

CMR INSTITUTE OF TECHNOLOGY

Analog Electronic Circuits-21EC34

Solution for Internal Assessment Test – II Dec2022

CMR
INSTITUTE OF
TECHNOLOGY

USN

--	--	--	--	--	--	--	--	--	--

Internal Assessment Test - II

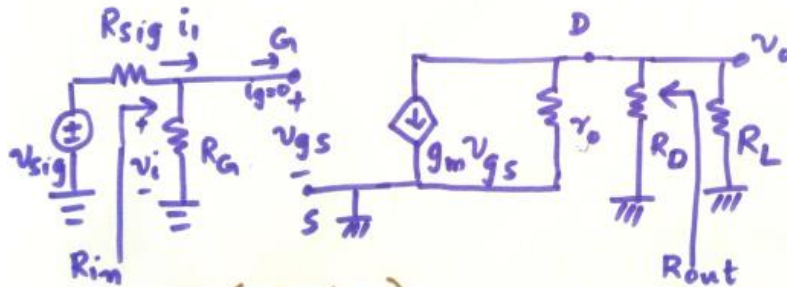
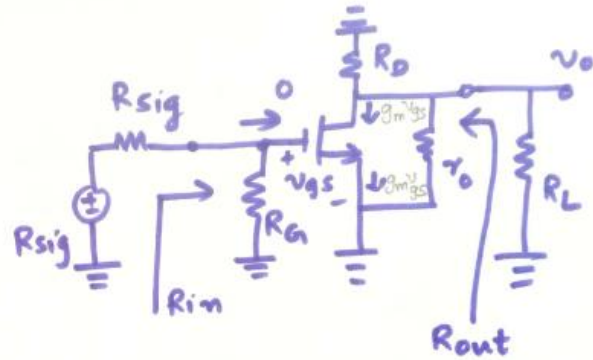
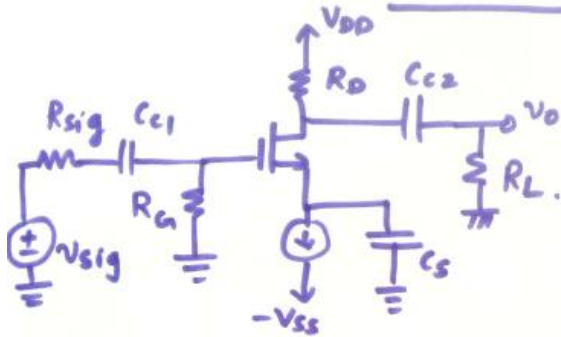
Sub:	Analog Electronic Circuits						Code:	21EC34	
Date:	27/ 12/ 2022	Duration:	90 mins	Max Marks:	50	Sem:	3 rd	Branch:	ECE
Answer Any FIVE FULL Questions									

		Marks	OBE	
			CO	RBT
1.	Using small signal model of MOSFET derive the overall gain and output impedance of CS amplifier without source resistance.	[10]	CO2	L3
2.	Draw and explain the complete frequency response of a common source amplifier. Derive the expression for its lower cut-off frequency.	[10]	CO2	L2
3.	Find the midband gain A_M , and the upper 3-dB frequency f_H of a CS amplifier fed with a signal source having an internal resistance $R_{sig} = 100 \text{ k}\Omega$. The amplifier has $R_G = 4.7\text{M}\Omega$, $R_D = R_L = 15 \text{ k}\Omega$, $g_m = 1\text{mA/V}$, $r_o = 150\text{k}\Omega$, $C_{gs} = 1\text{pF}$ and $C_{gd} = 0.4\text{pF}$	[10]	CO2	L3
4	State Barkhausen criteria for oscillation. With relevant circuit diagrams and equations explain the following a) Hartley Oscillator b) Crystal Oscillator.	[10]	CO2	L2

5.	Explain the working of a monostable multivibrator using 555 Timer IC. Design a circuit using 555 Timer to get a monoshot pulse of width 10ms. Choose $C = 0.1\mu\text{F}$	[10]	CO4	L3
6.	Explain the operation of 4-bit R-2R DAC with neat circuit. For the R-2R DAC, with $R = 10\text{k}\Omega$ and $R_F = 20\text{k}\Omega$ and $V_{REF} = 5\text{V}$, determine the output voltage when the inputs $b_2 = b_1 = 5\text{V}$ and $b_0 = b_3 = 0\text{V}$	[10]	CO4	L3
7	a) Derive the expression for gain with feedback for an operational amplifier in noninverting configuration. b) Write short notes on AC and DC amplifiers using opamp	[10]	CO4	L2
8.	A CS amplifier utilizes a MOSFET biased at $I_D = 0.25\text{mA}$ with $V_{OV} = 0.25\text{V}$ and $R_D = 20\text{k}\Omega$. The device has $V_A = 50\text{V}$. The amplifier is fed with a source having $R_{sig} = 100\text{k}\Omega$, and a $20\text{-k}\Omega$ load is connected to the output. Find R_{in} , A_{vo} , A_v and R_o and G_v . If to maintain reasonable linearity, the peak of the input sine-wave signal is limited to 10% of $(2V_{OV})$ what is the peak of the sine wave voltage at the output?	[10]	CO2	L3

1. Using small signal model of MOSFET derive the overall gain and output impedance of CS amplifier without source resistance.

