

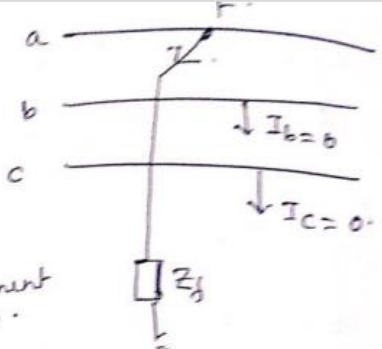
Sub:	Power System Analysis-1	Code:	18EE62
Date:	08/07/2022	Duration:	90 mins
		Max Marks:	50
		Sem:	6 th
		Branch:	EEE

Answer Any FIVE FULL Questions. Assume missing Data

	Marks	OBE	
		CO	RBT

1. Find out the expression of fault current when power system, is subjected to a) LG fault through a fault impedance with necessary diagrams.

LG Fault



Terminal Conditions

$V_a = I_a Z_f$
 $I_b = 0$
 $I_c = 0$

Symmetrical Component Relations

$$I_{a0} = \frac{1}{3} (I_a + I_b + I_c) = \frac{1}{3} I_a$$

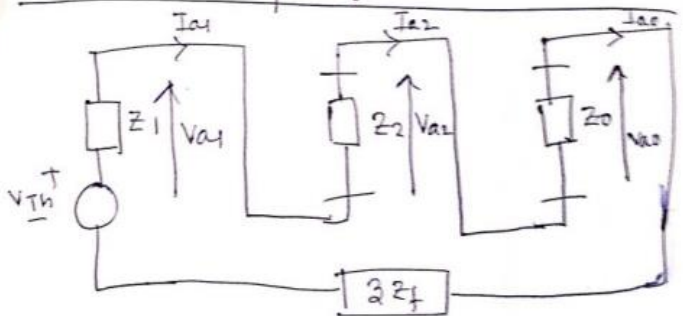
$$I_{a1} = \frac{1}{3} (I_a + \alpha I_b + \alpha^2 I_c) = \frac{1}{3} I_a$$

$$I_{a2} = \frac{1}{3} (I_a + \alpha^2 I_b + \alpha I_c) = \frac{1}{3} I_a$$

$$I_{a1} = I_{a2} = I_{a0} = \frac{1}{3} I_a$$

as $V_a = I_a Z_f$
 $V_{a0} + V_{a1} + V_{a2} = I_a Z_f = 3 I_{a0} Z_f$

Interconnection of sequence networks



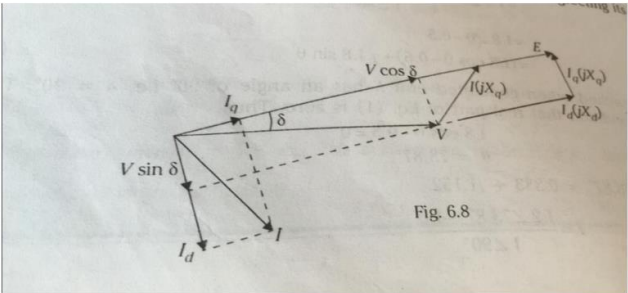
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Fault Current

$$I_f = I_a = 3 I_{a0} = \frac{3 V_{Th}}{Z_1 + Z_2 + Z_0 + 3 Z_f}$$

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2.	<p>Derive Power angle equation of synchronous machine for salient with necessary graph.</p>  <p style="text-align: center;">Fig. 6.8</p>	10	CO5	L3
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$E/\delta \Rightarrow$ Generated emf in the syn m/c.
 $V/\delta =$ Bus bar voltage (taken as ref).
 $X_d =$ direct axis syn reactance.
 $X_q =$ quadrature axis syn reactance.
 $I =$ current delivered at lagging pf ϕ .

