

Internal Assessment Test III – July 2022

Sub: Finite Element Methods

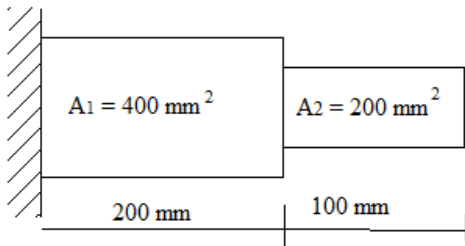
	Max				
Date: 08/07/2022	Duration: 90 mins	Marks: 50	Sem: VI		

Note: Answer all questions.

Code:	18ME61
Branch:	MECH

Marks OBE
CO RBT

- 1 Evaluate Eigen values & Eigen vector for stepped bar shown in figure 1. Take $E = 200$ GPa, Density = 7850 kg/m^3 . Draw mode shapes

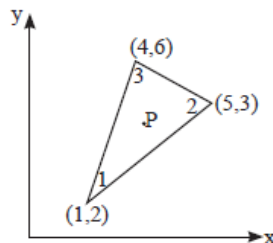


20 CO4 L3

- 2 Explain the various boundary conditions in steady state heat transfer problems with simple sketches.

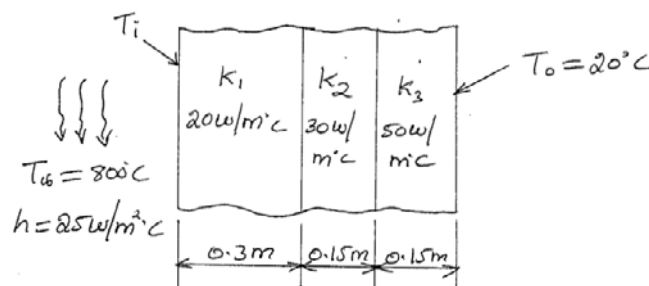
6 CO5 L2

- 3 The nodal co-ordinates of a triangular element are shown in fig. The x - coordinates of an interior point P is 3.3 and shape function. $N_1 = 0.3$. Determine N_2 , N_3 and y - coordinate point P.



10 CO4 L2

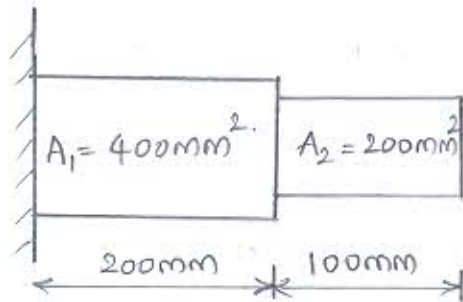
- 4 A composite wall is as shown in figure consists of three materials. The outer temperature T_0 is 20°C . Convective heat transfer takes place on inner surface of the wall with $T_\infty = 800^\circ\text{C}$. The convective heat transfer coefficient is $25 \text{ W/m}^2\text{C}$. Determine the temperature distribution in the wall.



14 CO5 L3

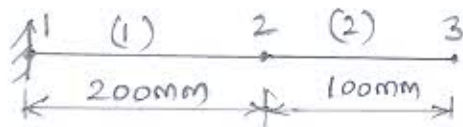
(P) Evaluate eigen vectors & eigen values for the stepped bar shown. Take $E = 200 \text{ GPa}$; density = 7850 kg/m^3 ,

Draw mode shapes.



Sol

F.E. Model



Elemental Stiffness matrix

$$k = \frac{EA}{l_e} \begin{bmatrix} 1 & -1 \\ -1 & 1 \end{bmatrix}$$

$$k_1 = \frac{200 \times 10^3 \times 400}{200} \begin{bmatrix} 1 & -1 \\ -1 & 1 \end{bmatrix} = 10^5 \begin{bmatrix} 4 & -4 \\ -4 & 4 \end{bmatrix} \begin{matrix} 1 & 2 \\ & 2 \end{matrix}$$

$$k_2 = \frac{200 \times 10^3 \times 200}{100} \begin{bmatrix} 1 & -1 \\ -1 & 1 \end{bmatrix} = 10^5 \begin{bmatrix} 4 & -4 \\ -4 & 4 \end{bmatrix} \begin{matrix} 2 & 3 \\ & 3 \end{matrix}$$

