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## Fifth Semester B.E. Degree Examination, Feb./Mar.2022

### Electrical Machine Design

Time: 3 hrs.

Max. Marks: 100

- Note: 1. Answer any FIVE full questions, choosing ONE full question from each module.  
2. Assume any missing data suitably.*

#### Module-1

- 1 a. What are the important considerations for the design of electrical machines? Explain in brief and what are its limitations? (10 Marks)  
b. Mention the desirable properties of electrical insulating materials. Also give the classification of insulating material based on temperature with an example for each. (10 Marks)

OR

- 2 a. What are the desirable properties of magnetic materials? Explain in brief magnetic material and its classification. (10 Marks)  
b. Write brief note on modern manufacturing techniques in the design of electrical machines. (10 Marks)

#### Module-2

- 3 a. Discuss the various factors which govern the choice of number of poles in a DC machine. And what are the advantages of choosing larger number of poles. (10 Marks)  
b. Calculate the diameter and length of armature for a 7.5 kW, 4 pole, 1000 rpm, 220 V shunt motor. Given : Full load efficiency 83%, Maximum gap flux density =  $0.9 \text{ wb/m}^2$ ; Specific electric loading = 30000 ampere conduction per metre ; field form factor = 0.7. Assume that the maximum efficiency occurs at full load and the field current is 2.5% of rated current. The pole face is square. (10 Marks)

OR

- 4 a. The following particulars refer to the shunt field coil for a 440 V, 6 pole, DC generator :  
MMF per pole = 7000 A, Depth of winding = 50 mm, Length of inner turn = 1.1 m; Length of outer turn = 1.4 m, Loss radiated from outer surface excluding ends =  $1400 \text{ W/m}^2$ , Space factor = 0.62 ; Resistivity =  $0.02 \text{ } \Omega/\text{m}$  and  $\text{mm}^2$ . Calculate  
(i) The diameter of the wire (ii) Length of coil  
(iii) Number of turns and (iv) Exciting current (10 Marks)  
b. Define specific electric and magnetic loadings of a DC machines. What are the merits and demerits of selecting higher value of specific loadings? Mention the factors to be consider during the choice of specific loading. (10 Marks)

#### Module-3

- 5 a. Derive the output equation of a 3 phase core type transformer and hence deduce an expression for output-emf/turn. (10 Marks)  
b. Determine the dimension of core and yoke for a 200 KVA, 50 Hz single phase core type transformer. A cruciform core is used with distance between adjacent limbs equal to 1.6 times the width of core laminations. Assume voltage per turn 14 V, maximum flux density  $1.1 \text{ wb/m}^2$ , windows space factor 0.32, current density  $3 \text{ A/mm}^2$  and stacking factor = 0.9. The net iron area is  $0.56 d^2$  in a cruciform core where d is diameter of circumscribing circle. Also the width of largest stamping is  $0.85 d$ . (10 Marks)

Important Note : 1. On completing your answers, compulsorily draw diagonal cross lines on the remaining blank pages.  
2. Any revealing of identification, appeal to evaluator and /or equations written eg, 42+8 = 50, will be treated as malpractice.

OR

- 6 a. Explain the procedure to calculate the no load current for a single phase transformer. (10 Marks)
- b. A 250 KVA, 6600/400 V, 3 phase core type transformer has a total loss of 4800 W at full load. The transformer tanks is 1.25 m in height and  $1\text{m} \times 0.5\text{m}$  in plan. Design a suitable scheme for tubes if the average temperature rise is to be limited to  $35^\circ\text{C}$ . The diameter of tubes is 50 mm and are spaced 75 mm from each other. The average height of tubes is 1.05 m. Specific heat dissipation due to radiation and convection is respectively 6 and  $6.5 \text{ W/m}^2 - ^\circ\text{C}$ . Assume that convection is improved by 35 percent due to provision of tubes. (10 Marks)

