

USN

## Internal Assessment Test 4 –Feb. 2022

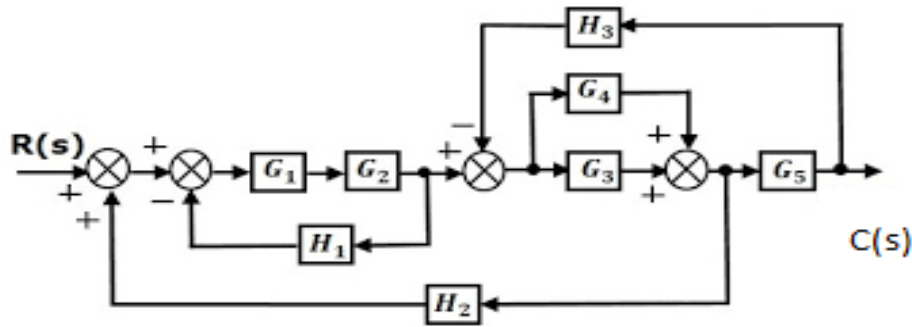
Sub:	Control Engineering	Sub Code:	18ME71/17ME73/ 15ME73	Branch:	ME
Date:	01.02.22	Duration:	90 min's	Max Marks:	50
		Sem/Sec:	VII/A&B		OBE

Answer All the Questions

MARKS

CO  
RB  
T

1

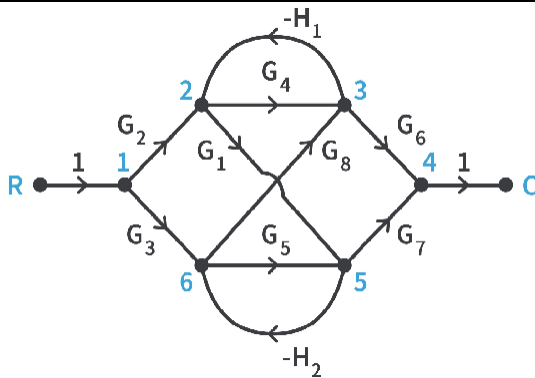


[10]

CO2  
L3

Reduce the block diagram and determine transfer function of the given system.

2

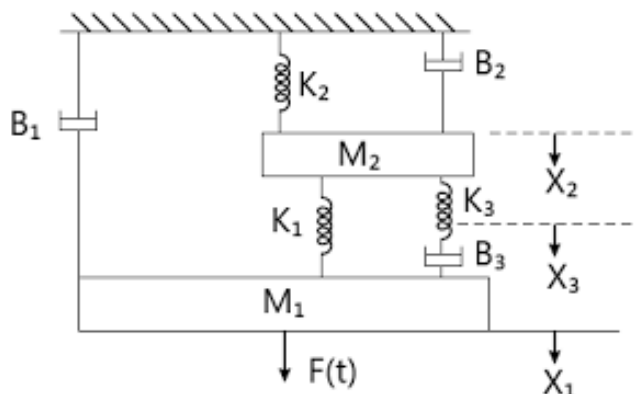


[10]

CO2  
L3

Determine the transfer function of the given system using Mason's Gain Formula.

3



[10]

CO1  
L3

Draw equivalent mechanical system of the given system. Hence write the set of equilibrium equations for it and obtain electrical analogous circuits using FV and FI analogy.

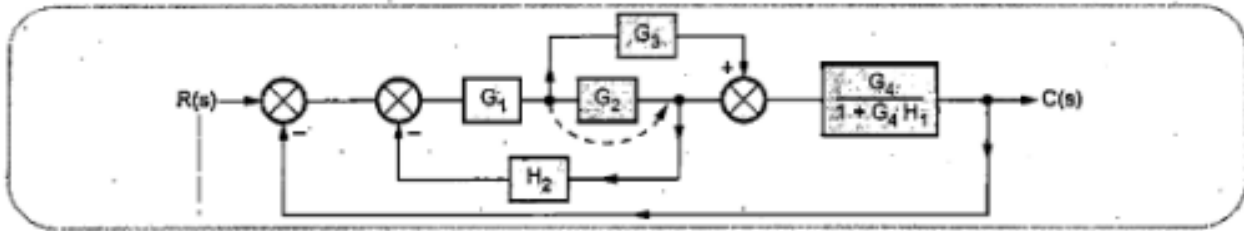
4.	Obtain the expression for peak time and rise time for a second order control system in terms of damping factor and natural frequency.	[10]	CO3	L3
5.	<p>A unity feedback system is characterised by open loop transfer function</p> $G(s) = \frac{16}{s(s+2)}$ <p>If the system is subjected to unit step input, determine:</p> <ul style="list-style-type: none"> <li>i) Undamped natural frequency</li> <li>ii) Damping ratio</li> <li>iii) Peak overshoot</li> <li>iv) Peak time</li> <li>v) Settling time</li> </ul>	[10]	CO4	L3

Faculty Signature

CCI Signature

HOD Signature

1)



Shift take off point of  $G_3$  after the block  $G_2$ .

