



Internal Assessment Test 1 – May 2022

Sub: Finite Element Methods
Date: <u>06/05/2022</u> Duration: <u>90 mins</u> Max Marks: <u>50</u> Sem: <u>VI</u>

Code: 18ME61
Branch: MECH

Marks	OBE	
	CO	RBT
8	CO1	L2
2	CO1	L1
10	CO3	L2
10	CO2	L3

- 1 Explain the basic steps involved in FEM.
- 2 Write the equilibrium equation for 2D state of stress.
- 3 Derive stiffness matrix for one dimensional bar element.
- 4 A cantilever beam of span 'L' is subjected to a point load at free end. Derive an equation for the deflection at free end by using RR method. Assume polynomial displacement function.



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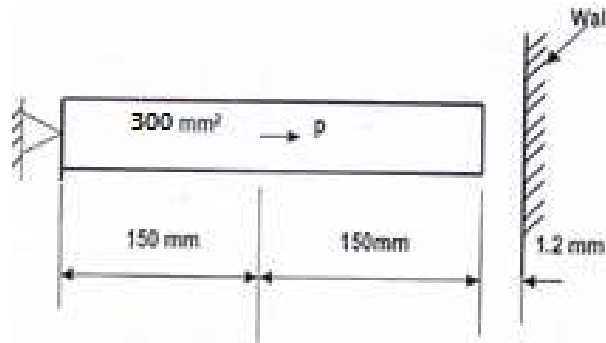
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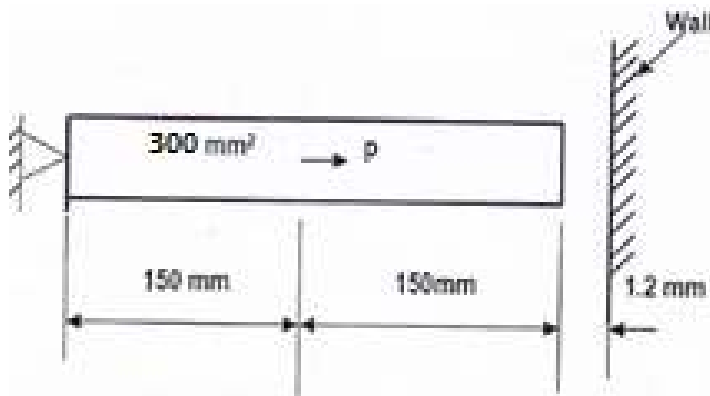
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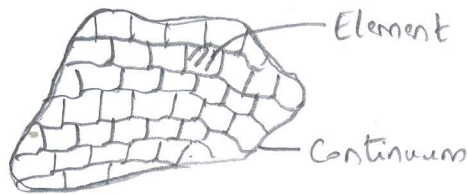
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1 STEPS IN FEA1. Discretization of given Continuum

In this step, the continuum is subdivided into number of parts called finite elements. The type of element selected depends on the kind of analysis namely 1D, 2D or 3D.

2. Selection of displacement model for each element

The displacement variation for each element is unknown. Hence a mathematical model is represented for each finite element. They can be either polynomial or trigonometric functions.

3. Generation of stiffness matrix for each finite element4. To derive global stiffness matrix

$$K = K_1 + K_2 \dots$$

5. Imposing the equilibrium equation

$$[K][q] = [F]$$

6) Enforcing the boundary conditions of the given problem

There are two methods to enforce the boundary

Condition

i) Elimination method - We eliminate the corresponding rows & columns where we have constraints

ii) Penalty Method - Add a constant $C = |\max k_{ij}| \times 10^4$ to the first & last element of diagonal.

7) Determination of unknowns.

In this step, the unknowns such as stresses, displacements, strains etc are found.