Module-4

- 7 a. Derive expression for rotor bar and end ring current of squirrel cage induction motor. (10 Marks)
- b. Find the main dimension of a 15 kW, 3 phase, 400 V, 50 Hz, 2810 rpm squirrel cage induction motor having an efficiency of 0.88 and a full load power factor of 0.9.  
Assume :  
Specific magnetic loading =  $0.5 \text{ wb/m}^2$   
Specific electric loading =  $25000 \text{ A/m}$   
Take the rotor peripheral speed as approximately 20 m/s at synchronous speed. (10 Marks)

OR

- 8 a. With usual notations, derive the output equations of a 3 phase induction machine. (10 Marks)
- b. Discuss the factors to be considered while deciding the length of air gap, number of stator and rotor slots in an induction motor. (10 Marks)

Module-5

- 9 a. What is SCR of a synchronous machine? What are the effects of SCR on machine performance? (10 Marks)
- b. Determine the main dimensions for a 1000 KVA, 50 Hz, 3 phase, 375 rpm alternator. The average air gap flux density is  $0.55 \text{ wb/m}^2$  and the ampere conductors per meter are 28000. Use rectangular poles and assume a suitable value for ratio of core length of pole pitch in order that bolted on pole construction is used for which the maximum permissible peripheral speed is 50 m/s. The runaway speed is 1.8 times the synchronous speed. (10 Marks)

OR

- 10 a. The fields coils of a salient pole alternator are wound with a single layer winding of bare copper strip 30 mm deep, with separating insulation 0.15 mm thick. Determine a suitable winding length, number of turns and thickness of conductor to develop an mmf of 12000 A with a potential difference of 5 V per coil and with a loss of  $1200 \text{ W/m}^2$  of total coil surface. The mean length of turn is 1.2 m. The resistivity of copper is  $0.021 \text{ } \Omega/\text{m}$  and  $\text{mm}^2$  (10 Marks)
- b. Explain the factors to be considered in the selection of number of armature slots of a synchronous machine. (10 Marks)

\* \* \* \* \*

## Comments from BOE EEE, to the following Subjects Scheme & Solutions

"SURESH HL" <dr.hlsuresh\_eee@sirmvit.edu>

March 16, 2022 5:30 PM

To: boe@vtu.ac.in

Dear Sir,

Please find the attached file for **Comments from BOE EEE, to the following Subjects Scheme & Solutions of 18EE55**

Regards

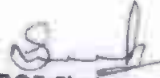
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Comments from BOE EEE, to the following Subjects Scheme & Solutions		
Subject Code	Name of Subject	Comments from BOE EEE
18EE55	Electrical Machine Design	As per the Scrutiny of same from BOE members no corrections are required

Hence the may be considered for the further Process.

  
 BOE Chairman 16/03/2022  
 EEE Composite Board  
 Dr. H L Suresh  
 Sir MVIT, Bangalore



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Visvesvaraya Technological University  
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Signature of Scrutinizer 18/11/21