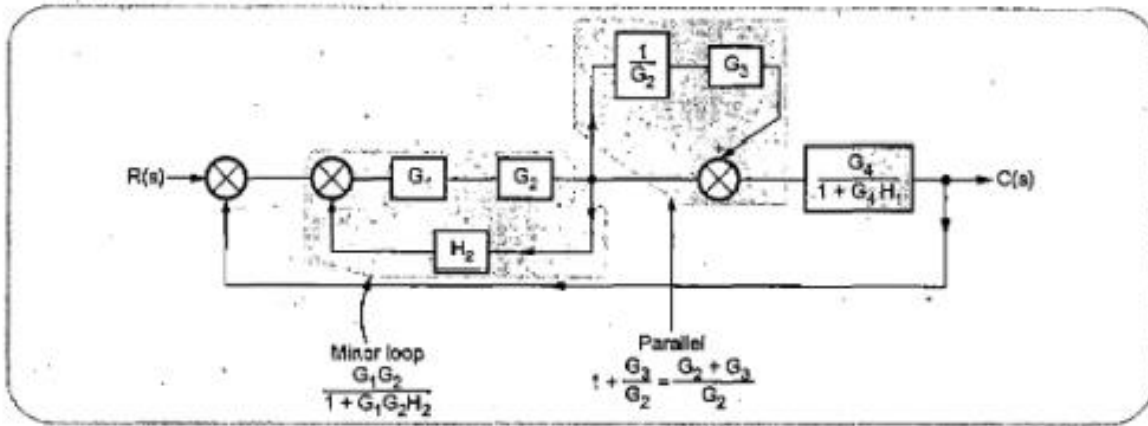


Fig. 5.3.37 (b)

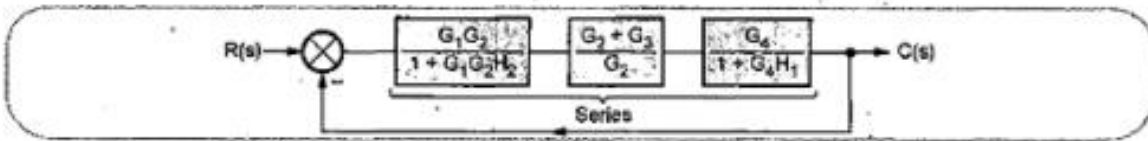


Fig. 5.3.37 (c)

$$\therefore \frac{C(s)}{R(s)} = \frac{G_1 G_4 (G_2 + G_3)}{(1 + G_1 G_2 H_2) (1 + G_4 H_1)} \cdot \frac{1}{1 + \frac{G_1 G_4 (G_2 + G_3)}{(1 + G_1 G_2 H_2) (1 + G_4 H_1)}}$$

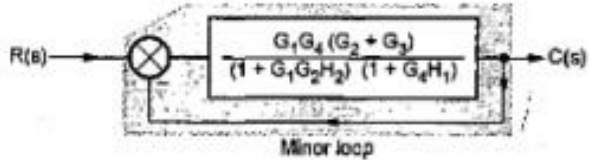


Fig. 5.3.37 (d)

$$\therefore \frac{C(s)}{R(s)} = \frac{G_1 G_4 (G_2 + G_3)}{1 + G_1 G_2 H_2 + G_4 H_1 + G_1 G_2 G_4 H_1 H_2 + G_1 G_2 G_4 + G_1 G_3 G_4}$$

2)

Sol : The number of forward paths are  $K = 6$ .

The forward path gains are,

$$T_1 = G_1 G_2 G_3, \quad T_2 = G_4 G_5 G_6$$

$$T_3 = G_1 G_7 G_8, \quad T_4 = G_4 G_8 G_3$$

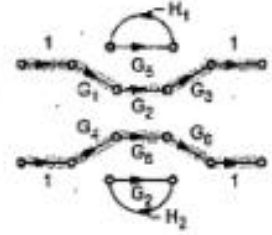
$$T_5 = G_4 G_8 (-H_2) G_7 G_6, \quad T_6 = G_1 G_7 (-H_1) G_8 G_3$$

The feedback loop gains are,

$$L_1 = -G_5 H_1, \quad L_2 = -G_2 H_2, \quad L_3 = +G_7 H_1 G_8 H_2$$

The two nontouching loops are  $L_1, L_2$ .