Common Source Amplifier.



$$i_g = 0; R_{in} = R_G$$

$$v_i = v_{sig} \frac{R_{in}}{R_{in} + R_{sig}} = \frac{v_{sig} R_G}{R_G + R_{sig}}$$

$$R_G \gg R_{sig}; v_i \approx v_{sig}$$

$$v_{gs} = v_i$$

$$v_o = -g_m v_{gs} (r_o \parallel R_D \parallel R_L)$$

$$\text{Voltage gain } A_v = -g_m (r_o \parallel R_D \parallel R_L)$$

$$R_{out} = r_o \parallel R_D$$

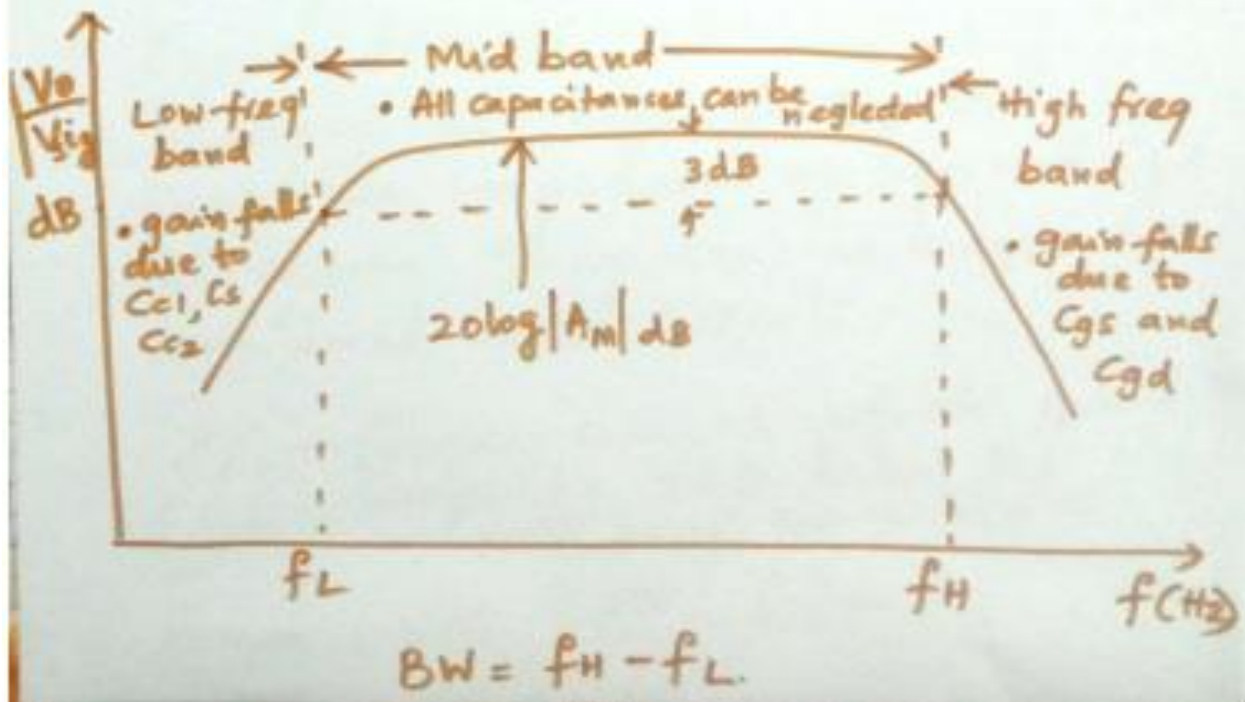
Overall voltage gain

$$G_v = \frac{R_{in}}{R_{in} + R_{sig}} A_v = \frac{R_G}{R_G + R_{sig}} (-g_m (r_o \parallel R_D \parallel R_L))$$

2. Draw and explain the complete frequency response of a common source amplifier. Derive the expression for its lower cut-off frequency.

FREQ RESPONSE OF CS AMPLIFIER.

- * Dependence of the gain of the MOSFET Common Source Amplifier on the frequency of the input signal.
- * C_{c1} , C_{c2} , C_s were acting as perfect shortckt when we studied the equivalent ckt model
- * Internal capacitances C_{gs} and C_{gd} were neglected.
- * These assumptions are valid only in Mid band Region \Downarrow



* Mid band gain A_m corresponds to the overall voltage gain G_v

$$A_m = \frac{V_o}{V_{sig}} = - \frac{R_G}{R_G + R_{sig}} g_m (r_o \parallel R_D \parallel R_L)$$

* Gain falls off in the low freq band because as freq \downarrow , capacitive impedance $X_c = \frac{1}{c\omega} = \frac{1}{c \times 2\pi f}$ increases for

