USN					



Internal Assessment	Test 3	ΙΔΝ	2023_Schem	e and colutions
THICHIAL ASSESSINCH		I /A I N .	-/W//)-/3 CHCHI	E AUG SOULIOUS

Sub:	Analysis of Ind	leterminate str	ructures			Sub Code:	18CV52	Branch:	Civil	Engg
Date:	19.01.2023	Duration:	90 min's	Max Marks:	50	Sem / Sec:	4	4 A		OBE
	0	1 1 .	1 .	0.6.11			. 04		MAR	CO RBT

1 (a)	Figure 1 shows a continuous beam ABCD, calculate the fixed end moments, if the	
	support D rotates by 0.002 radians in anticlockwise direction and supports B sinks by	
	8mm. Take E=210 GPa and I=0.1 Gmm4	

Question number 1 is mandatory; answer any 2 full questions from Q2 to Q4.

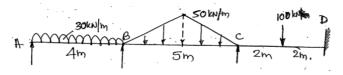
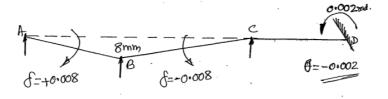


Fig.1.a



$$E = 210 \times 10^{9} \times 10^{6} = 210 \times 10^{3} \text{ N/mm}^{2}$$

$$EI = \frac{(210 \times 10^3)(0.1)10^9}{(10^3)(10^3)^2} = \frac{10000 \text{ kn-m}^2}{21000 \text{ kn-m}^2}$$

Additional moment =
$$-\frac{6ETS}{J^2}$$
 (Sinking)
$$= \frac{4ETO}{J} \Rightarrow \text{Near and Ratation}$$

$$=\frac{4EI0}{J}$$
 \rightarrow Near and Robotion

$$M_{Fd\theta} = -\frac{c_{0}1^{2}}{12} \underbrace{\frac{(6ETO)}{J^{2}}}_{12} = \frac{-30x4^{2}}{12} \underbrace{\frac{6(200)(9\cos 8)}{4^{2}}}_{2} = -103x0 \text{ km-t}$$

$$M_{F\theta\theta} = +\frac{c_{0}1^{2}}{12} \underbrace{\frac{(6ETO)}{J^{2}}}_{12} = \frac{-30x4^{2}}{96} \underbrace{\frac{6(200)(9\cos 8)}{4^{2}}}_{2} = -103x0 \text{ km-t}$$

$$M_{F\theta\theta} = +\frac{c_{0}1^{2}}{96} \underbrace{\frac{(6ETO)}{J^{2}}}_{12} = \frac{-5(50)5^{2}}{96} \underbrace{\frac{6(200)(-6\cos 8)}{5^{2}}}_{5^{2}}$$

$$M_{FC\theta} = -\frac{W1}{96} \underbrace{\frac{(6ETO)}{J^{2}}}_{12} = \frac{105x4}{96} \underbrace{\frac{2(2000)(-6\cos 8)}{5^{2}}}_{5^{2}}$$

$$M_{FC\theta} = -\frac{W1}{8} \underbrace{\frac{(6ETO)}{J^{2}}}_{12} = \frac{105x4}{8} \underbrace{\frac{2(2000)(-6\cos 8)}{4}}_{4} = -\frac{100x4}{8} \underbrace{\frac{2(2000)(-6\cos 8)}{4}}_{4}$$

$$= +8$$

$$2 (a) \text{ Analyse the continuous beam shown in Fig. 2.a by Kani's method and draw BMD, SFD}$$

$$M_{F\theta\theta} = -25 \text{ kn-m}, M_{F\theta\theta} = +25$$

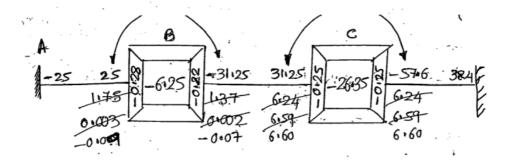
$$M_{F\theta\theta} = -25 \text{ kn-m}, M_{F\theta\theta} = +25$$

$$M_{F\theta\theta} = -31^{2}5, M_{FC\theta} = +31^{2}5$$

$$M_{F\theta\theta} = -576, M_{FD} = 38.4$$

(b)	Rotation	Factor	(For Intermediate	$\left(\cdot \right)$
\ -	The same of the sa		**	