$$P = |V| \cos \delta \left[\frac{|I_q|}{1} + |V| \sin \delta \right] |I_d|.$$

$$|I_q X_q| = |V \sin \delta|.$$

$$|I_q| = \frac{|V \sin \delta|}{X_q}.$$

$$|I_d X_d| = |E - V \cos \delta|.$$

$$|I_d| = \frac{|E| - |V \cos \delta|}{X_d}.$$

$$P = |V| \cos \delta \left(\frac{|V \sin \delta|}{X_q} + |V \sin \delta| + \frac{|E| - |V \cos \delta|}{X_d} \right).$$

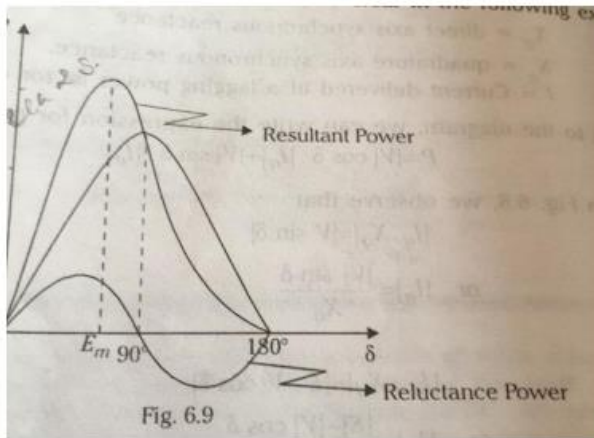
$$= \frac{|V|^2 \sin^2 \delta}{2X_q} + \frac{|V| |E| \sin \delta}{X_d} - \frac{V^2 \sin^2 \delta}{2X_d}.$$

$$= \frac{|V|^2 \sin^2 \delta}{2} \left(\frac{1}{X_q} - \frac{1}{X_d} \right) + \frac{|V| |E| \sin \delta}{X_d}.$$

$$P = \frac{|V| |E| \sin \delta}{X_d} + \frac{|V|^2 \sin^2 \delta}{2} \left(\frac{X_d - X_q}{X_d X_q} \right).$$

Reluctance Power.

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3. Define a) steady state stability, b) transient stability, c) steady state stability limit, d) transient stability limit.

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L1

Stability Limits:

Steady state stability limit (SSSL), refers to the maximum flow of power possible through a particular point in the system without the loss of stability when a small a gradual disturbance occurs in the system.

Transient stability limit (TSL) refers to to the maximum flow of power possible through a particular point in the system without the loss of stability when a large and sudden disturbance occurs in the system. TSL is lower than SSSL.

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4. Derive equal area criteria, and find its application with respect to following: sudden change in input.

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L2

Stability analysis can be carried out by
Equal Area Criterion (EAC).

⇒ It provides qualitative analysis of stability of syn m/c. without

...ing swing equation

Consider swing equation of a single machine connected to an infinite bus

$$M \frac{d^2\delta}{dt^2} = P_a$$

Multiplying both sides of the equation by

$$\frac{2}{M} \frac{d\delta}{dt}, \text{ we get}$$

$$2 \frac{d\delta}{dt} \times \frac{d^2\delta}{dt^2} = \frac{2}{M} P_a \frac{d\delta}{dt}$$

$$\frac{d}{dt}(\dot{\delta}^2) = 2 \frac{P_a}{M} \frac{d\delta}{dt}$$

$$\text{or } \frac{d}{dt} \left(\frac{d\delta}{dt} \right)^2 = \frac{2}{M} P_a \frac{d\delta}{dt}$$

$$\left(\frac{d\delta}{dt} \right)^2 = \frac{2}{M} \int_{\delta_0}^{\delta} P_a \frac{d\delta}{dt} \cdot dt$$

$$= \frac{2}{M} \int_{\delta_0}^{\delta} P_a d\delta$$

$$\frac{d\delta}{dt} = \sqrt{\frac{2}{M} \int_{\delta_0}^{\delta} P_a d\delta}$$

$$\frac{d\delta}{dt} = 0 \quad \text{i.e.} \quad \sqrt{\frac{2}{M} \int_{\delta_0}^{\delta} P_a d\delta} = 0$$