Global Stiffness matrix

$$k = 10^5 \begin{bmatrix} 4 & -4 & 0 \\ -4 & 8 & -4 \\ 0 & -4 & 4 \end{bmatrix} \begin{matrix} 1 \\ 2 \\ 3 \end{matrix}$$

Elemental mass matrix

$$m^e = \frac{SAle}{6} \begin{bmatrix} 2 & 1 \\ 1 & 2 \end{bmatrix}$$

$$m^{e_1} = \frac{7850 \times 10^{-9} \times 400 \times 200}{6} \begin{bmatrix} 2 & 1 \\ 1 & 2 \end{bmatrix} = \begin{bmatrix} 0.2093 & 0.1047 \\ 0.1047 & 0.2093 \end{bmatrix} \begin{matrix} 1 & 2 \\ 2 & 1 \end{matrix}$$

$$m^{e_2} = \frac{7850 \times 10^{-9} \times 200 \times 100}{6} \begin{bmatrix} 2 & 1 \\ 1 & 2 \end{bmatrix} = \begin{bmatrix} 0.0523 & 0.0261 \\ 0.0261 & 0.0523 \end{bmatrix} \begin{matrix} 2 & 3 \\ 3 & 2 \end{matrix}$$

Global mass matrix

$$m^e = \begin{bmatrix} 0.2093 & 0.1047 & 0 \\ 0.1047 & 0.157 & 0.0261 \\ 0 & 0.0261 & 0.0523 \end{bmatrix} \begin{matrix} 1 & 2 & 3 \\ 2 & 1 & 3 \\ 3 & 2 & 1 \end{matrix}$$

$$Ku - \lambda Mu = 0$$

$$\left| 10^5 \begin{bmatrix} 4 & -4 & 0 \\ -4 & 8 & -4 \\ 0 & -4 & 4 \end{bmatrix} - \lambda \begin{bmatrix} 0.2093 & 0.1047 & 0 \\ 0.1047 & 0.157 & 0.0261 \\ 0 & 0.0261 & 0.0523 \end{bmatrix} \right| = 0$$

$$\left| 10^5 \begin{bmatrix} 8 & -4 \\ -4 & 4 \end{bmatrix} - \lambda \begin{bmatrix} 0.157 & 0.0261 \\ 0.0261 & 0.0523 \end{bmatrix} \right| = 0$$

$$\left| \begin{bmatrix} 8 \times 10^5 & -4 \times 10^5 \\ -4 \times 10^5 & 4 \times 10^5 \end{bmatrix} - \begin{bmatrix} 0.157 \lambda & 0.0261 \lambda \\ 0.0261 \lambda & 0.0523 \lambda \end{bmatrix} \right| = 0$$

$$\begin{vmatrix} 8 \times 10^5 - 0.157 \lambda & -(4 \times 10^5 + 0.0261 \lambda) \\ -(4 \times 10^5 + 0.0261 \lambda) & 4 \times 10^5 - 0.0523 \lambda \end{vmatrix} = 0$$

$$\Rightarrow (8 \times 10^5 - 0.157 \lambda)(4 \times 10^5 - 0.0523 \lambda) - (4 \times 10^5 + 0.0261 \lambda)^2 = 0$$

$$\Rightarrow (3.2 \times 10^{11} - 41840 \lambda - 62800 \lambda + 8.211 \times 10^{-3} \lambda^2)$$

$$- (1.6 \times 10^{11} + 6.8121 \times 10^{-4} \lambda^2 + 20850 \lambda) = 0$$

$$\Rightarrow 1.6 \times 10^{11} - 125520 \lambda + 7.53 \times 10^{-3} \lambda^2 = 0$$

$$\lambda_1 = 1.39 \times 10^6$$

$$\lambda_2 = 15.3 \times 10^6$$

$$\lambda_1 = \omega_1^2 = 1.39 \times 10^6$$

$$\omega_2^2 = 15.3 \times 10^6$$

$$\omega_1 = 1178.98 \text{ rad/s}$$

$$\omega_2 = 3911.52 \text{ rad/s}$$

For Mode Shapes

1st mode shape

$$[K - \lambda M] x = 0$$

$$\left\{ 10^5 \begin{bmatrix} 8 & -4 \\ -4 & 4 \end{bmatrix} - \lambda_1 \begin{bmatrix} 0.157 & 0.0261 \\ 0.0261 & 0.0523 \end{bmatrix} \right\} \begin{bmatrix} x_2^{(1)} \\ x_3^{(1)} \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \end{bmatrix}$$