18EE55

Scheme & Solutions

Subject Title : ELECTRICAL MACHINE DESIGN

Subject Code : 18EE55

Question Number	Solution	Marks Allocated									
1a,	<p>Major Consideration</p> <p>1, Cost, 2, Durability, 3, Magnetic Circuit, 4, Electric Circuit 5, Dielectric circuit, 6 Thermal circuit, 7, Mechanical Parts.</p> <p>With Explanation for Each <math>1 \times 7M = 7M</math> ✓</p> <p>Limitations in design.</p> <p>1, Saturation, 2, Temperature rise, 3, Insulation 4, Efficiency, 5, Mechanical parts, 6, Commutation 7, Power factor -</p> <p>With Explanation for Each <math>\frac{1}{2} \times 6 = 3M</math> ✓</p>	10M ✓									
b,	<p>Desirable properties of Insulating materials</p> <p>i, High dielectric strength. ii, High resistivity iii, Low dielectric hysteresis iv, Good thermal conductivity v, High degree of thermal stability</p> <p>with Explanation for Each property <math>5 \times 1M = 5M</math> ✓</p> <p>Classification based on Thermal Considerations</p> <table border="0"> <tr> <td>Class Y - <math>90^\circ</math></td> <td rowspan="6">} Explanation With Example of material <math>5M</math></td> </tr> <tr> <td>Class A - <math>105^\circ</math></td> </tr> <tr> <td>Class E - <math>120^\circ</math></td> </tr> <tr> <td>Class B - <math>130^\circ</math></td> </tr> <tr> <td>Class F - <math>155^\circ</math></td> </tr> <tr> <td>Class H - <math>180^\circ</math></td> </tr> <tr> <td>Class C - above <math>180^\circ</math>.</td> <td></td> </tr> </table>	Class Y - $90^\circ$	} Explanation With Example of material $5M$	Class A - $105^\circ$	Class E - $120^\circ$	Class B - $130^\circ$	Class F - $155^\circ$	Class H - $180^\circ$	Class C - above $180^\circ$ .		10M ✓
Class Y - $90^\circ$	} Explanation With Example of material $5M$										
Class A - $105^\circ$											
Class E - $120^\circ$											
Class B - $130^\circ$											
Class F - $155^\circ$											
Class H - $180^\circ$											
Class C - above $180^\circ$ .											

Question Number	Solution	Marks Allocated
29	<p>Desirable properties of magnetic materials</p> <ol style="list-style-type: none"> <li>i. Low reluctance core should have high permeable.</li> <li>ii. High saturation index.</li> <li>iii. High Electrical resistivity</li> <li>iv. Narrow hysteresis loop.</li> <li>v. High Curie point</li> </ol> <p style="text-align: right;">with Explanation 5 x 1M = 5M ✓</p> <ol style="list-style-type: none"> <li>i. Diamagnetic</li> <li>ii. Paramagnetic</li> <li>iii. Ferromagnetic</li> <li>iv. Antiferromagnetic</li> <li>v. Ferrimagnetic material.</li> </ol> <p style="text-align: right;">with Explanation 5 x 1M = 5M</p>	10M ✓
b,	<p>Modern machine manufacturing techniques</p> <ul style="list-style-type: none"> <li>* from fraction of watts to several hundred of megawatts in a single unit.</li> <li>* Rotational speed from few revolutions to several thousand revolutions. — (2M)</li> <li>* Small size m/c, Medium size. Large size, Larger size with specializations — (2M)</li> <li>* Smaller m/c with less material</li> <li>* Magnetic material with high permeability.</li> <li>* Significant improvement in reliability.</li> <li>* Higher Electro magnetic loading</li> <li>* Reduces cost.</li> <li>* Machine work with operates satisfactory under the desired environmental condition.</li> </ul> <p style="text-align: right;">For Each point 1x6M = 6M</p>	10M ✓
<u>MODULE-2</u>		
39	<p>choice of number of poles</p> <ol style="list-style-type: none"> <li>i. Length and diameter of the machine</li> <li>ii. Consider hysteresis loss</li> </ol>	