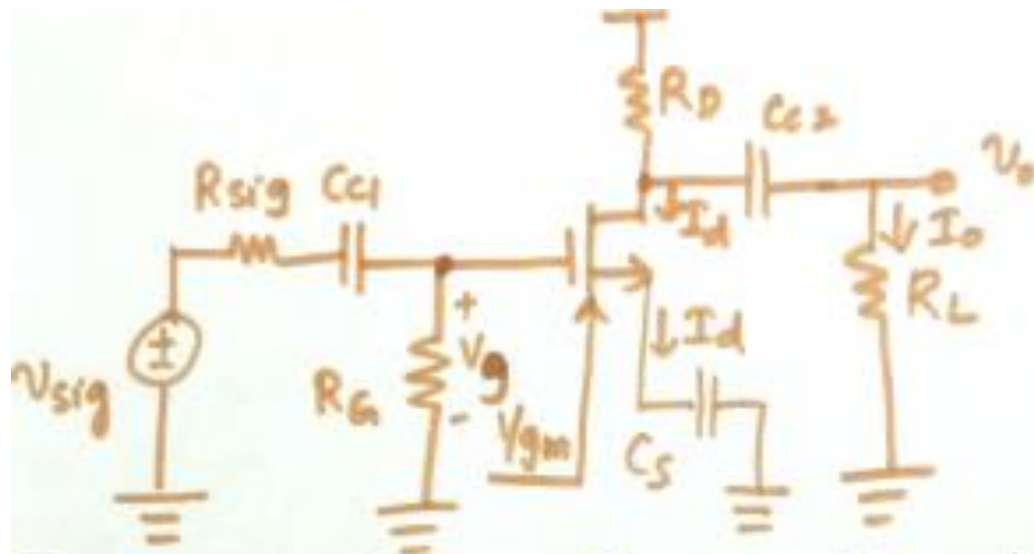
C_{e1}, C_{e2}, C_s . [of the order of μF].
So they no longer act as short circuits

* Gain falls off in the high freq band because at high freq, the capacitive impedance of C_{gs} and C_{gd} decreases. They can no longer be considered open circuits

* f_L - frequencies at which gain drops by 3dB below the mid band gain value.

* Band width (BW) = $f_H - f_L$

Low Frequency Response



To find the low-freq Response, V_{DD} and V_{SS} voltage sources are short circuited, current source I is open circuited. The coupling capacitors and by pass capacitor is taken into consideration. For simplicity r_o is neglected (it has minor effect also)

$$V_g = V_{sig} \cdot \frac{R_G}{R_{sig} + \frac{1}{sC_{c1}} + R_G}$$

In low freq Response, we need to consider the effect of 3 capacitors. All of them affect the Low frequency Response.

There will be three break frequencies represented as :-

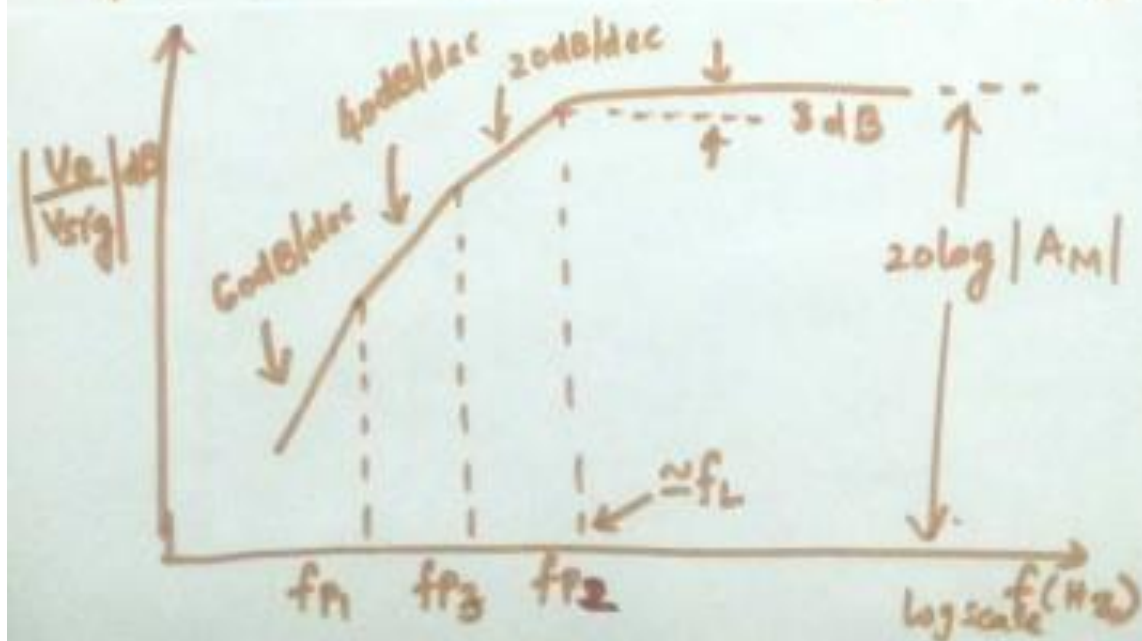
$$\omega_{p1} = \frac{1}{C_1(R_G + R_{sig})}$$

$$\omega_{p2} = \frac{g_{m0}}{C_5}$$

$$\omega_{p3} = \frac{1}{C_2(R_D + R_L)}$$

Over all low-frequency transfer function is given by

$$\frac{V_o}{V_{sig}} = - \left[\frac{R_G}{R_G + R_{sig}} \right] (g_m R_D \parallel R_L) \left(\frac{s}{s + \omega_{p1}} \right) \left(\frac{s}{s + \omega_{p2}} \right) \left(\frac{s}{s + \omega_{p3}} \right)$$



