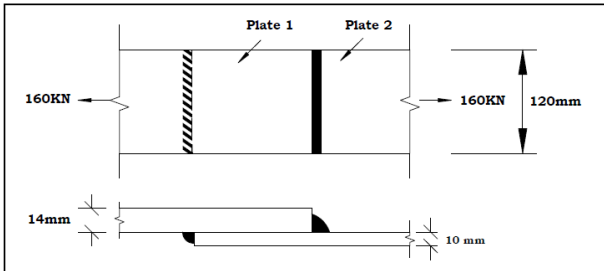
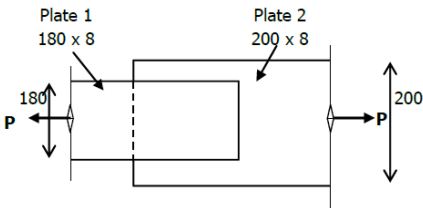


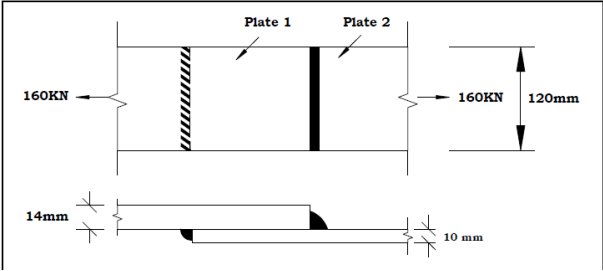
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Scheme and solution of Internal Assessment Test 2 – June 2022

Sub:	Design of steel structures	Sub Code:	18CV61	Branch:	Civil		
Date:	9/06/2022	Duration:	90 min's	Max Marks:	50		
		Sem / Sec:	6		OBE		
<b>Answer any ALL Questions</b>					<b>MARKS</b>	<b>CO</b>	<b>RBT</b>
<b>Note: Use of IS 800:2007 is permitted and assume missing data.</b>							
1 (a)	Design a suitable fillet weld to connect a tie bar 60mm X 8mm to a 12mm thick gusset plate. Assume shop welds. Use Fe 410 steel.		[05]	CO1	L2		
1 (b)	A tie bar of 120 mm x 10 mm(p2) is to be connected to other of size 120 mm x 14 mm(p1). if the tie bars are to be loaded by a pull of 160 KN, find out the size of end fillets such that the stresses in both the end fillets are same. Take $f_u=410 \text{ N/mm}^2$ , Assume shop welding. 8marks		[10]	CO1	L4		
1 (c)	Design the fillet welded joint between two plates of size 180 mm x 8 mm and 200 mm x 8 mm to develop the full strength of the smaller plate in tension. Assuming field welding.		[10]				
2(a)	A bracket plate 12mm thick is to be bolted to the flange of column ISHB 350@710.2 N.m by means of close tolerance and turned bolts. M20 bolts of grade 4.6 are arranged in two vertical row 100mm apart at a pitch of 70mm. Design a bracket connection if the bracket plate carries a load of 120kN at a lever arm of 250mm		[20]				
2(b)	Calculate the strength of 20mm dia bolt of grade 4.6 for the following cases. The main plates to be joined are 12mm thick. Lap joint		[5]				