$$\int_{\delta_0}^{\delta} P_a d\delta = 0$$

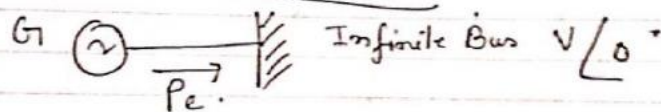
Applications of Equal Area Criterion

Illustration of EAC of stability for several types of disturbances in SMIB.

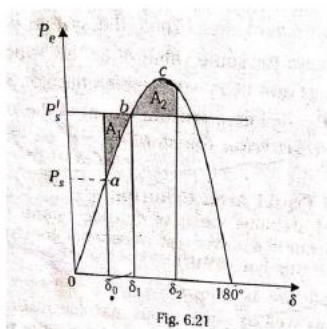
Assumption:

- 1) T.L and syn m/c resistance are neglected.
- 2) Rotor speed of syn m/c is constant.
- 3) Mech I/P to m/c constant.
- 4) Voltage behind transient reactance const.
- 5) Effect of damper winding neglected.

a) Sudden Change in I/P



Let us consider sudden increase in mechanical:



Curve $P_e - \delta$ shows the power angle curve.
with the system operating at point a
corresponding to I/P P_s .

Let mechanical I/P be P_s .

\therefore Accelerating Power $P_a = P_s - P_e$, causes
rotor to accelerate.

$\delta \uparrow \Rightarrow$ electric power transfer \uparrow ,

$P_a \downarrow$ till a point b at which $P_a = 0$.

But rotor angle δ continues to \uparrow because
of inertia of rotor, and P_a becomes (-ve)
causing to rotor decelerate.

At point c where area $A_1 = \text{area } A_2$

$$\text{on } \int_{\delta_0}^{\delta_2} P_a d\delta = 0 \Rightarrow \frac{d\delta}{dt} = 0 \text{ (rotor vel.)}$$

and then starts to become negative owing
to continued negative P_a

Rotor angle reaches the max value δ_2 and

then starts to decrease.

$$A_1 = \int_{\delta_0}^{\delta_1} (P_{s'} - P_e) d\delta$$

$$A_2 = \int_{\delta_1}^{\delta_2} (P_e - P_{s'}) d\delta$$

Find $(\delta_2)_{max}$ such that $A_1 = A_2$.

As $P_{s'}$ increases a limiting condition is finally reached when area A_1 equals the entire area A_2 above the line $P_{s'}$ (as in fig 2).

Under this condition δ_2 acquires the max. value δ_{cr} .

$$\delta_2 = \delta_{cr} = 180^\circ - \delta_1$$

\Rightarrow system is critically stable.

if $P_{s'}$ increases further $A_2 < A_1$
 \Rightarrow system is unstable

5a Discuss about how to improve transient stability.

5

CO5

L2

The generator terminals. Load compensates for at least some of the reduction of load on generators and so reduces the acc. of the machine.

(c) Fast re-energizing or bypass valving! \rightarrow The stability of a unit is improved by decreasing the mechanical I/P power to the turbine. When a fault occurs control scheme detects the diff betn mech I/P and reduces electrical o/p of the generator initiates the closing of a turbine valve to reduce the power I/P.

(d) Full load rejection technique!

(e) Using superconducting fault current limiters (SFCL).