$$\left\{ 10^5 \begin{bmatrix} 8 & -4 \\ -4 & 4 \end{bmatrix} - 1.39 \times 10^6 \begin{bmatrix} 0.157 & 0.0261 \\ 0.0261 & 0.0523 \end{bmatrix} \right\} \begin{bmatrix} x_2^{(1)} \\ x_3^{(1)} \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \end{bmatrix}$$

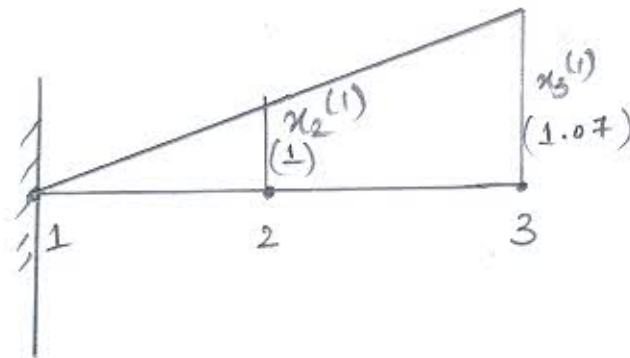
$$\left\{ 10^5 \begin{bmatrix} 8 & -4 \\ -4 & 4 \end{bmatrix} - \begin{bmatrix} 2.18 \times 10^5 & 0.036 \times 10^5 \\ 0.36 \times 10^5 & 0.727 \times 10^5 \end{bmatrix} \right\} \begin{bmatrix} x_2^{(1)} \\ x_3^{(1)} \end{bmatrix} = 0$$

$$8 \times 10^5 x_2^{(1)} - 2.18 \times 10^5 x_2^{(1)} - 4 \times 10^5 x_3^{(1)} - 0.36 \times 10^5 x_3^{(1)} = 0$$

$$(5.82 \times 10^5) x_2^{(1)} - 4.86 \times 10^5 x_3^{(1)} = 0$$

$$x_3^{(1)} = 1.07 x_2^{(1)}$$

$$x^{(1)} = \begin{bmatrix} x_2^{(1)} \\ x_3^{(1)} \end{bmatrix} = \begin{bmatrix} x_2^{(1)} \\ 1.07 x_2^{(1)} \end{bmatrix} = x_2^{(1)} \begin{bmatrix} 1 \\ 1.07 \end{bmatrix} //$$



Second mode shape

$$[K - \lambda_2 M] = 0$$

$$\left\{ 10^5 \begin{bmatrix} 8 & -4 \\ -4 & 4 \end{bmatrix} - \lambda_2 \begin{bmatrix} 0.157 & 0.0261 \\ 0.0261 & 0.0523 \end{bmatrix} \right\} \begin{bmatrix} x_2^{(2)} \\ x_3^{(2)} \end{bmatrix} = 0$$

$$\left\{ 10^5 \begin{bmatrix} 8 & -4 \\ -4 & 4 \end{bmatrix} - 15.3 \times 10^6 \begin{bmatrix} 0.157 & 0.0261 \\ 0.0261 & 0.0523 \end{bmatrix} \right\} \begin{bmatrix} x_2^{(2)} \\ x_3^{(2)} \end{bmatrix} = 0$$