	Marks
<p>1(b). A tie bar of 120 mm x 10 mm(p2) is to be connected to other of size 120 mm x 14 mm(p1). if the tie bars are to be loaded by a pull of 160 KN, <b>find out the size of end fillets</b> such that the stresses in both the end fillets are same. Take <math>f_u=410 \text{ N/mm}^2</math>, Assume shop welding.</p> 	10
<p>Let <math>D_1</math> and <math>D_2</math> be the size of the weld of Plate (1) and Plate (2)</p> $\frac{D_1}{D_2} = \frac{14}{10}$	1
<p><math>D_1 = 1.4D_2</math> Length of the weld in each case = 120mm</p>	
<p>Strength of the weld of Plate 1 = <math>0.707D_1 * l * f_{wd}</math>  <math>= 0.707 * 1.4D_2 * l * \frac{410}{\sqrt{3} * 1.25}</math>  <math>= 22492.72D_2 \text{ N}</math></p>	1
<p>Strength of the weld of Plate 2 = <math>0.707D_2 * l * f_{wd}</math>  <math>= 0.707 * D_2 * l * \frac{410}{\sqrt{3} * 1.25}</math>  <math>= 16066.23 D_2 \text{ N}</math></p>	1
<p>Load carried by the tie bars = 160 kN</p>	
<p>Since there are two sizes of the weld I,e <math>D_1</math> and <math>D_2</math></p>	
<p><math>P = P_1 + P_2</math>   <math>160 * 10^3 = 22492.72D_2 + 16066.23 D_2</math></p>	1
<p><math>D_2 = 4.15 \text{ mm}</math> say 5mm (minimum size of the weld = 3mm, maximum size of weld = <math>10 - 1.5 = 8.5 \text{ mm}</math>)</p>	1
<p><math>D_1 = 1.4D_2</math>  <math>= 1.4 * 5 = 7 \text{ mm}</math> (minimum size of the weld = 5mm, maximum size of weld = <math>14 - 1.5 = 12.5 \text{ mm}</math>)</p>	1
<p>Overlap length: it is the maximum of following  <math>4 * t = 4 * 10 = 40 \text{ mm}</math> and <math>40 \text{ mm}</math>  Width of plate (120 mm)</p>	2

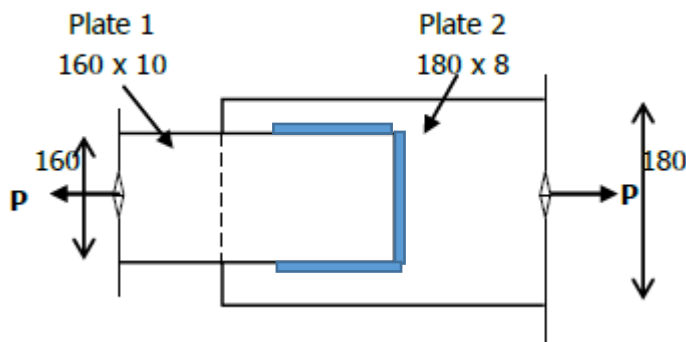
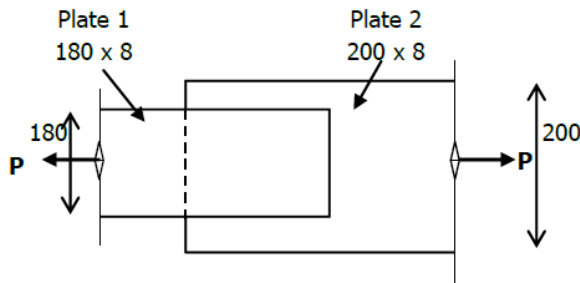
Length of longitudinal weld given = 120 mm

Provide 7 mm size weld for plate (1) and 5 mm size weld for plate (2) to a length of 120mm.

2

**1(c) Design the fillet welded joint between two plates of size 180 mm x 8 mm and 200 mm x 8 mm to develop the full strength of the smaller plate in tension. Assuming field welding.**

10



Tension capacity of the member 1 =  $T_{dg} = \frac{A_g \times f_y}{\lambda_{mo}} = \frac{160 \times 10 \times 250}{1.1 \times 1000} = 363.64 \text{N}$

1

Tension capacity of the member 2 =  $T_{dg} = \frac{A_g \times f_y}{\lambda_{mo}} = \frac{180 \times 8 \times 250}{1.1 \times 1000} = 327.30 \text{N}$

1

Strength of joint = full strength of thinner plate = 327.30 kN

Strength of weld =  $0.707 D * l * f_{wd}$   
 $= 0.707 * 8 * l * \frac{410}{\sqrt{3} * 1.5}$   
 $= 892.60 * L \text{ N}$

1

By condition equilibrium = total strength of joint = strength of weld  
 $= 327.03 * 10^3 = 892.60 * L$

Total length of the weld =  $L = \frac{327.30 * 1000}{892.60}$   
 $= 366.65 \text{ mm}$