$$\therefore L_1 L_2 = +G_2 G_5 H_1 H_2$$



$$\therefore \Delta = 1 - [L_1 + L_2 + L_3] + [L_1 L_2] = 1 + G_5 H_1 + G_2 H_2 - G_7 G_8 H_1 H_2 + G_2 G_5 H_1 H_2$$

For  $T_1$ ,  $L_1$  is nontouching.

$$\therefore \Delta_1 = 1 - L_1 = 1 + G_5 H_1$$

For  $T_2$ ,  $L_2$  is nontouching.

$$\therefore \Delta_2 = 1 - L_2 = 1 + G_2 H_2$$

For  $T_3$  to  $T_6$  all loops are touching to all forward paths.

$$\therefore \Delta_3 = \Delta_4 = \Delta_5 = \Delta_6 = 1$$

$$\therefore \text{Gain} = \frac{\sum T_K \Delta_K}{\Delta} = \frac{T_1 \Delta_1 + T_2 \Delta_2 + T_3 \Delta_3 + T_4 \Delta_4 + T_5 \Delta_5 + T_6 \Delta_6}{\Delta}$$

$$\therefore \text{Gain} = \frac{G_1 G_2 G_3 (1 + G_5 H_1) + G_4 G_5 G_6 (1 + G_2 H_2) + G_1 G_7 G_8 + G_4 G_8 G_3 - G_4 G_8 G_7 G_6 H_2 - G_1 G_3 G_7 G_8 H_1}{1 + G_5 H_1 + G_2 H_2 - G_7 G_8 H_1 H_2 + G_2 G_5 H_1 H_2}$$

... Ans.

3)

$$f(t) = M_1 \frac{d^2 x_1}{dt^2} + K_1 (x_1 - x_2) + B_1 \frac{d(x_1 - x_2)}{dt}$$

$$0 = K_1 (x_2 - x_1) + B_1 \frac{d(x_2 - x_1)}{dt} + M_2 \frac{d^2 x_2}{dt^2} + B_2 \frac{dx_2}{dt} + K_2 x_2$$

i) F-V analogy : Use  $F \rightarrow V$ ,  $M \rightarrow L$ ,  $B \rightarrow R$ ,  $K \rightarrow \frac{1}{C}$ ,  $x \rightarrow q$ ,

$$\frac{dx}{dt} \rightarrow i, x \rightarrow \int i dt, \frac{d^2 x}{dt^2} \rightarrow \frac{di}{dt}$$

$$v(t) = L_1 \frac{di_1}{dt} + \frac{1}{C_1} \int (i_1 - i_2) dt + R_1 (i_1 - i_2)$$

$$0 = R_1 (i_2 - i_1) + \frac{1}{C_1} \int (i_2 - i_1) dt + L_2 \frac{di_2}{dt} + R_2 i_2 + \frac{1}{C_2} \int i_2 dt$$

Based on loop basis, F-V network is shown in the Fig. 4.8.9 (b).

ii) F-I analogy : Use  $F \rightarrow L$ ,  $M \rightarrow C$ ,  $B \rightarrow \frac{1}{R}$ ,  $K \rightarrow \frac{1}{L}$ ,  $x \rightarrow \phi$ ,

$$\frac{dx}{dt} \rightarrow v(t), x \rightarrow \int v(t) dt, \frac{d^2 x}{dt^2} \rightarrow \frac{dv(t)}{dt}$$

$$i(t) = C_1 \frac{dv_1(t)}{dt} + \frac{1}{L_1} \int (v_1 - v_2) dt + \frac{1}{R_1} (v_1 - v_2)$$

$$0 = \frac{1}{L_1} \int (v_2 - v_1) dt + \frac{1}{R_1} (v_2 - v_1) + C_2 \frac{dv_2}{dt} + \frac{1}{R_2} v_2 + \frac{1}{L_2} \int v_2 dt$$

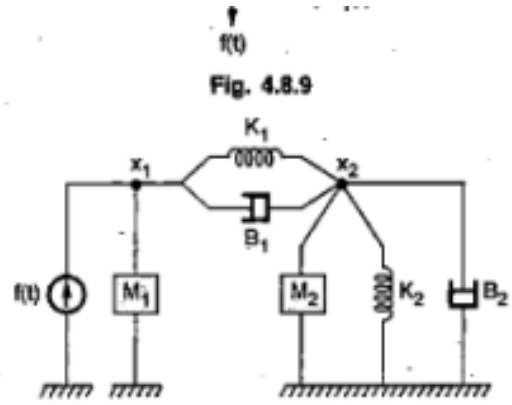


Fig. 4.8.9 (a)