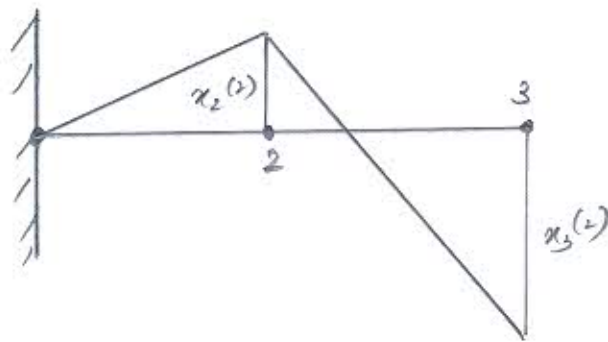
$$\left\{ 10^5 \begin{bmatrix} 8 & -4 \\ -4 & 4 \end{bmatrix} - \begin{bmatrix} 2.4 \times 10^6 & 0.399 \times 10^6 \\ 0.399 \times 10^6 & 0.8 \times 10^6 \end{bmatrix} \right\} \begin{bmatrix} x_2^{(2)} \\ x_3^{(2)} \end{bmatrix} = 0$$

$$(8 \times 10^5 - 2.4 \times 10^6) x_2^{(2)} - (-4 \times 10^5 - 0.399 \times 10^6) x_3^{(2)} = 0$$

$$-1.6 \times 10^6 x_2^{(2)} - 0.799 \times 10^6 x_3^{(2)} = 0$$

$$x_3^{(2)} = -2.00 x_2^{(2)}$$

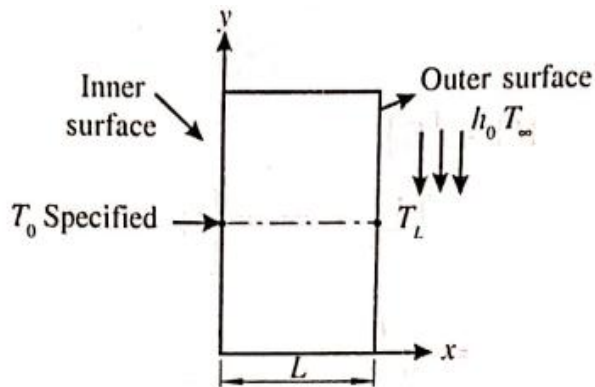
$$x_2^{(2)} = \begin{bmatrix} x_2^{(2)} \\ x_3^{(2)} \end{bmatrix} = \begin{bmatrix} x_2^{(2)} \\ -2 x_2^{(2)} \end{bmatrix} = x_2^{(2)} \begin{bmatrix} 1 \\ -2.00 \end{bmatrix}$$



BOUNDARY CONDITIONS

- Specified Temperature Boundary Condition
- Specified Heat Flux Boundary Condition
- Convection Boundary Condition

Specified Temperature Boundary Condition

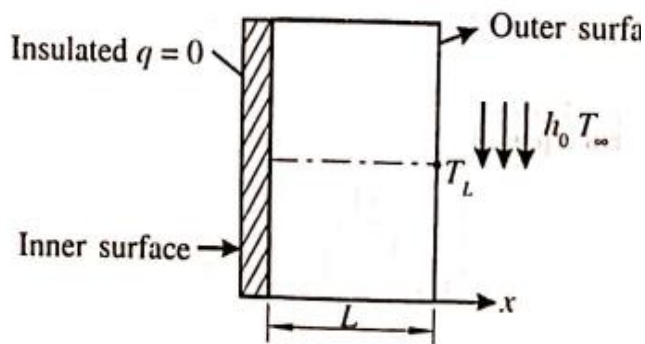


The boundary condition for this problem are

At $x = 0$, $T = T_0$ (Specified temperature)

At $x = L$, $q = h_0 (T_L - T_\infty)$

Specified Heat Flux Boundary Condition

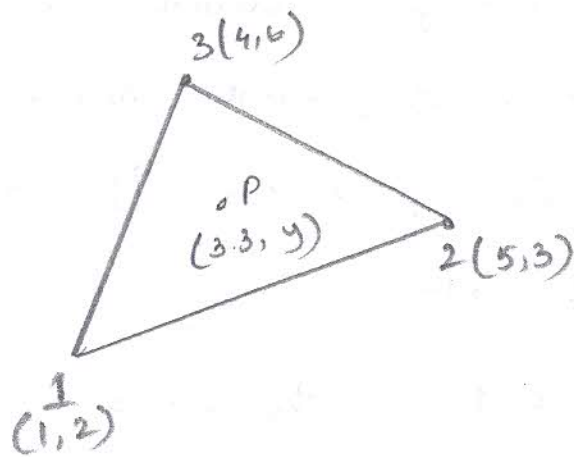


The boundary condition for this problem are

At $x = 0$, $q = q_0 = 0$

At $x = L$, $q = h_0 (T_L - T_\infty)$

Where, q_0 is the specified heat flux on the boundary.