1

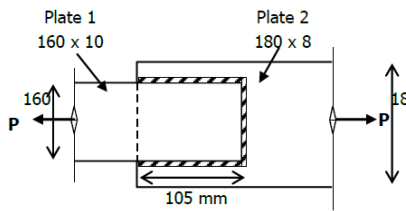
$B = 160 \text{ mm}$ ,  $16 * t = 16 * 8 = 128 \text{ mm}$ ,  
 since  $b$  is greater than  $16 * t$ , end fillet weld of length 160 mm has to be provided

1

along with longitudinal side fillet weld

$$\text{length of longitudinal weld on each side} = \frac{366.65 - 160}{2} = 103.32\text{mm}$$

$$= 105\text{mm}$$



**Length of longitudinal weld required:** It is the maximum of the following

1. Overlap length a)  $4 \times 8 = 32$  mm b) 40 mm
2. Length of longitudinal weld calculated = **105 mm.**

**1(a). Design a suitable fillet weld to connect a tie bar 60mm X 8mm to a 12mm thick gusset plate. Assume shop welds. Use Fe 410 steel.**

**Solution:**

**Effective length= $l$ =**

Tension capacity of the plate =  $T_{dg} = A_g f_y / \lambda_{m0}$

$$= 60 \times 8 \times 250 / 1.1 = 109.09\text{kN}$$

Strength of the weld =  $0.707D * l * \frac{f_u}{\sqrt{3} \lambda_{mw}}$

$$= 0.707 * 6 * l * \frac{410}{\sqrt{3} * 1.25}$$

$$= 803.31 \text{ l N/mm}$$

**On applying the equilibrium condition**

$$109.09 * 10^3 = 803.31 * l$$

$$l = 109.09 * 10^3 / 803.31 = 135.80\text{mm} = 140\text{mm is the total length of weld}$$

**Therefore, for each side  $140/2 = 70\text{mm}$**

D= size of the weld = minimum size of weld = 5mm

= maximum size of the weld =  $8 - 1.5 = 6.5\text{mm} = 6\text{mm}$

**Length of longitudinal weld required:** It is the **maximum** of the following

1. Overlap length a)  $4 \times 8 = 32$  mm b) 40 mm

2. Width of plate (60 mm)

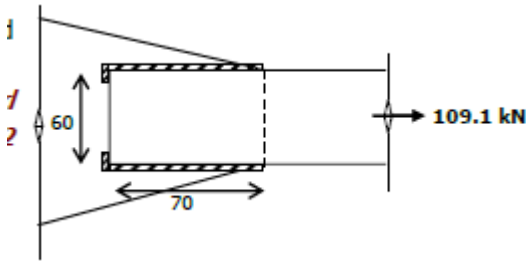
3. Length of longitudinal weld calculated = 70 mm

**The overall length of weld provided with end return of (2 x D) = 2 x 70 + 2 x 6 + 2 x 6 = 164 mm**

**Note:**

If  $b < 16t = 128$ , ----- only longitudinal weld can be provided =  $16 * 8 = 128$

If  $b > 16t$ , along with longitudinal weld End weld also should be provided



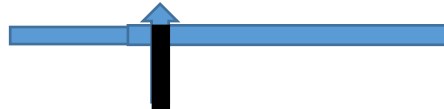
1

2(b) calculate the strength of 20mm dia bolt of grade 4.6 for the following cases. The main plates to be joined are 12mm thick.

a) Lap joint

**Solution:**

a) Lap joint



Strength of bolt in single shear: (assume fully threaded bolt)

$$V_{dsb} = \frac{f_{ub}}{\sqrt{3}} (n_n A_{nb} + n_s A_{sb}) / \gamma_{mb}$$

$$= \frac{400}{\sqrt{3}} (1 * 0.78 * \pi * 20 * 20 / 4 + 0) / 1.25 = 56.58 \text{ kN}$$

2

Bolts in Bearing =  $V_{dpb} = (2.5 K_b d t f_u) / \gamma_{mb}$

$K_b$  is least of  $e/3d_o$ ,  $p/3d_o - 0.25$ ,  $f_{ub}/f_u$ , 1 from the IS 800:2007 pg no 75