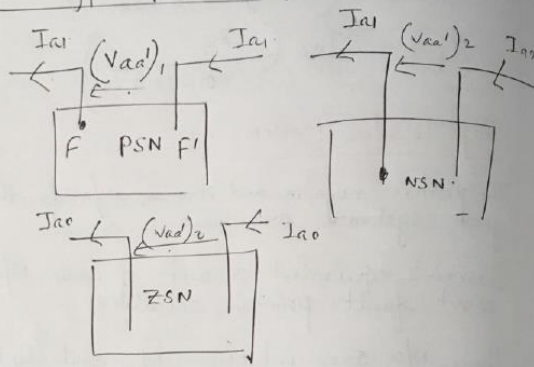
5b Write short notes on series type of fault.

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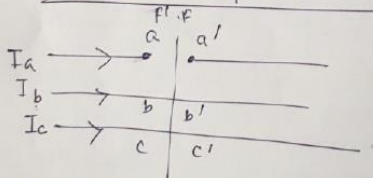
CO4

L2

Series types of Faults



One Conductor open fault



Terminal Condition

$$I_a = 0$$

$$V_{bb'} = 0$$

$$V_{cc'} = 0$$

Symmetrical Component Relation.

$$(V_{aa'})_1 = \frac{1}{3} (V_{aa} + \alpha V_{bb'} + \alpha^2 V_{cc'})$$

$$= \frac{1}{3} (V_{aa} + 0 + 0) = \frac{1}{3} V_{aa'}$$

(-ve) seq. voltage is.

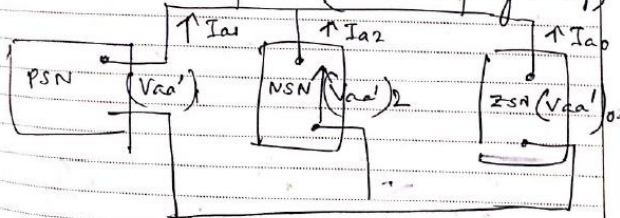
$$(V_{aa'})_2 = \frac{1}{3} (V_{aa} + \alpha^2 V_{bb'} + \alpha V_{cc'})$$

$$= \frac{1}{3} V_{aa'}$$

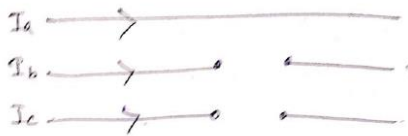
$$(V_{aa'})_0 = \frac{1}{3} (V_{aa} + V_{bb'} + V_{cc'}) = 0 \cdot \frac{1}{3} V_{aa'}$$

$\therefore I_{a0} = 0 \quad I_{a0} + I_{a1} + I_{a2} = 0$

Similar to LLG fault (Interms of sym comp)



Two conductors open fault



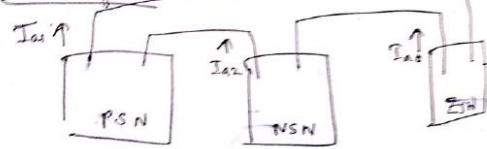
Terminal Condition: $I_b = 0$
 $I_c = 0$
 $V_{aa'} = 0$

Symmetrical Component Relation

$$I_{a0} = \frac{1}{3} (I_a + I_b + I_c) = \frac{1}{3} I_a$$

Wdy $I_{a1} = \frac{1}{3} I_a$, $I_{a2} = \frac{1}{3} I_a$
 as $V_{aa'} = 0 \therefore (V_{aa'})_0 + (V_{aa'})_1 + (V_{aa'})_2 = 0$

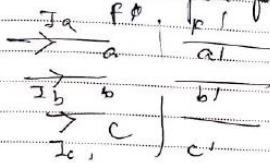
Like LG fault



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Three conductors open fault



Terminal Condition: $I_a + I_b + I_c = 0$
 $I_{a0} = I_{a1} + I_{a2} = 0$

Open circuit

6 A synchronous motor is receiving 10MW of power at 0.8pf lag at 6kV. An LG fault takes place at the middle point of the transmission line as shown in figure. Find the fault current. The ratings of the generator, motor and the transformer areas under:

Generator: 20 MVA, 11kV, $X_1=0.2$ pu, $X_2=0.1$ pu, $X_0=0.1$ pu

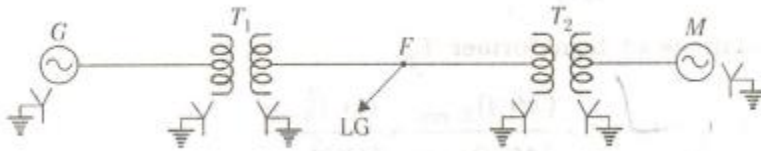
Transformer T1: 18MVA, 11.5Y-34.5YkV, $X=0.1$ pu

Transmission Line: $X_1=X_2=5\Omega$, $X_0=10\Omega$

Transformer T2: 15MVA, 6.9Y-34.5 Y kV, $X=0.1$ pu

Motor: 15MVA, 6.9kV, $X_1=0.2$ pu, $X_2=X_0=0.1$ pu

10 CO4 L4



Part 11.pdf

Solution

Base Values Let the base power for entire system be

$$(MVA)_{B, new} = 20 MVA$$

Base voltage of gen = 11 kV

$$n \text{ of T.L.} = 11 \times \frac{34.5}{11.5} = 33 kV$$

$$n \text{ of motor} = 33 \times \frac{6.9}{34.5} = 6.6 kV$$

Sequence reactances of generator

$$X_1 = 0.2 \times \frac{20}{20} \times \frac{11^2}{11^2} = 0.2 p.u.$$

$$X_2 = 0.1 \times \frac{20}{20} \times \frac{11^2}{11^2} = 0.1 p.u.$$

$$X_0 = 0.1 \times \frac{20}{20} \times \frac{11^2}{11^2} = 0.1 p.u.$$

Sequence reactance of "

$$X_1 = X_2 = X_0 = X \times \frac{(MVA)_{B, new}}{(MVA)_{B, old}} \times \frac{(kV)_{B, old}^2}{(kV)_{B, new}^2}$$

$$= 0.1 \times \frac{20}{18} \times \frac{11.5^2}{11^2} = 0.12 p.u.$$

Sequence reactance of T.L

$$X_1 = X_2 = X(\Omega) \times \frac{(MVA)_{B, new}}{(kV)_B^2}$$

$$= 5 + 5 \times \frac{20}{33^2} = 0.092 p.u.$$

$$X_0 = 10 \times \frac{20}{33^2} = 0.184 p.u.$$

Sequence reactance of T2

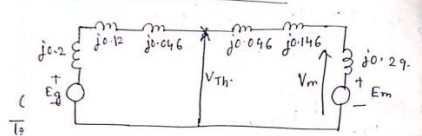
$$X_1 = X_2 = X_0 = X \times \frac{20}{15} \times \frac{6.9^2}{6.6^2} = 0.146 p.u.$$

Sequence reactances of Motor

$$X_1 = 0.2 \times \left(\frac{20}{15}\right) \times \left(\frac{6.9^2}{6.6^2}\right) = 0.29 p.u.$$

$$X_2 = X_0 = 0.1 \times \frac{20}{15} \times \frac{(6.9)^2}{(6.6)^2} = 0.145 p.u.$$

Positive Sequence Network



To find the voltage at the fault point (V_{Th})

The current drawn by the motor.

$$I_m = \frac{10 \times 10^6}{\sqrt{3} \times 6 \times 10^3 \times 0.8} \angle \cos^{-1} 0.8$$

$$= 12028 \angle -36.87^\circ \text{ A}$$

Base current in the motor (I_m) $I_m \text{ pu} = \frac{20 \times 10^6}{\sqrt{3} \times 6 \times 10^3}$

$$I_m \text{ pu} = \frac{12028}{1749.55} \angle -36.87^\circ = 0.687 \angle -36.87^\circ \text{ pu}$$

$$V_{Th} \text{ in pu} = \frac{6}{6.6} = 0.909 \angle 0^\circ \text{ pu}$$

\therefore Voltage at the fault point

$$V_{Th} = V_m + I_m (j0.046 + j0.146)$$

$$= 0.909 \angle 0^\circ + 0.687 \angle -36.87^\circ \times 0.192 \angle 90^\circ$$