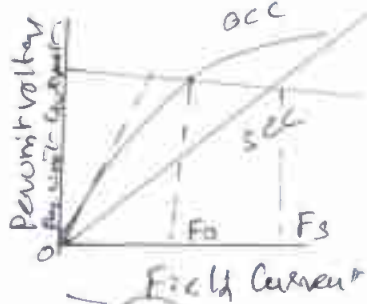
Question Number	Solution	Marks Allocated
	<p>III, Weight of the copper            IV, Length of commutator            V, Labour charges            VI, Flash over            VII, Distortion of field form</p> <p>For each point  <math>1 \text{ m} \times 7 = 7 \text{ m}</math></p> <p>Advantages of larger no of poles</p> <p>i, weight armature core &amp; yokes            ii, cost of armature and field conductors - (3m)            iii, overall length and diameter of machine</p>	10M
b,	<p>Power i/p = <math>\frac{P}{\eta} = \frac{7500}{0.83} = 9040 \text{ W}</math></p> <p>Total loss = <math>9040 - 7500 = 1540 \text{ W}</math></p> <p>constant loss = <math>\frac{1540}{2} = 770 \text{ W}</math></p> <p>motor current at full load = <math>\frac{7500}{0.83 \times 220} = 41.1 \text{ A}</math></p> <p>Field current = <math>0.025 \times 41.1 = 1.03 \text{ A}</math></p> <p>Friction and windage loss = <math>770 - 220 = 543 \text{ W}</math></p> <p><math>B_{av} = k_f B_g = 0.7 \times 0.9 = 0.63 \text{ T/m}^2</math></p> <p><math>C_o = \pi^2 \times 0.63 \times 30000 \times 10^{-3} = 186.5</math></p> <p><math>n = \frac{1000}{60} = 16.67 \text{ rps}</math></p> <p><math>D^2 L = \frac{P_a}{C_o n} = \frac{8.1}{186.5 \times 16.67} = 2.6 \times 10^{-3} \text{ m}^3</math></p> <p>For <math>\frac{L}{\pi D} = 1</math></p> <p><math>L = 0.7 \times \frac{\pi D}{4} = 0.55 D</math></p> <p><math>0.55 D^3 = 2.61 \times 10^{-3}</math></p> <p><math>D = 0.17 \text{ m}</math></p> <p><math>L = 0.09 \text{ m}</math></p> <p>For each point <math>1 \text{ m} \times 10 = 10 \text{ m}</math></p>	10M

Question Number	Solution	Marks Allocated
4a	<p>Voltage across the shunt field winding = <math>0.8 \times 440 = 352V</math></p> <p>voltage across each field coil = <math>2.8 \times 352/6 = 58.7V</math></p> <p>length of mean turn <math>L_{mt} = \frac{L_o + L_i}{2} = \frac{1.4 + 1.1}{2} = 1.25m</math></p> <p>Area of field conductor <math>a_f = \frac{A_{fpp} L_{mt}}{E_f} = 2.98 mm^2</math></p> <p>Diameter of bare conductor <math>d = 1.95 mm</math></p> <p>no. of turns <math>T_f = \frac{S + h + d}{E_f} \times 10^6 = 1.04 \times 10^4 h_f</math></p> <p>Area of outer surface <math>L_o h_f = 1.4 h_f</math></p> <p>Permissible loss <math>\Delta t = 1960 h_f</math></p> <p>Field current <math>I_f = \frac{\Delta t}{E_f} = 33.4 h_f</math></p> <p><math>A_{fpp} = I_f T_f = 33.4 h_f \times 1.04 \times 10^4 h_f = 7000 \text{ or } T_f = 210/h_f</math></p> <p><math>T_f^2 = 1.04 \times 10^4 h_f \times \frac{210}{h_f} = 21.84 \times 10^6</math></p> <p><math>T_f = 1475</math></p> <p><math>R_f = 12.4 \Omega</math></p> <p><math>I_f = 4.73A</math></p> <p><math>h_f = \frac{T_f}{1.04 \times 10^4} = 0.142m</math></p> <p>For less value <math>1m \times 10</math></p>	10M
b.	<p><u>Specific Electro-loading</u>: The no of armature ampere conductors per meter <math>a_c = \frac{I_z Z}{\pi D}</math> - (2M)</p> <p><u>Specific Magnetic loading</u>: Average flux density over the air gap of a machine. - (1M)</p> <p><math>B_{av} = \frac{P\phi}{\pi DL}</math> - (1M)</p> <p>Advantage of higher value - (2M)</p> <p>Demerits of high value - (2M) factors to be noted (2M)</p>	10M