2. Equilibrium equations for 2D state of stress

$$\frac{\partial \sigma_x}{\partial x} + \frac{\partial \tau_{xy}}{\partial y} + X = 0$$

$$\frac{\partial \tau_{yx}}{\partial x} + \frac{\partial \sigma_y}{\partial y} + Y = 0$$

3. Stiffness matrix for one dimensional bar element

$$\text{Strain energy for 3 D element } U_e = \frac{1}{2} \int_V \sigma^T \epsilon \, dv$$

$$\text{Strain energy for 1D element } U_e = \frac{1}{2} \int_{l_e} \sigma^T \epsilon \, A \, dx$$

$$\text{Strain } \epsilon = Bq$$

$$\text{where } B = \frac{1}{l_e} [-1 \quad 1]$$

$$q = \begin{bmatrix} q_1 \\ q_2 \end{bmatrix}$$

$$\text{Strain energy for 1D element } U_e = \frac{1}{2} \int_{l_e} [EBq]^T Bq \, A \, dx$$

Relation between natural and Cartesian coordinate is

$$\xi = \frac{x-x_1}{x_2-x_1} - 1$$

$$\frac{d\xi}{dx} = \frac{2}{l_e}$$

$$U_e = \frac{1}{2} \int_{l_e} q^T B^T E Bq \, A \, \frac{l_e}{2} \, d\xi$$

$$U_e = \frac{1}{2} q^T \left[EA \frac{l_e}{2} \int_{l_e} B^T B d\xi \right] q$$

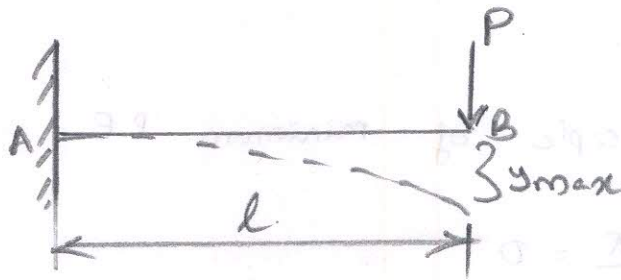
$$U_e = \frac{1}{2} q^T k_e q$$

Where $k_e = \text{stiffness matrix}$

$$k_e = EA \frac{l_e}{2} \int_{l_e} B^T B d\xi$$

$$K = \frac{EA}{l_e} \begin{bmatrix} 1 & -1 \\ -1 & 1 \end{bmatrix}$$

- 4 A Cantilever beam subjected to point load at free end. Derive an eqn for max' deflection using R.R method.



Sol \Rightarrow Potential Energy functional

$$\pi = \text{S.E} + \text{W.P}$$

(+ve) (-ve)

$$\text{S.E} = \frac{EI}{2} \int_0^l \left(\frac{d^2y}{dx^2} \right)^2 dx$$

$$\text{W.P} = P \cdot y_{max}$$

\Rightarrow Assume displacement function

$$y = a_0 + a_1x + a_2x^2 + a_3x^3$$

B.C At A, $x=0$, $y=0$ At A, $x=0$, $\frac{dy}{dx} = 0$

$$\boxed{a_0 = 0}$$

$$\frac{dy}{dx} = a_1 + 2a_2x + 3a_3x^2$$

$$\boxed{a_1 = 0}$$

$$y = a_2x^2 + a_3x^3$$

$$\frac{dy}{dx} = 2a_2x + 3a_3x^2 \quad \text{--- (1)}$$

$$\frac{d^2y}{dx^2} = 2a_2 + 6a_3x$$

$$y = y_{\max} \quad \text{at } x = l$$

$$y = a_2x^2 + a_3x^3$$

$$y_{\max} = a_2l^2 + a_3l^3$$

3) P.E functional

$$\pi = \frac{EI}{2} \int_0^l (2a_2 + 6a_3x)^2 dx - P(a_2l^2 + a_3l^3)$$

$$= \frac{EI}{2} \int_0^l [4a_2^2 + 36a_3^2x^2 + 24a_2a_3x] dx - P(a_2l^2 + a_3l^3)$$

$$= \frac{EI}{2} \left[4a_2^2x + 36a_3^2 \frac{x^3}{3} + 24a_2a_3 \frac{x^2}{2} \right]_0^l - P(a_2l^2 + a_3l^3)$$

$$\pi = \frac{EI}{2} \left[4a_2^2l + 36a_3^2 \frac{l^3}{3} + 24a_2a_3 \frac{l^2}{2} \right] - P(a_2l^2 + a_3l^3)$$