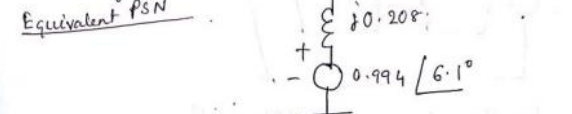
$$= 0.994 \angle 6.1^\circ \text{ pu}$$

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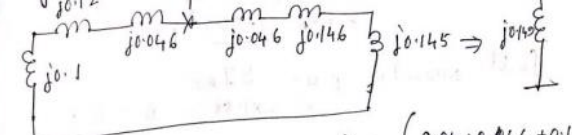
To find Thevenin's Impedance Z_{Th} at point F

$$Z_{1Th} = j \left[(0.2 + 0.12 + 0.046) \parallel \left(\frac{j0.046 + j0.146}{0.29} \right) \right]$$

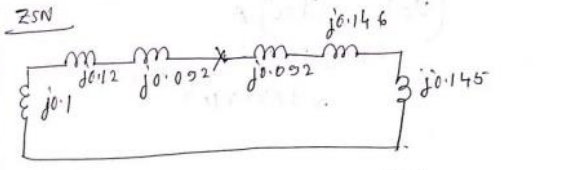
$$= j0.208 \text{ p.u.}$$



Negative Sequence Network (N_2N).

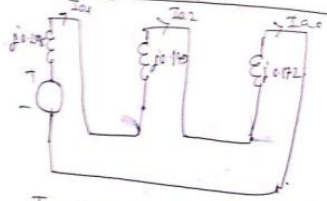


$$Z_{2Th} = \left[j(0.1 + 0.12 + 0.046) \parallel (0.04 + 0.046 + 0.145) \right]$$



$$Z_{0Th} = j0.172$$

Interconnection of sequence networks



$$I_{a1} = I_{a2} = I_{a0} = \frac{0.994 \angle 6.1^\circ}{j(0.208 + j0.140 + j0.172)}$$

$$= 1.88 \angle -83.9^\circ \text{ p.u.}$$

fault current p.u. = $3 I_{a0}$
 $= 3 \times 1.88 = 5.64 \text{ p.u.}$

fault current in Ampere.

$$\left(\frac{I_f}{I_{TL}} \right)_{\text{p.u.}} \times (I_{TL})_{\text{A}}$$

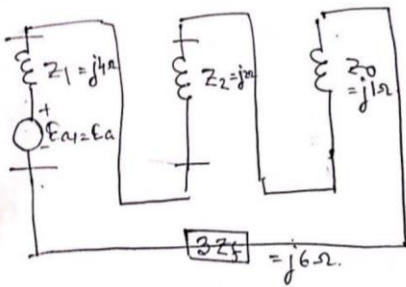
$$= \frac{5.64 \times 20 \times 10^3}{\sqrt{3} \times 33 \times 10^3} = 1973.49 \text{ A.}$$

7. A three phase generator with an open circuit voltage of 400V is subjected to an LG fault through a fault impedance of $j2\Omega$. Determine the fault current if $Z_1=j4\Omega$, $Z_2=j2\Omega$, $Z_0=j1\Omega$

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L3



$$I_{a1} = I_{a2} = I_{a0}$$

$$= \frac{E_a}{Z_1 + Z_2 + Z_0 + 3Z_f}$$

$$= \frac{400/\sqrt{3} \angle 0^\circ}{j(4 + 2 + 1 + 6)}$$

$$= \frac{400/\sqrt{3} \angle 0^\circ}{j17.765}$$

$$I_f = 3 |I_{a0}|$$

$$= 530.295 \text{ A}$$