$$x = N_1 x_1 + N_2 x_2 + N_3 x_3$$

$$3.3 = 0.3(1) + \eta(5) + (1 - \xi - \eta)4$$

$$3.3 = 0.3 + 5\eta + 4 - 4\xi - 4\eta$$

$$-4\xi + \eta = -1$$

$$-4(0.3) + \eta = -1$$

$$\eta = 0.2$$

$$\therefore N_2 = \eta = 0.2 //$$

$$N_3 = 1 - \xi - \eta = 1 - 0.3 - 0.2 = 0.5$$

$$N_3 = 0.5 //$$

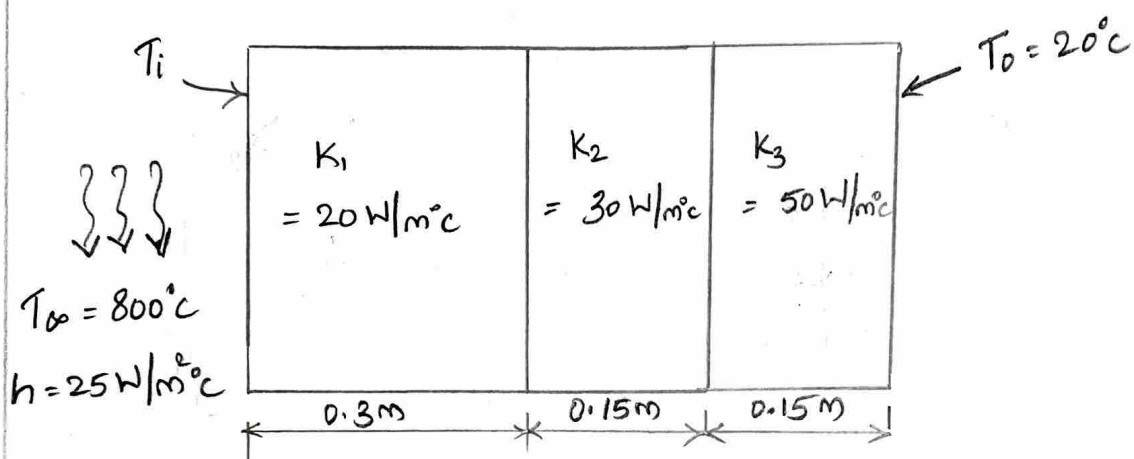
y coordinate

$$y = N_1 y_1 + N_2 y_2 + N_3 y_3$$

$$= 0.3(2) + 0.2(3) + 0.5(6)$$

$$y = 4.2 //$$

A Composite wall is as shown in figure Consists of three materials. The outer temperature T_o is 20°C . Convective heat transfer takes place on inner surface of the wall with $T_\infty = 800^\circ\text{C}$. The Convective heat transfer coefficient is $25\text{ W/m}^2\text{C}$. Determine the temperature distribution in the wall.

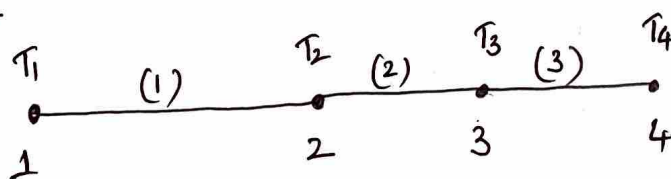


Sol

$$k_1 = 20\text{ W/m}^\circ\text{C} ; k_2 = 30\text{ W/m}^\circ\text{C} ; k_3 = 50\text{ W/m}^\circ\text{C}$$

$$h = 25\text{ W/m}^2\text{C} ; T_\infty = 800^\circ\text{C}$$

F.E. Model



Element stiffness matrix

$$[K] = \frac{AK}{L} \begin{bmatrix} 1 & -1 \\ -1 & 1 \end{bmatrix}$$

For element 1

$$[K_1] = \frac{1 \times 20}{0.3} \begin{bmatrix} 1 & -1 \\ -1 & 1 \end{bmatrix} = \begin{bmatrix} 66.67 & -66.67 \\ -66.67 & 66.67 \end{bmatrix}$$