3. Find the midband gain A_M , and the upper 3-dB frequency f_H of a CS amplifier fed with a signal source having an internal resistance $R_{sig} = 100 \text{ k}\Omega$. The amplifier has $R_G = 4.7 \text{ M}\Omega$, $R_D = R_L = 15 \text{ k}\Omega$, $g_m = 1 \text{ mA/V}$, $r_o = 150 \text{ k}\Omega$, $C_{gs} = 1 \text{ pF}$ and $C_{gd} = 0.4 \text{ pF}$

The equivalent capacitance, C_{eq} , is found as

$$\begin{aligned} C_{eq} &= (1 + g_m R'_L) C_{gd} \\ &= (1 + 7.14) \times 0.4 = 3.26 \text{ pF} \end{aligned}$$

The total input capacitance C_{in} can be now obtained as

$$C_{in} = C_{gs} + C_{eq} = 1 + 3.26 = 4.26 \text{ pF}$$

The upper 3-dB frequency f_H is found from

$$\begin{aligned} f_H &= \frac{1}{2\pi C_{in} (R_{sig} \parallel R_G)} \\ &= \frac{1}{2\pi \times 4.26 \times 10^{-12} (0.1 \parallel 4.7) \times 10^6} \\ &= 382 \text{ kHz} \end{aligned}$$

$$A_M = -\frac{R_G}{R_G + R_{sig}} g_m R'_L$$

where

$$R'_L = r_o \parallel R_D \parallel R_L = 150 \parallel 15 \parallel 15 = 7.14 \text{ k}\Omega$$

$$g_m R'_L = 1 \times 7.14 = 7.14 \text{ V/V}$$

Thus,

$$A_M = -\frac{4.7}{4.7 + 0.1} \times 7.14 = -7 \text{ V/V}$$

4. State Barkhausen criteria for oscillation. With relevant circuit diagrams and equations explain the following a) Hartley Oscillator b) Crystal Oscillator.

III) Oscillation Criterion: (Barkhausen Criterion)

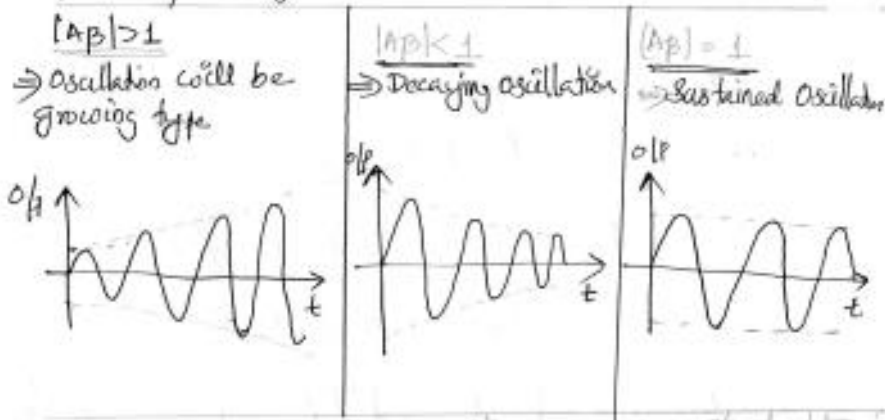
The condition for the feedback loop to provide sinusoidal oscillation

$$1 - A(j\omega_0)\beta(j\omega_0) = 0$$

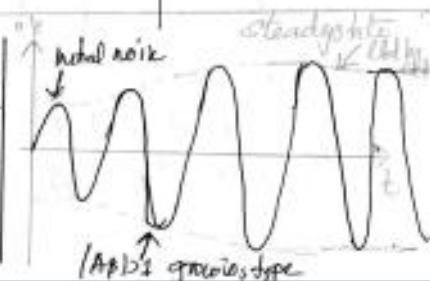
or $|A(j\omega_0)\beta(j\omega_0)| = 1$ and $\angle A(j\omega_0)\beta(j\omega_0) = 0$ or 360°

Condition:

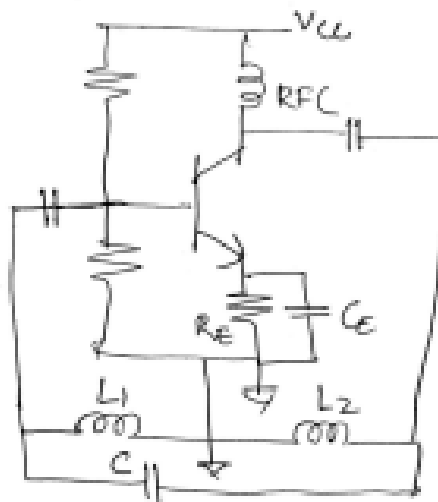
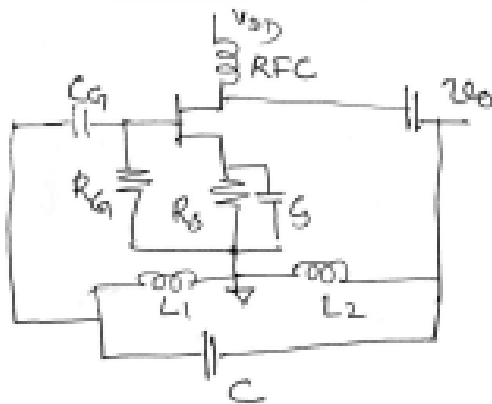
To produce sustained oscillation at ω_0 , the magnitude of loop gain should be unity and phase of loop gain should be zero.