4) Using Principle of minimum P.E

$$\frac{\partial \pi}{\partial a_2} = 0 \quad ; \quad \frac{EI}{2} [8a_2l + 12a_3l^2] - Pl^2 = 0 \quad \rightarrow \text{(1)}$$

$$\frac{\partial \pi}{\partial a_3} = 0 \quad ; \quad \frac{EI}{2} [24a_3l^3 + 12a_2l^2] - Pl^3 = 0 \quad \rightarrow \text{(2)}$$

Max deflection

$$y_{\max} = a_2 l^2 + a_3 l^3$$

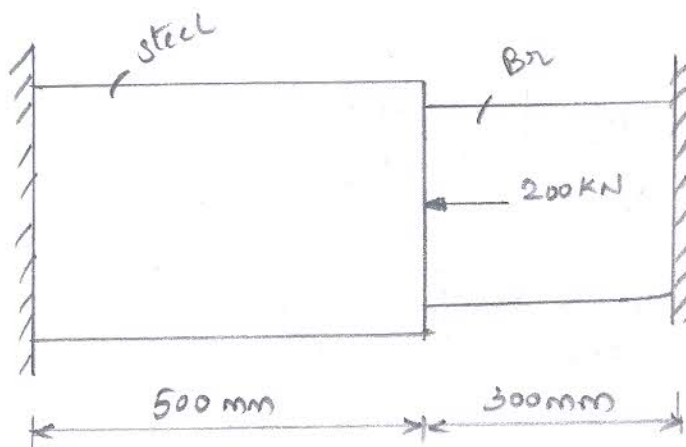
$$= \frac{P \cdot l^3}{2EI} - \frac{Pl^3}{6EI}$$

$$y_{\max} = \frac{Pl^3}{3EI}$$

$$\left[\frac{12}{l^3} \frac{Pl^3}{3EI} + \frac{12}{l^3} \frac{Pl^3}{3EI} + \frac{12}{l^3} \frac{Pl^3}{3EI} \right] \frac{12}{l^3} = \frac{12}{l^3}$$

5

A Compound bar 800 mm long is made of Steel of 500 mm length with an area of 400 mm^2 with the remaining length made of brass having an area of 300 mm^2 . At the junction it is subjected to an axial load of 200 kN which is in compression to steel. Both the ends are fixed. $E_{st} = 200 \text{ GPa}$; $E_{br} = 70 \text{ GPa}$. Using Penalty method find the foll. nodal displacement, stress in each element, reaction at supports.

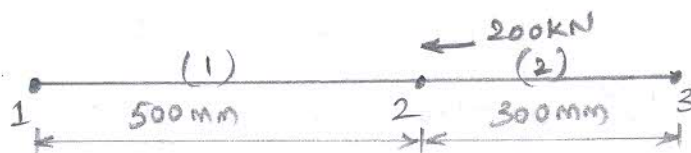
Sol

$$E_{st} = 200 \text{ GPa}$$

$$E_{br} = 70 \text{ GPa}$$

$$A_1 = 400 \text{ mm}^2$$

$$A_2 = 300 \text{ mm}^2$$

F.E. Model

Stiffness matrix for each element

For element 1

$$K_1 = \frac{E_{st} A_1}{L_1} \begin{bmatrix} 1 & -1 \\ -1 & 1 \end{bmatrix}$$

$$= \frac{200 \times 10^3 \times 400}{500} \begin{bmatrix} 1 & -1 \\ -1 & 1 \end{bmatrix}$$

$$K_1 = 10^5 \begin{bmatrix} 1 & 2 \\ -1.6 & 1.6 \end{bmatrix} \begin{matrix} 1 \\ 2 \end{matrix}$$

For element 2

$$K_2 = \frac{E_{br} \cdot A_2}{L_2} \begin{bmatrix} 1 & -1 \\ -1 & 1 \end{bmatrix}$$

$$= \frac{70 \times 10^3 \times 300}{300} \begin{bmatrix} 1 & -1 \\ -1 & 1 \end{bmatrix}$$

$$= 10^5 \begin{bmatrix} 2 & 3 \\ -0.7 & 0.7 \end{bmatrix} \begin{matrix} 2 \\ 3 \end{matrix}$$