		•		
		K	Σκ	U=(-1/2)K
	BA	1/4 = 0.251		-0.28
©	BC	I/5 = 0,50I	0:4SI	-0.22
	CB	I/5 = 0120I		-0.25
С	CD	T/5 = 0.20I	0'4I	-0125



$$m'8A = -0.28(-6.25 + 0) = 1.75$$

 $m'8C = -0.22(-6.25 + 0) = 1.37$
 $m'CO = -0.25(-26.35 + 1.37) = 6.24$
 $m'CD = -0.25(-26.35 + 1.37) = 6.24$

$$\begin{array}{c} \text{Toid}(2) \\ \text{m' Bh} = -0.028(-6.25 + 6.24) = 0.002. \\ \text{m' CB} = -0.022(-6.25 + 6.25) = 0.002 \\ \text{m' CB} = -0.025(-26.35 + 0.002) = 6.59 \\ \text{m' CD} = -0.025(-26.35 + 0.002) = 6.59 \\ \text{m' CD} = -0.025(-26.35 + 0.002) = 6.59 \\ \text{m' CD} = -0.025(-26.35 + 0.002) = 6.60 \\ \text{m' CD} = -0.025(-26.35 - 0.00) = 6.60 \\ \text{m' CD} = -0.025(-26.35 - 0.00) = 6.60 \\ \text{m' CD} = -0.025(-26.35 - 0.00) = 6.60 \\ \text{m' CD} = -0.025(-26.35 - 0.00) = 6.60 \\ \text{m' CD} = -0.025(-26.35 - 0.00) = 6.60 \\ \text{m' CD} = -0.025(-26.35 - 0.00) = 6.60 \\ \text{Mah} = -25 + 2(0) - 0.09 = -25.09 \text{ km·m G} \\ \text{Meh} = +25 + 2(-0.00) + 0 = 24.82 \text{ km·m G} \\ \text{MCB} = +31.25 + 2(-0.00) + 6.60 = -24.49 \text{ km·m G} \\ \text{MCD} = -54.6 + 2(6.60) - 0.00 = -44.40 \text{ G} \\ \text{MCD} = -54.6 + 2(6.60) - 0.00 = -44.40 \text{ G} \\ \text{MCD} = -54.6 + 2(6.60) - 0.00 = -45.84 \text{ km·m G} \\ \text{MCD} = -54.6 + 2(6.60) - 0.00 = -45.84 \text{ km·m G} \\ \text{MCD} = -54.6 + 2(6.60) - 0.00 = -45.84 \text{ km·m G} \\ \text{MCD} = -54.6 + 2(6.60) - 0.00 = -45.84 \text{ km·m G} \\ \text{MCD} = -54.6 + 2(6.60) - 0.00 = -45.84 \text{ km·m G} \\ \text{MCD} = -54.6 + 2(6.60) - 0.00 = -45.84 \text{ km·m G} \\ \text{MCD} = -54.6 + 2(6.60) - 0.00 = -45.84 \text{ km·m G} \\ \text{MCD} = -54.6 + 2(6.60) - 0.00 = -45.84 \text{ km·m G} \\ \text{MCD} = -54.6 + 2(6.60) - 0.00 = -45.84 \text{ km·m G} \\ \text{MCD} = -54.6 + 2(6.60) - 0.00 = -45.84 \text{ km·m G} \\ \text{MCD} = -54.6 + 2(6.60) - 0.00 = -45.84 \text{ km·m G} \\ \text{MCD} = -54.6 + 2(6.60) - 0.00 = -45.84 \text{ km·m G} \\ \text{MCD} = -54.6 + 2(6.60) - 0.00 = -45.84 \text{ km·m G} \\ \text{MCD} = -54.6 + 2(6.60) - 0.00 = -45.84 \text{ km·m G} \\ \text{MCD} = -54.6 + 2(6.60) - 0.00 = -45.84 \text{ km·m G} \\ \text{MCD} = -54.64 \text{ km·m G} \\ \text{MCD} = -54.84 \text{ km·m G} \\ \text{MCD} = -54.64 \text{ km·m G} \\ \text{MCD} = -54.84 \text{ km·m G} \\ \text{MCD} = -54.64 \text{ km·m G} \\ \text{MCD} = -54.44 \text{ km·m G} \\ \text{MCD} = -54.64 \text{ km·m G} \\ \text{MCD} = -54.64 \text{ km·m G} \\ \text{MCD} = -54.64 \text{ k$$

$$M_{FAB} = -\frac{\omega L}{8} = -\frac{20 \times 4}{8} = -10 \text{ kNm}$$

$$M_{FBA} = \frac{\omega L}{8} = \frac{20 \times 4}{3} = 10 \text{ kNm}$$

$$M_{FBA} = \frac{\omega L}{8} = \frac{20 \times 4}{3} = 10 \text{ kNm}$$

$$MF_{6C} = -\frac{\omega L^2}{l^2} = -\frac{15 \times 3^2}{l^2} = -11.25 \text{KNm}$$

$$M_{FCB} = \frac{\omega l^2}{12} = \frac{15 \times 3^2}{12} = 11 - 25 \text{kNm}$$