*** In practical scenario $|A\beta| > 1$
 \rightarrow It is not possible to keep $|A\beta| = 1$
 then after some time due to non linearity of amplifiers the steady state envelope gives sustained o/p.



Hartley Oscillator:



All the discussions related to Colpitt's oscillator is valid here too.

Frequency of oscillation

$$X_1 + X_2 = X_3$$

$$\omega L_1 + \omega L_2 = \frac{1}{\omega C}$$

$$(L_1 + L_2) \omega = \frac{1}{\omega C}$$

$$\omega^2 = \frac{1}{(L_1 + L_2) C}$$

$$2\pi f = \frac{1}{(L_1 + L_2) C} \Rightarrow$$

$$L_1 + L_2 \Rightarrow L_{eq}$$

mutual inductance

$$\Rightarrow L_1 + L_2 + 2M \Rightarrow L_{eq}$$

$$f = \frac{1}{2\pi \sqrt{L_{eq} C}}$$

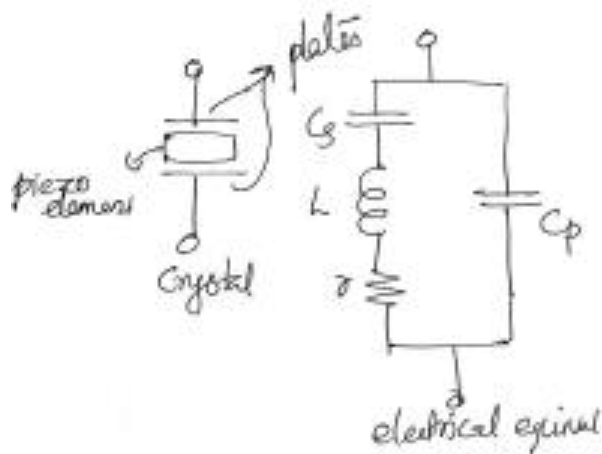
Note: To obtain sustained oscillations the amplifier gain must be greater than L_1/L_2

$$A > L_1/L_2$$

Crystal Oscillators:

Piezoelectric crystal such as quartz, exhibits electromechanical resonance that are very stable and highly selective.

(8)



$C_p \rightarrow$ capacitance b/w the two plates of the crystal.

- ① The resonance properties are characterised by large inductance L (10's H), very small series capacitor C_s (0.0005 pF) and series resistance r .

[$Q = \omega_0 L / r \Rightarrow$ hundred thousand]
parallel capacitance C_p (few pico farad)

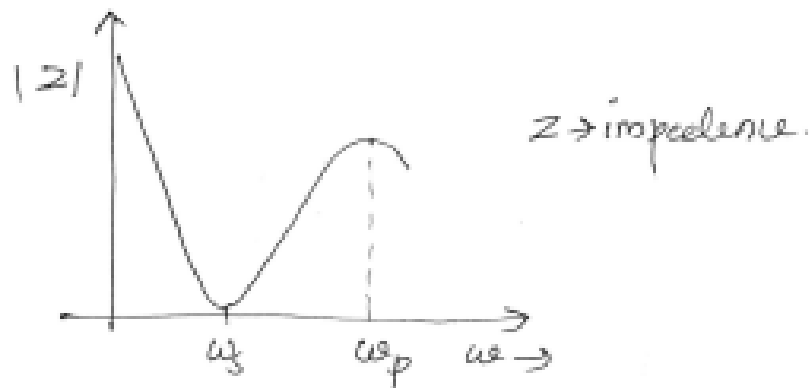
- ② The crystal will have a series resonance where the arm L, C_s and r will be purely resistive. This will happen when

$$X_L = X_{C_s} \Rightarrow \omega_s L = \frac{1}{\omega_s C_s} //$$

$$\boxed{\omega_s = \frac{1}{\sqrt{LC_s}}} \rightarrow \text{Series resonance freq.}$$

Parallel resonance will happen at a freq. ω_p when

$$X_L = X_{C_s} + X_{C_p} \Rightarrow \omega_p = \frac{1}{\sqrt{L \left(\frac{C_s C_p}{C_s + C_p} \right)}} //$$



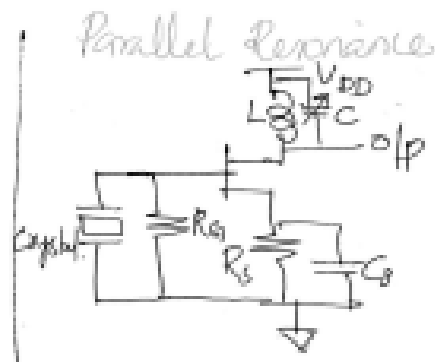
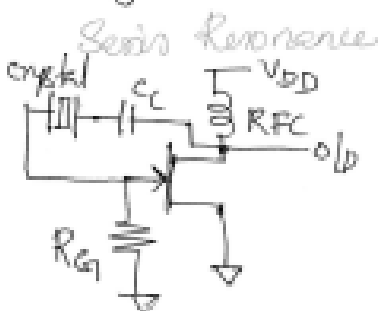
Piezoelectric effect

⊕ When an alternating voltage is applied across the crystal, mechanical vibrations are setup at a natural frequency.

