is essential to boost the load output voltage above the source voltage.
- Therefore, a large value of L is essential in a step-up chopper.



## Mode 2: Switch is OFF

- When the chopper CH is switched OFF, the current through the L can not reduce instantaneously rather it decays exponentially.
- Due to this behavior of L, it will force the current through the diode D and load for the entire time period  $T_{OFF}$ .
- Since, the current through the inductor L tends to decrease, the polarity of the emf induced in inductor L is reversed as shown in above figure.
- As a result, the voltage across the load becomes equal to the sum of source voltage and emf induced in inductor.
- Thus, the output voltage exceeds the source voltage  $V_s$ .
- The load / output voltage may be written as below.



$$V_o = V_s + L(di/dt)$$



## Average Output Voltage Equation

When the converter is turned on, the voltage across the inductor is

$$v_L = L \frac{di}{dt} \Rightarrow di = \frac{v_L}{L} dt = \frac{V_s}{L} t_1$$

and this gives the peak-to-peak ripple current in the inductor as

$$\Delta I = \frac{V_s}{L} t_1$$

The average output voltage is

$$v_o = V_s + L \frac{\Delta I}{t_2}$$

$$= V_s \left( 1 + \frac{t_1}{t_2} \right) = V_s \left( 1 + \frac{k\tau}{(1-k)\tau} \right)$$

$$= V_s \frac{1}{1-k}$$

$$v_o = V_s \frac{1}{1-k}$$

*K value can be changed from 0 to 1.*

$$\Delta I = \frac{V_s}{L} t_1$$

$$t_1 = k\tau$$

$$t_2 = (1-k)\tau$$

8 With the neat circuit diagram and waveforms, Explain the operation of single-phase full bridge inverter supplying resistive a load.

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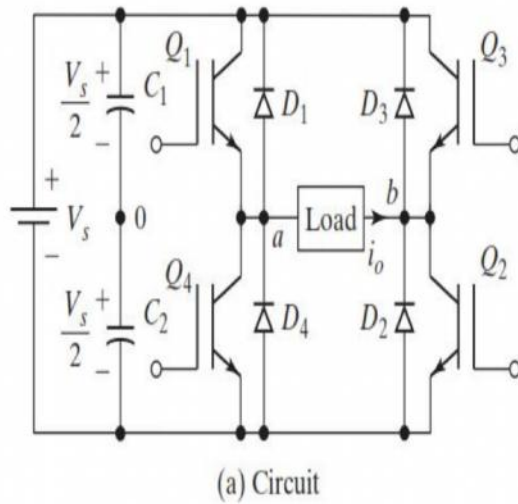
CO5

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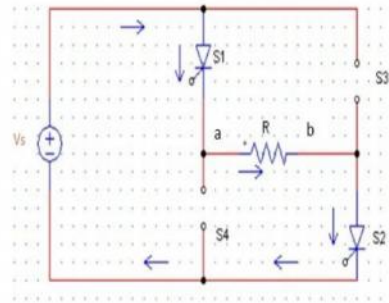
### Single Phase Bridge Inverter

- Full bridge single phase inverter is a switching device that **generates a square wave AC output voltage** on the application of **DC input** by adjusting the **switch turning ON and OFF** based on the appropriate switching sequence, where the output voltage generated is of the form **+Vs, -Vs, Or 0**.
- A single-phase bridge voltage-source inverter (VSI)
- It consists of four choppers (Q1 D1, Q2 D2, Q3 D3, Q4 D4).
- When transistors Q1 and Q2 are turned on simultaneously, the input voltage Vs appears across the load.
- If transistors Q3 and Q4 are turned on at the same time, the voltage across the load is reversed and is -Vs.