Global stiffness matrix

$$K = K_1 + K_2$$

$$= 10^5 \begin{bmatrix} 1.6 & -1.6 & 0 \\ -1.6 & 2.3 & -0.7 \\ 0 & -0.7 & 0.7 \end{bmatrix}$$

Using Penalty method

$$C = |\max K_{ij}| \times 10^4$$

$$= 2.3 \times 10^5 \times 10^4$$

$$C = 2.3 \times 10^9$$

'C' should be added to first & last element of the diagonal

$$K = 10^5 \begin{bmatrix} 1.6 & -1.6 & 0 \\ +C & & \\ -1.6 & 2.3 & -0.7 \\ 0 & -0.7 & 0.7 \\ & & +C \end{bmatrix}$$

$$K = \begin{bmatrix} 2.30016 \times 10^9 & -1.6 \times 10^5 & 0 \\ -1.6 \times 10^5 & 2.3 \times 10^5 & -0.7 \times 10^5 \\ 0 & -0.7 \times 10^5 & 2.30007 \times 10^5 \end{bmatrix}$$

Equilibrium eqn.

$$[K][q] = [F]$$

$$\begin{bmatrix} 2.30016 \times 10^9 & -1.6 \times 10^5 & 0 \\ -1.6 \times 10^5 & 2.3 \times 10^5 & -0.7 \times 10^5 \\ 0 & -0.7 \times 10^5 & 2.30007 \times 10^5 \end{bmatrix} \begin{bmatrix} q_1 \\ q_2 \\ q_3 \end{bmatrix} = \begin{bmatrix} 0 \\ -200 \times 10^3 \\ 0 \end{bmatrix}$$

Solving
Equilibrium eqn.

$$q_1 = -6.0491 \times 10^{-5} \text{ mm}$$

$$q_2 = -0.8696 \text{ mm}$$

$$q_3 = -2.6466 \times 10^{-5} \text{ mm}$$

Stresses in each element

For element 1

$$\sigma_1 = EBQ$$

$$= E \frac{b}{l_1} [-1 \ 1] \begin{bmatrix} q_1 \\ q_2 \end{bmatrix}$$

$$= \frac{200 \times 10^3}{500} [-1 \ 1] \begin{bmatrix} -6.0491 \times 10^{-5} \\ -0.8696 \end{bmatrix}$$

$$\sigma_1 = -347.82 \text{ N/mm}^2$$

For element 2

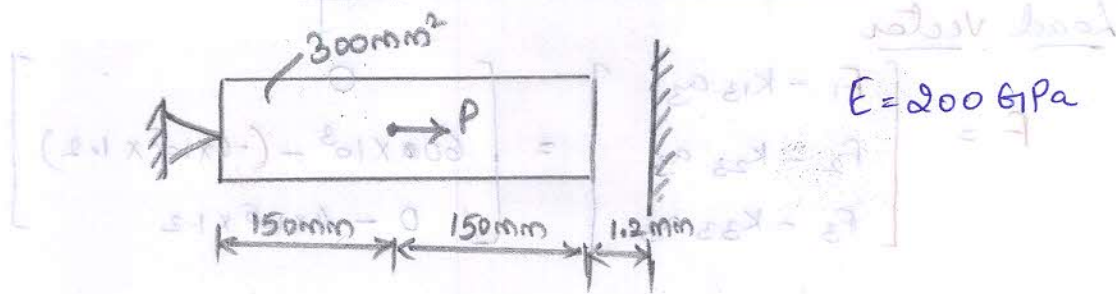
$$\sigma_2 = EBQ$$

$$= E \frac{b}{l_2} [-1 \ 1] \begin{bmatrix} q_3 \\ q_4 \end{bmatrix}$$

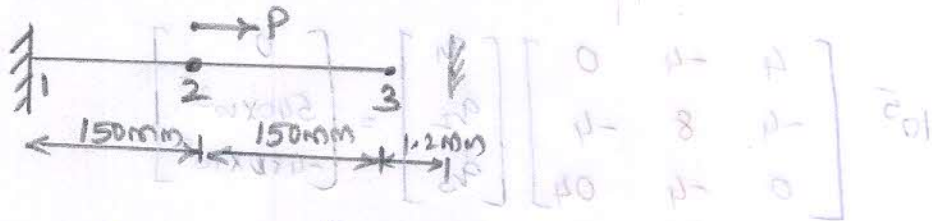
$$= 70 \times 10^3 \times \frac{1}{300} [-1 \ 1] \begin{bmatrix} -0.8696 \\ -2.6466 \times 10^{-5} \end{bmatrix}$$