⊖ When mechanical stress is applied, a difference in potential develops across the plates.

Note: Crystal oscillators are highly stable, so they are used in communication equipment and processor clock circuits.

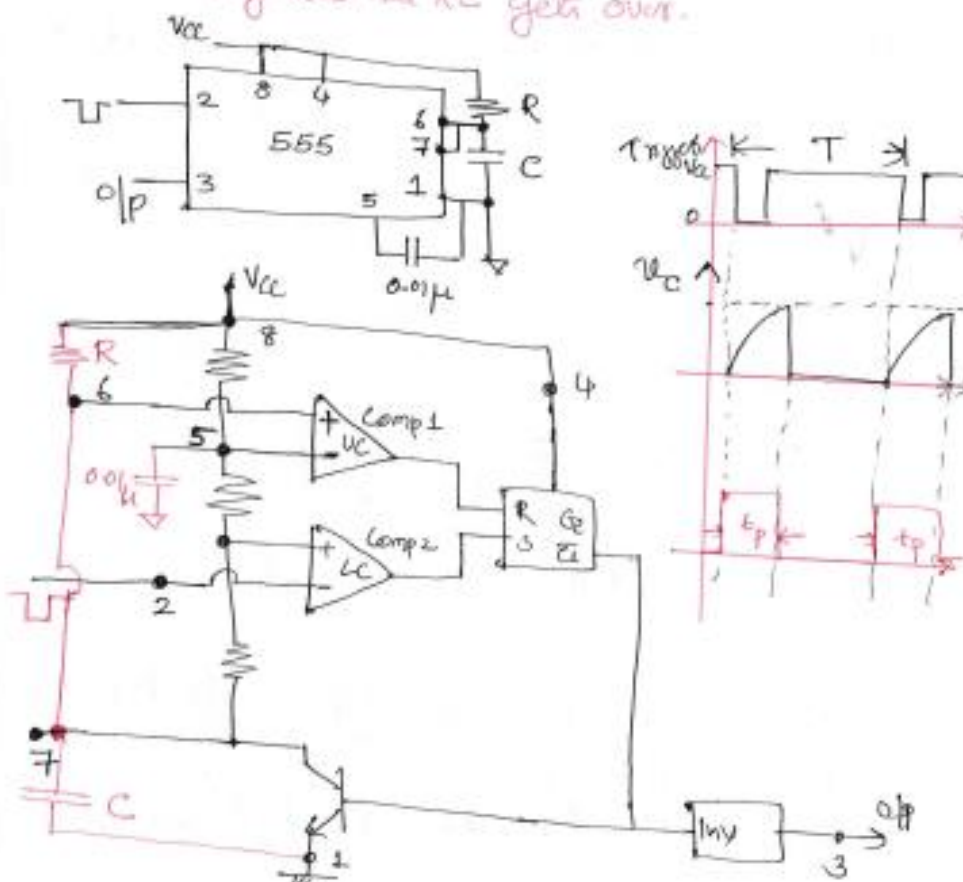
Crystal Oscillator ckt:



5. Explain the working of a monostable multivibrator using 555 Timer IC. Design a circuit using 555 Timer to get a monoshot pulse of width 10ms. Choose $C = 0.1\mu\text{F}$

Monostable Multivibrator using 555 IC (3)

- * It has one stable state:
- * It is also called as one shot, it is a pulse generating circuit.
- * The ckt remains in the stable state (normally logic zero). It will switch to quasi stable state once an external Trigger pulse is applied. It goes back to stable state once the time duration determined by external RC gets over.



I] When ckt is slw on, no trigger pulse present
capacitor voltage is zero

$$V_6 = 0, V_2 = V_{CC}$$

Upper comparator output will be '0' and lower
comparator output will be '0'

* $R=0, S=0$, F/F (retains the stable state)
becomes reset, $\Phi = 0, \bar{\Phi} = 1$

#SSS timer output zero. Transistor Φ is 'on'
capacitor won't be charging.

II] When a -ve trigger pulse is applied at Pin 2
The lower comparator output goes high

$S=1, R=0$, the F/F is set and Φ is

off. The output will be '1' (SSS o/p)

\Rightarrow the capacitor starts charging to V_{CC} thru R.
The trigger pulse will be removed, $S=0, R=0 \Rightarrow$ state remains
unchanged
once capacitor voltage reaches $\frac{2}{3}V_{CC}$

$$V_C > \frac{2}{3}V_{CC} \Rightarrow V_6 > \frac{2}{3}V_{CC}$$

the upper comparator state changes

$R=1$
 $S=0$ } F/F is reset, Φ is ON.

SSS output goes low. Capacitor discharge thru
 Φ . (Fast discharge) \rightarrow stable state. Remains here
till next pulse comes.