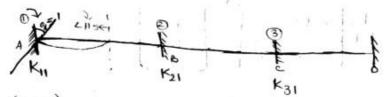
$$MF_{cD} = -\frac{\omega a b^2}{L^2} = -\frac{10 \times 2 \times 1^2}{3^2} = -2 \cdot 222 knm$$

$$MFac = \frac{\omega a^2 b}{l^2} = \frac{10 \times 4 \times 1}{9} = 4.944 \times Nm$$

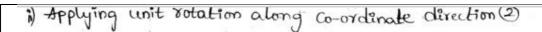
$$\begin{bmatrix} P \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix} \qquad \begin{bmatrix} PL \end{bmatrix} = \begin{bmatrix} -10 \\ -1 \cdot 25 \\ 9 \cdot 03 \end{bmatrix} \qquad \begin{bmatrix} \Delta \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \\ 0 \\ 0 \end{bmatrix}$$

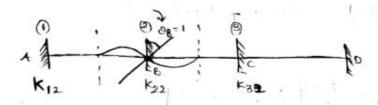
step 3 - Stiffners matrix

1) Applying unit rotation along co-ordenate direction 1

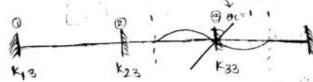


$$K_{21} = \left(\frac{2^{\prime}EI}{\lambda}\right)_{8A} = \frac{2EI}{4} = 0.5EI$$





Mi) Applying unit rotation along Co-ordinate direction 3



$$\begin{bmatrix} \mathbf{k} \end{bmatrix} = \begin{bmatrix} \mathbf{k}_{11} & \mathbf{k}_{12} & \mathbf{k}_{13} \\ \mathbf{k}_{21} & \mathbf{k}_{22} & \mathbf{k}_{23} \\ \mathbf{k}_{31} & \mathbf{k}_{32} & \mathbf{k}_{33} \end{bmatrix} = \begin{bmatrix} \mathbf{E} \\ \mathbf{E} \\ \mathbf{0} \end{bmatrix} \begin{bmatrix} \mathbf{0.5} & 2.333 & 0.667 \\ 0 & 0.667 & 2.667 \end{bmatrix}$$

$$M_{BC} = -11.25 + \frac{2}{3} \text{ FI} \left[2 \left(\frac{-0.778}{\text{EI}} \right) + \frac{-3.192}{\text{EI}} \right]$$

$$= -11.25 - 11.0373 - 2.123$$

$$M_{BC} = -14.451 \text{ kNm}$$

$$M_{CB} = 11.25 + \frac{2}{3} \text{ EI} \left[2 \left(\frac{-3.192}{\text{EI}} \right) + \left(\frac{-0.778}{\text{EI}} \right) \right]$$

$$= 11.2.5 - 4.256 - 0.5186$$

$$M_{B} = 6.4754 \text{ kNm}$$

$$M_{CD} = -2.222 + \frac{2}{2} \text{ EII} \left[2 \left(\frac{-3.192}{\text{EII}} \right) + (0) \right]$$

$$= -2.222 - 4.256$$

$$M_{CD} = -6.478 \text{ kNm}$$

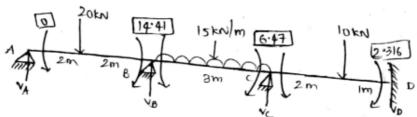
$$M_{CD} = -6.478 \text{ kNm}$$

$$M_{CD} = 4.444 + \frac{2}{3} \text{ EII} \left[0 + \left(-\frac{3.192}{\text{EII}} \right) \right]$$

$$= 4.449 - 2.128$$

$$M_{CD} = 2.316 \text{ kNm}$$

Steps: SED & BMD:



$$F_y = 0$$

 $7 V_A + V_0 + V_C + V_0 = 20 + 45 + 10$

$$= -V_0 \times 3 + 10 \times 2 + 2.316 - 6.47 = 0$$

$$V_0 = 5.282 \text{ kN}$$

$$9 \quad V_4 \times 7 + V_8 \times 3 + 6.47 - 20 \times 5 - 15 \times 3 \times \frac{3}{2} = 0$$