$$\sigma_2 = 202.88 \text{ N/mm}^2$$

6



F.E. Model

Elemental stiffness matrix

$$K = \frac{EA}{L_e} \begin{bmatrix} 1 & -1 \\ -1 & 1 \end{bmatrix}$$

For element 1

$$K_1 = \frac{200 \times 10^3 \times 300}{150} \begin{bmatrix} 1 & -1 \\ -1 & 1 \end{bmatrix}$$

$$K_1 = 10^5 \begin{bmatrix} 4 & -4 \\ -4 & 4 \end{bmatrix}$$

For element 2

$$K_2 = \frac{200 \times 10^3 \times 300}{150} \begin{bmatrix} 1 & -1 \\ -1 & 1 \end{bmatrix}$$

$$K_2 = 10^5 \begin{bmatrix} 4 & -4 \\ -4 & 4 \end{bmatrix}$$

Global stiffness matrix

$$K = 10^5 \begin{bmatrix} 4 & -4 & 0 \\ -4 & 8 & -4 \\ 0 & -4 & 4 \end{bmatrix}$$

Load Vector

$$F = \begin{bmatrix} F_1 - K_{13} a_3 \\ F_2 - K_{23} a_3 \\ F_3 - K_{33} a_3 \end{bmatrix} = \begin{bmatrix} 0 \\ 600 \times 10^3 - (-4 \times 10^5 \times 1.2) \\ 0 - 4 \times 10^5 \times 1.2 \end{bmatrix} = \begin{bmatrix} 0 \\ 540 \times 10^3 \\ -480 \times 10^3 \end{bmatrix}$$

Equilibrium eqn. $[K][q] = [F]$

$$10^5 \begin{bmatrix} 4 & -4 & 0 \\ -4 & 8 & -4 \\ 0 & -4 & 4 \end{bmatrix} \begin{bmatrix} q_1 \\ q_2 \\ q_3 \end{bmatrix} = \begin{bmatrix} 0 \\ 540 \times 10^3 \\ -480 \times 10^3 \end{bmatrix}$$

Applying B.C : Using Elimination Method

$$10^5 \begin{bmatrix} 4 & -4 & 0 \\ -4 & 8 & -4 \\ 0 & -4 & 4 \end{bmatrix} \begin{bmatrix} q_1 \\ q_2 \\ q_3 \end{bmatrix} = \begin{bmatrix} 0 \\ 540 \times 10^3 \\ -480 \times 10^3 \end{bmatrix}$$

$$q_1 = 0; \quad q_2 = 0.675 \text{ mm}; \quad q_3 = 1.2 \text{ mm.}$$

Displacement at node 1 : $q_1 = 0$

$$\text{Node 2 : } q_2 = 0.675 \text{ mm}$$

$$\text{Node 3 : } q_3 = 1.2 \text{ mm} //$$

Stress in each element

$$\sigma = E \cdot B \cdot q = E \cdot \frac{1}{L_e} \begin{bmatrix} -1 & 1 \end{bmatrix} \begin{bmatrix} q_1 \\ q_2 \end{bmatrix}$$

Element 1

$$\sigma_1 = 200 \times 10^3 \times \frac{1}{150} \begin{bmatrix} -1 & 1 \end{bmatrix} \begin{bmatrix} 0 \\ 0.675 \end{bmatrix}$$

$$\sigma_1 = 900 \text{ N/mm}^2 //$$

Element 2

$$\sigma_2 = 200 \times 10^3 \times \frac{1}{150} \begin{bmatrix} -1 & 1 \end{bmatrix} \begin{bmatrix} 0.675 \\ 1.2 \end{bmatrix}$$

$$\sigma_2 = 700 \text{ N/mm}^2 //$$