For element 2

$$K_2 = \frac{1(30)}{0.15} \begin{bmatrix} 1 & -1 \\ -1 & 1 \end{bmatrix} = \begin{bmatrix} 200 & -200 \\ -200 & 200 \end{bmatrix} \begin{matrix} 2 & 3 \\ 3 & 2 \end{matrix}$$

For element 3

$$K_3 = \frac{1(50)}{0.15} \begin{bmatrix} 1 & -1 \\ -1 & 1 \end{bmatrix} = \begin{bmatrix} 333.33 & -333.33 \\ -333.33 & 333.33 \end{bmatrix} \begin{matrix} 3 & 4 \\ 4 & 3 \end{matrix}$$

Global stiffness

$$[K] = \begin{bmatrix} 66.67 & -66.67 & 0 & 0 \\ -66.67 & 266.67 & -200 & 0 \\ 0 & -200 & 533.33 & -333.33 \\ 0 & 0 & -333.33 & 333.33 \end{bmatrix} \begin{matrix} 1 & 2 & 3 & 4 \\ 2 & 1 & 3 & 4 \\ 3 & 2 & 1 & 4 \\ 4 & 3 & 2 & 1 \end{matrix}$$

At node 1; convection is taking place

$$[K_h] = hA \begin{bmatrix} 1 & 0 \\ 0 & 0 \end{bmatrix} = 25(1) \begin{bmatrix} 1 & 0 \\ 0 & 0 \end{bmatrix}$$
$$= \begin{bmatrix} 25 & 0 \\ 0 & 0 \end{bmatrix} \begin{matrix} 1 & 2 \\ 2 & 1 \end{matrix}$$

Global stiffness

$$[K] = [K] + [K_h]$$

$$[K] = \begin{bmatrix} 91.67 & -66.67 & 0 & 0 \\ -66.67 & 266.67 & -200 & 0 \\ 0 & -200 & 533.33 & -333.33 \\ 0 & 0 & -333.33 & 333.33 \end{bmatrix}$$

Force Vector

$$\begin{aligned} [F_h] &= A h T_{\infty} \begin{bmatrix} 1 \\ 0 \end{bmatrix} \\ &= 1 (25) (800) \begin{bmatrix} 1 \\ 0 \end{bmatrix} \\ &= \begin{bmatrix} 20,000 \\ 0 \end{bmatrix} \end{aligned}$$

Equilibrium eqn $[K][T] = [F]$

$$\begin{bmatrix} 91.67 & -66.67 & 0 & 0 \\ -66.67 & 266.67 & -200 & 0 \\ 0 & -200 & 533.33 & -333.33 \\ 0 & 0 & -333.33 & 333.33 \end{bmatrix} \begin{bmatrix} T_1 \\ T_2 \\ T_3 \\ T_4 \end{bmatrix} = \begin{bmatrix} 20000 \\ 0 \\ 0 \\ 0 \end{bmatrix}$$

Since Temp at node 4 ; $T_4 = 20^\circ\text{C}$

$$-200T_2 + 533.33T_3 - 333.33T_4 = 0$$

$$-200(T_2) + 533.33T_3 - 333.33(20) = 0$$

$$-200T_2 + 533.33T_3 = 6666.67$$

$$\therefore \begin{bmatrix} 91.67 & -66.67 & 0 \\ -66.67 & 266.67 & -200 \\ 0 & -200 & 533.33 \end{bmatrix} \begin{bmatrix} T_1 \\ T_2 \\ T_3 \end{bmatrix} = \begin{bmatrix} 20000 \\ 0 \\ 6666.67 \end{bmatrix}$$

$$T_1 = 304.76^\circ\text{C} ; T_2 = 119.05^\circ\text{C} ; T_3 = 57.14^\circ\text{C}$$

Nodal temp.

$$\begin{bmatrix} T_1 \\ T_2 \\ T_3 \end{bmatrix} = \begin{bmatrix} 304.76 \\ 119.05 \\ 57.14 \end{bmatrix}^\circ\text{C}$$