Question Number	Solution	Marks Allocated
59.	$Q = 3V_p I_p \times 10^{-3}$ $= 3E_p I_p \times 10^{-3} = 3E_p \Gamma_p I_p \times 10^{-3}$ $= 3E_p A \Gamma \times 10^{-3}$ $= 3 \times 4.44 f \phi_m \times \frac{k_w A_w \delta}{4} \times 10^{-3} \quad \leftarrow (7m)$ $= 3.33 f \phi_m k_w A_w \delta \times 10^{-3}$ <div style="border: 1px solid black; padding: 2px; display: inline-block;"> <math display="block">= 3.33 f B_m \delta k_w A_w A_i \times 10^{-3} \text{ (KVA)}</math> </div> <p>Voltage per turn = <math>E_p = 4.44 f \phi_m</math></p> $\sqrt{4.44 f \times 2 \times 10^3} \sqrt{Q} = K \sqrt{Q}$ $K = \sqrt{4.44 f \times 2 \times 10^3} = \left[ 4.44 f \frac{\phi_m}{A \Gamma} \times 10^3 \right]^{1/2} \quad (3m)$	10M
b.	<p>Net area <math>A_i = 0.0573 \text{ m}^2</math></p> <p>Diameter <math>d = \sqrt{A_i / 0.56} = 0.32 \text{ m}</math></p> <p>Width of largest stamping <math>a = 0.85d = 0.272 \text{ m}</math></p> <p>Distance between core centre <math>D = 1.69 = 0.435 \text{ m}</math></p> <p><math>W = D - d = 0.115 \text{ m}</math></p> <p><math>Q = 2.22 f B_m k_w \delta A_w A_i \times 10^{-3}</math></p> <p><math>200 = 2.22 \times 50 \times 1.1 \times 0.32 \times 3 \times 10^6 \times A_w \times 0.0573 \times 10^{-3}</math></p> <p><math>A_w = 0.0298 \text{ m}^2 \quad H_w = \frac{0.0298}{0.115} = 0.26 \text{ m}</math></p> <p><math>D_y = 0.272 \text{ m} \quad H_y = 0.272 \text{ m}</math></p> <p>over all height of frame <math>H = H_w + 2H_y</math></p> <p><math>26 + 2 \times 0.272 = 0.804 \text{ m}</math></p> <p>over all length of frame <math>W = D + a</math></p> <p><math>43.5 + 0.272 = 0.737 \text{ m}</math></p> <p>For finding each value <math>1M \times 10 = 10M</math></p>	10M

Question Number	Solution	Marks Allocated
69	<p><math>l_c</math> - length of flux path through core  <math>l_y</math> - length of flux path through yoke.  <math>l_c = Hw, l_y = W</math></p> <p><math>I_m = \frac{A \rho_0}{\sqrt{2} \cdot TP}</math> with steps  <math>\alpha</math> 10M</p> <p><math>I_0 = \sqrt{I_m^2 + I_x^2}</math> Explanations</p>	10M
b,	<p>Total no. of tubes provided = <math>62 + 2 = 64</math> (2M)  dissipating surface <math>(1+x)S_c = 3.75(1+x)</math>  Specific loss dissipation = <math>\frac{36.5}{1+x} \text{ W/m}^2 \cdot ^\circ\text{C}</math>  loss dissipation = <math>\frac{125 + 88x}{1+x} \text{ W/m}^2 \cdot ^\circ\text{C}</math>  <math>x = 2.73</math> (3M)  diagram - (3M) Explanations (2M)</p>	10M
74.	<p>Expression for rotor bar - (5M)  Design of End ring - diagram - 3M  Explanations - 2M</p>	10M
b.	<p><math>Q = \frac{15}{0.88 \times 10^9} = 18.34</math> <math>C_0 = 11k_w B_{av} G_c \times 10^{-3}</math>  <math>= 181.3</math>  The rotor speed is 2800 rpm nearest synchronous speed is 3000 rpm.  <math>n_s = 50 \text{ rps}</math> <math>D^2 L = \frac{Q}{C_0 n_s} = 2.88 \times 10^{-3} \text{ m}^3</math>  The rotor diameter is an almost equal to stator bore.  <math>\pi D n_s = 20 \Rightarrow D = 0.1257 \text{ m}</math>  <math>L = \frac{2.88 \times 10^{-3}}{(0.1257)^2} = 0.174 \text{ m}</math></p>	10M