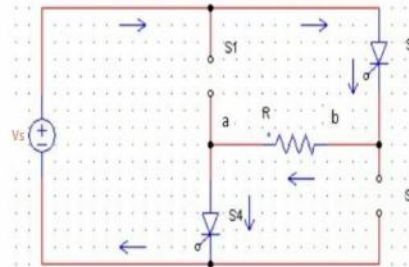
# Single Phase Bridge Inverter



Mode 1



Mode 2

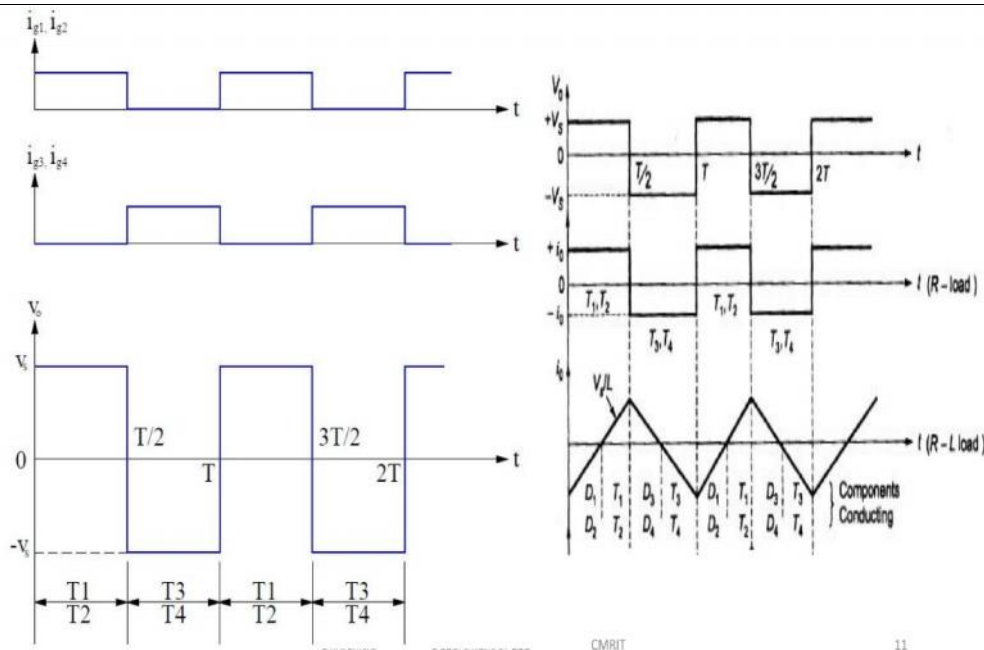


## Mode 1 (0 to T/2):-

- During this mode switch **S1** and switch **S2** are **ON** and switch **S3** and switch **S4** are **OFF** From period 0 to T/2.
- Current flowing path during this mode is  $V_s - S1 - a - R(\text{load resistor}) - b - S2 - V_s$ .
- Voltage across the load resistor is positive  $V_s$ . ( $V_o = V_s$ )

## Mode 2 (T/2 to T):-

- During this mode switch **S3** and switch **S4** are **ON** and switch **S1** and switch **S2** are **OFF** From period T/2 to T.
- Current flowing path during this mode is  $V_s - S3 - b - R(\text{load resistor}) - a - S4 - V_s$ .
- Voltage across the load resistor is negative  $V_s$ . ( $V_o = -V_s$ )



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## Switching States of single phase full bridge inverter

Switch States for a Single-Phase Full-Bridge Voltage-Source Inverter

State	State No.	Switch State*	$v_{ao}$	$v_{bo}$	$v_o$	Components Conducting
$S_1$ and $S_2$ are on and $S_4$ and $S_3$ are off	1	10	$V_s/2$	$-V_s/2$	$V_s$	$S_1$ and $S_2$ if $i_o > 0$ $D_1$ and $D_2$ if $i_o < 0$
$S_4$ and $S_3$ are on and $S_1$ and $S_2$ are off	2	01	$-V_s/2$	$V_s/2$	$-V_s$	$D_4$ and $D_3$ if $i_o > 0$ $S_4$ and $S_3$ if $i_o < 0$
$S_1$ and $S_3$ are on and $S_4$ and $S_2$ are off	3	11	$V_s/2$	$V_s/2$	0	$S_1$ and $D_3$ if $i_o > 0$ $D_1$ and $S_3$ if $i_o < 0$
$S_4$ and $S_2$ are on and $S_1$ and $S_3$ are off	4	00	$-V_s/2$	$-V_s/2$	0	$D_4$ and $S_2$ if $i_o > 0$ $S_4$ and $D_2$ if $i_o < 0$
$S_1, S_2, S_3,$ and $S_4$ are all off	5	off	$-V_s/2$ $V_s/2$	$V_s/2$ $-V_s/2$	$-V_s$ $V_s$	$D_4$ and $D_3$ if $i_o > 0$ $D_1$ and $D_2$ if $i_o < 0$



**CI**

**CCI**

**HOD**