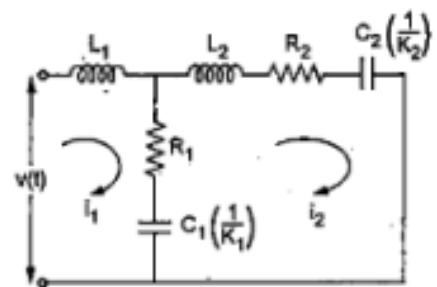


Fig. 4.8.9 (b) F-V analogy

4)

**Derivation of Peak Time  $T_p$**

Transient response of second order underdamped system is given by,

$$c(t) = 1 - \frac{e^{-\xi \omega_n t}}{\sqrt{1-\xi^2}} \sin(\omega_d t + \theta) \quad \text{where } \theta = \tan^{-1} \frac{\sqrt{1-\xi^2}}{\xi}$$

As at  $t = T_p$ ,  $c(t)$  will achieve its maxima. According to Maxima theorem,

$$\left. \frac{dc(t)}{dt} \right|_{t=T_p} = 0$$

So differentiating  $c(t)$  w.r.t. 't' we can write,

$$\text{i.e. } -\frac{e^{-\xi \omega_n t} (-\xi \omega_n) \sin(\omega_d t + \theta)}{\sqrt{1-\xi^2}} - \frac{e^{-\xi \omega_n t}}{\sqrt{1-\xi^2}} \omega_d \cos(\omega_d t + \theta) = 0$$

Substituting  $\omega_d = \omega_n \sqrt{1-\xi^2}$

$$\frac{\xi \omega_n e^{-\xi \omega_n t}}{\sqrt{1-\xi^2}} \sin(\omega_d t + \theta) - \frac{e^{-\xi \omega_n t}}{\sqrt{1-\xi^2}} \omega_n \sqrt{1-\xi^2} \cos(\omega_d t + \theta) = 0$$

$$\xi \sin(\omega_d t + \theta) - \sqrt{1-\xi^2} \cos(\omega_d t + \theta) = 0 \quad \text{i.e. } \tan(\omega_d t + \theta) = \frac{\sqrt{1-\xi^2}}{\xi}$$

$$\text{Now } \theta = \tan^{-1} \frac{\sqrt{1-\xi^2}}{\xi} \quad \text{i.e. } \frac{\sqrt{1-\xi^2}}{\xi} = \tan \theta$$

$$\tan(\omega_d t + \theta) = \tan \theta$$

From trigonometric formula,

$$\tan(n\pi + \theta) = \tan \theta$$

$$\omega_d t = n\pi \quad \text{where } n = 1, 2, 3$$

But  $T_p$ , time required for first peak overshoot.  $\therefore n = 1$

$$\omega_d T_p = \pi$$

$$T_p = \frac{\pi}{\omega_d} = \frac{\pi}{\omega_n \sqrt{1-\xi^2}} \text{ sec}$$

$\{c(t)\}_{t=T_r} = 1$  for unit step input

$$\therefore 1 = 1 - \frac{e^{-\xi \omega_n T_r}}{\sqrt{1-\xi^2}} \sin(\omega_d T_r + \theta)$$

$$\therefore -\frac{e^{-\xi \omega_n T_r}}{\sqrt{1-\xi^2}} \sin(\omega_d T_r + \theta) = 0$$

Equation will get satisfied only if,

$$\sin(\omega_d T_r + \theta) = 0$$

Trigonometrically this is true only if,

$$\omega_d T_r + \theta = n\pi \quad \text{where } n = 1, 2, \dots$$

As we are interested in first attempt use  $n = 1$

$$\therefore \omega_d T_r + \theta = \pi$$

$$\therefore T_r = \frac{\pi - \theta}{\omega_d} \text{ sec}$$

5)

Sol. : From given  $G(s)$ , the closed loop T.F. is,

$$\frac{C(s)}{R(s)} = \frac{G(s)}{1 + G(s)H(s)} = \frac{10}{s^2 + 2s + 16}$$

Comparing denominator with  $s^2 + 2\xi\omega_n s + \omega_n^2$ ,

$$\omega_n^2 = 16, \omega_n = 4, 2\xi\omega_n = 2, \xi = 0.25$$

i)  $\omega_n = 4$  rad/sec

ii)  $\xi =$  Damping ratio = 0.25

iii)  $\% M_p = e^{-\pi\xi/\sqrt{1-\xi^2}} \times 100 = 44.43 \%$

iv)  $\omega_d = \omega_n \sqrt{1-\xi^2} = 3.873$  rad/sec

$\therefore T_p = \frac{\pi}{\omega_d} = 0.811$  sec

v)  $T_v = \frac{4}{\xi\omega_n} = 4$  sec