Question Number	Solution	Marks Allocated
8a	<p>Output Equation of 3<math>\phi</math> Induction motor</p> $Q = 1.11 kW \text{ pp } \frac{1}{2} \pi \tau l_s \times 10^{-3}$ $Q = (11 \text{ Bav ac kw } \times 10^{-3}) D^2 L_m$ <div style="border: 1px solid black; padding: 5px; display: inline-block;"> <math>Q = C_o D^2 L_m</math> </div> <p style="text-align: right;">with usual notation derivations for output equation</p>	10M
b	<p>Power factor, Iron loss overloading capacity } for air gap. with Explanation</p> <p style="text-align: center;">(4M)</p> <p>No of stator slots &amp; rotor slots</p> <ul style="list-style-type: none"> <li>i. Tooth pulse losses</li> <li>ii. Leakage reactance</li> <li>iii. Ventilation</li> <li>iv. Magnetizing current &amp; iron losses</li> <li>v. Cost</li> </ul> <p style="text-align: right;">for each condition 1 x 6m = 6m with Explanation</p>	10M
9a	<p>Short circuit ratio</p> $SCR = \frac{O F_o}{O F_s} = \frac{C F_o}{B F_s}$ <div style="border: 1px solid black; padding: 5px; display: inline-block;"> <math>SCR = \frac{1}{X_d}</math> </div> <p style="text-align: center;">(2M)</p> <p style="text-align: center;">with Explanation (2M)</p> <div style="display: flex; align-items: center;">  </div> <p>Effect of SCR</p> <ul style="list-style-type: none"> <li>i. voltage regulation</li> <li>ii. Stability</li> <li>iii. Parallel operation</li> <li>iv. Short circuit currents</li> <li>v. Self Excitation</li> </ul> <p style="text-align: right;">For Each point with Explanation 1 x 5 = 5M</p>	10M

Question Number	Solution	Marks Allocated
96	$n_s = \frac{375}{60} = 6.25 \text{ rps.}$ $p = \frac{2 \times 50}{6.25} = 16$ <p>Assume a winding factor of 0.995</p> $\omega = 11 \text{ Ku Bav ae } \times 10^{-3} = 162.$ $D^2 L = 0.987 \text{ m}^3$ <p>Taking <math>\frac{L}{D} = 2</math> <span style="float: right;">1 x 10 m</span></p> $L = 0.393 D$ $0.393 D^3 = 0.987$ $D = 1.36 \text{ m and } L = 0.535 \text{ m}$ <p>Peripheral speed = <math>\pi D n_s = 26.7 \text{ m/s}</math></p>	10m
109	<p>Field conductor <math>af = 60.4 \text{ mm}^2</math></p> <p>Height of conductor = <math>\frac{60.4}{30} = 2 \text{ mm}</math></p> <p>Area of conductor = <math>30 \times 2 = 60 \text{ mm}^2</math></p> <p>Heat dissipating surface = <math>2 l_m t_f (h_f + d_f)</math></p> $= 2.4 h_f + 0.272$ $d_f = 1200 (2.4 h_f + 0.272) = 2880 h_f + 86.4$ $I_f = \frac{d_f}{E_f} = \frac{2880 h_f + 86.4}{E_f}$ $= 5.72 h_f + 17.3$ <p>Field mmf = <math>I_f T_f = (5.72 h_f + 17.3) T_f</math></p> $T_f = 91$ $h_f = 186 \text{ mm}$	10m

Question Number	Solution	Marks Allocated
10b.	<p>Factors considered for armature slots.</p> <ul style="list-style-type: none"><li>i. Balanced winding.</li><li>ii. Cost</li><li>iii. Hot spot temperature.</li><li>iv. Leakage reactance.</li><li>v. Tooth ripples</li><li>vi. Flux density in iron.</li></ul> <p>Each factors with explanation.</p> <p style="text-align: right;"><math>2 \times 5 = 10M</math></p>	10M
	<p><b>* APPROVED *</b></p> <p><i>[Signature]</i></p> <p><b>Registrar (Evaluation)</b></p> <p>Vijayavardhana Technological University</p> <p>BELAGAVI - 590018</p> <p><i>[Initials]</i></p>	