Time constant t_p (pulse width)

$t_p \rightarrow$ the time taken by capacitor to charge to $\frac{2}{3}V_{CC}$

from capacitor voltage eqn (charging)

$$V_c(t) = V_{final} + (V_{initial} - V_{final}) e^{-t/RC} \quad \text{--- (2)}$$

$$V_c(t_p) = \frac{2}{3} V_{CC} \quad t = t_p$$

$$V_{final} = V_{CC}, \quad V_{initial} = 0$$

from (2)

$$\frac{2}{3} V_{CC} = V_{CC} + (0 - V_{CC}) e^{-t_p/RC}$$

$$\frac{2}{3} - 1 = -e^{-t_p/RC}$$

$$\frac{1}{3} = e^{-t_p/RC}$$

$$3 = e^{t_p/RC}$$

$$\text{or } \boxed{t_p = (\ln 3) RC = 1.0986 RC \approx 1.1 RC}$$

$$1.1 RC = 10 \text{m}$$

$$\text{Given } C = 0.1 \mu\text{F}$$

$$R = 10 \text{m} / 1.1 * 0.1 \mu = 9.7 \text{kohm}$$

6. Explain the operation of 4-bit R-2R DAC with neat circuit. For the R-2R DAC, with $R=10\text{k}\Omega$ and $R_F=20\text{k}\Omega$ and $V_{REF}=5\text{V}$, determine the output voltage when the inputs $b_2=b_1=5\text{V}$ and $b_0=b_3=0\text{V}$

(ii) R-2R Ladder type DAC.

- Fig 5.2 represents a DAC with R and 2R resistors.

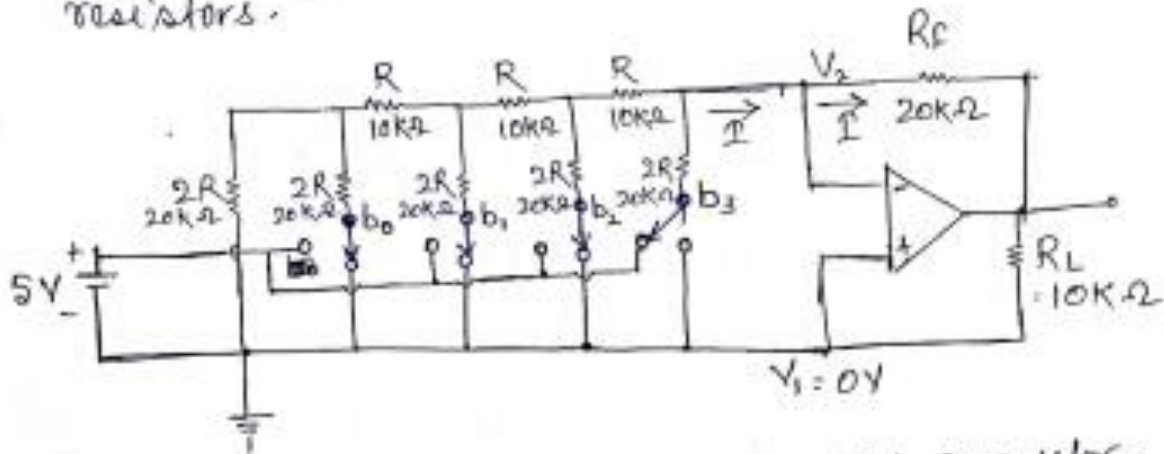


Fig 5.2.a :- D/A converter with R/2R resistor.

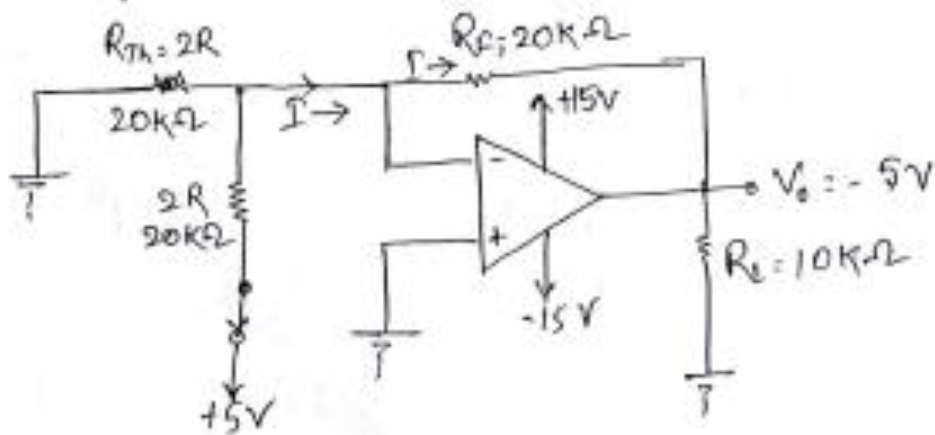


Fig 5.2.b :- Equivalent circuit when b_3 is high and b_0, b_1 & b_2 are low

- $b_0 \rightarrow$ LSB, $b_3 \rightarrow$ MSB (in 4-bit system).
- ~~For~~ ^{From} figure, a switch b_3 is connected to +5V (high) and other switches b_0, b_1 & b_2 are connected to ground, 0V (low).