Assumed  $e=40\text{mm}$ ,  $p=50\text{mm}$ ,  $d_o=20+2=22\text{mm}$

$$40 / 3 * 22 = 0.60$$

$$50 / 3 * 22 - 0.25 = 0.50$$

$$400 / 410 = 0.97$$

1

$$V_{dpb} = (2.5 * 0.50 * 20 * 12 * 410) / 1.25 = 98.40 \text{ kN}$$

Therefore, the strength of bolt in lap joint is 56.58kN

2

1

2(a) A bracket plate 12mm thick is to be bolted to the flange of column ISHB 350@710.2 N.m by means of close tolerance and turned bolts. M20 bolts of grade 4.6 are arranged in two vertical row 100mm apart at a pitch of 70mm. Design a bracket connection if the bracket plate carries a load of 120kN at a lever arm of 250mm

From SP-6 Properties of ISHB 350= Weight=72.4 kg

C/S area= 92.21cm<sup>2</sup>

depth of section= 350mm = width of web

Width of flange = 250mm

Thickness of flange = 11.6 mm

No. of bolts calculation

No. of bolts for regular connection = Load/ bolt value ( $B_v$ )

Bolt value is the least of **Shear and Bearing strength**

No. of bolts for bracket connection=  $\sqrt{\frac{6M}{p m B_v}}$

Assume dia of bolt as 20mm

**1. Design shear strength of the bolt:**

a.  $V_{dsb} = V_{nsb} / \gamma_{mf}$

b.  $V_{dsb} = \frac{f_{ub}}{\sqrt{3}} (n_n A_{nb} + n_s A_{sb}) / \gamma_{mb} = \frac{400}{\sqrt{3}} (1 * 0.78 * \pi * 20 * 20 / 4) / 1.25 = 45.26 \text{ kN}$

As given in IS 800:2007, Pg no 75

**2. Design bearing strength of plate**

$V_{dpb} = (2.5 K_b d t f_u) / \gamma_{mb}$

$K_b$  is least of

$e / 3d_o$ ,

$p / 3d_o - 0.25$ ,

$f_{ub} / f_u$ ,

1

from the IS 800:2007 pg no 75

Assumed  $e = 1.7 * d_o = 1.7 * 22 = 37.5 \text{ mm} = 40 \text{ mm}$ ,  $p = 70 \text{ mm}$ ,  $d_o = 20 + 2 = 22 \text{ mm}$

$40 / 3 * 22 = 0.61$

$70 / 3 * 22 - 0.25 = 0.81$

$800 / 410 = 1.95$

1

$V_{dpb} = (2.5 * 0.61 * 20 * 11.6 * 410 * 10^{-3}) / 1.25 = 116.04 \text{ kN}$

**$B_v = \text{bolt value} = 45.26 \text{ kN}$**

No of bolting rows given in question=  $m = 2$

$M = \text{ultimate moment} = \text{Ultimate load} * \text{eccentricity} = (1.5 * 120) * 250 = 45000 \text{ kN-m}$

1. No of bolts for bracket connection=  $\sqrt{\frac{6M}{p m B_v}} = \sqrt{\frac{6 * 45000}{70 * 2 * 45.26}} = 6.85 = 7 \text{ no's}$

250mm

$\sum r^2 = r_1^2 + r_2^2 + r_3^2 \dots\dots\dots$

$$\sum r^2 = 4(50^2 + 210^2) + 4(50^2 + 140^2) + 4(50^2 + 70^2) + 2(50^2 + 0^2) = 309400 \text{mm}^2$$

Force on the extreme bolts  $F =$  Magnitude of Resultant force =  
 $\sqrt{F_1^2 + F_2^2 + 2F_1F_2\cos\theta} = \sqrt{25.71^2 + 31.39^2 + 2 * 25.71 * 31.39\cos76.6} =$  should  
 be always less than bolt value = 44.95kN hence safe

4

Direction of the force on the extreme bolt =  $\theta = \tan^{-1}\frac{210}{50} = 76.6$

$F_1 =$  force due to direct load =  $\frac{180}{7} = 25.71 \text{kN}$

4

$F_2 =$  force due to Moment acting =  $\frac{M * r_n}{\sum r^2} = \frac{45000 * 215.87}{309400} = 31.39 \text{kN}$

$r_n =$  distance between cg of the section to the center of the extreme bolt

$$r_n = \sqrt{50^2 + 210^2} = 215.87 \text{mm}$$