- For particular set of inputs i.e.

$$b_3 \rightarrow 1$$

$$b_2 \rightarrow 0$$

$$b_1 \rightarrow 0$$

$$b_0 \rightarrow 0,$$

the Thevenin equivalent resistance R_T is, to the left of switch b_3 .

$$R_{Th} = \left[\left\{ \left[(2R \parallel 2R + R) \parallel 2R \right] + R \right\} \parallel 2R \right] + R$$

$$= 2R = 20k\Omega$$

- From Fig 5.2.b, it is clear, that R_{Th} is connected to ground, hence the current through R_{Th} will be zero. But the resistance $2R$ is connected to $+5V$, so the current flowing through $2R$ will be $5V/20k\Omega = 0.25mA$. This very same current flows through R_F . So, the output voltage will be.

$$V_o = -(20k\Omega)(0.25mA) = -5V.$$

- Therefore the output voltage equation can be written as

$$V_o = -R_F \left(\frac{b_3}{2R} + \frac{b_2}{4R} + \frac{b_1}{8R} + \frac{b_0}{16R} \right) \quad (5.2)$$

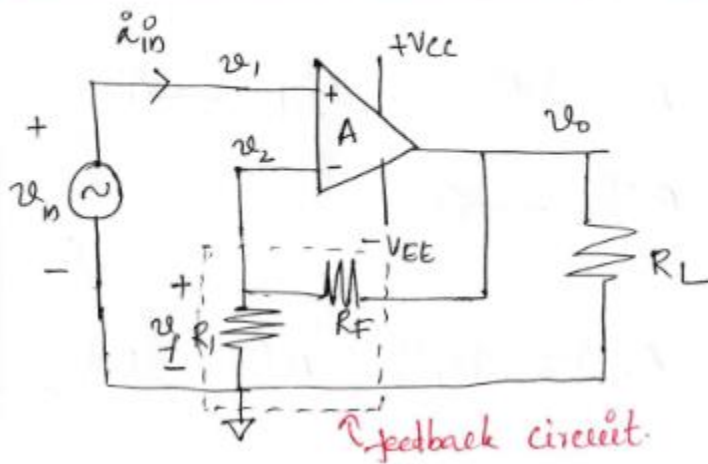
$$b_2 = b_1 = 5$$

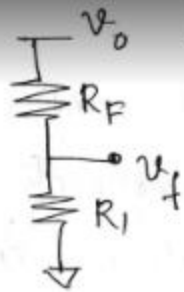
$$V_o = -20 \times 5 / 10 \left(\frac{1}{4} + \frac{1}{8} \right) = -3.75V$$

7. a) Derive the expression for gain with feedback for an operational amplifier in noninverting configuration. b) Write short notes on AC and DC amplifiers using opamp

a)

Non inverting Amplifier [Voltage Series feedback Amplifier]
with feedback





Open with ▾

$$v_f = \frac{v_o \times R_1}{R_1 + R_F}$$

$$B = \frac{v_f}{v_o} = \frac{R_1}{R_1 + R_F}$$

Substituting value of B in (3)

$$A_F = \frac{A}{1 + \frac{A R_1}{R_1 + R_F}} = \frac{A(R_1 + R_F)}{R_1 + R_F + A R_1} \quad (4)$$

Note: In ideal case $A \gg \frac{R_1 + R_F}{R_1}$. Typically is the order of \wedge thus if ideal op-amp is considered

$$1 + \frac{A R_1}{R_1 + R_F} \approx \frac{A R_1}{R_1 + R_F} \quad \text{OR}$$

$$R_1 + R_F + A R_1 \approx A R_1$$

thus eqn (4) becomes under ideal con.

$$A_F = \frac{A(R_1 + R_F)}{A R_1} = 1 + \frac{R_F}{R_1} \quad (5)$$

b)

DC and AC Amplifiers.

Based on the signal to amplify, the amplifier can be of two types.

- DC Amplifier
- AC Amplifier.

DC Amplifier.

In a DC amplifier the output signal changes in response to changes in its dc input levels. A dc amplifier can be inverting, non-inverting or differential.

AC Amplifier.

AC amplifier responds to the ac input. It is used ~~needed~~ when ac response characteristics i.e. low and high frequency limits ~~of the~~ is needed. Also if the ac input is riding on some dc level, it is necessary to use an ac amplifier with coupling ~~capacit~~ capacitor.

The coupling capacitor not only blocks the dc voltages but also sets but also sets the low frequency cut-off limit, given by

$$f_L = \frac{1}{2\pi C_i (R_{iF} + R_o)}$$

where, f_L = low-frequency cut-off.

C_i = coupling capacitor or dc blocking capacitor.

R_{iF} = ac input resistance

R_o = ac output resistance

8. A CS amplifier utilizes a MOSFET biased at $I_D = 0.25\text{mA}$ with $V_{OV} = 0.25\text{V}$ and $R_D = 20\text{k}\Omega$. The device has $V_A = 50\text{V}$. The amplifier is fed with a source having $R_{sig} = 100\text{k}\Omega$, and a $20\text{-k}\Omega$ load is connected to the output. Find R_{in} , A_{vo} , A_v and R_o and G_v . If to maintain reasonable linearity, the peak of the input sine-wave signal is limited to 10% of $(2V_{OV})$ what is the peak of the sine wave voltage at the output?

For CS amplifier

$$R_{in} = R_G$$

$$A_v = -g_m(r_o \parallel R_D \parallel R_L)$$

$$R_{out} = r_o \parallel R_D$$

$$G_v = \frac{R_G}{R_G + R_{sig}} g_m(r_o \parallel R_D \parallel R_L)$$

Here $R_G = \infty$

$R_{in} = \infty$

So $A_v = A_{vo}$

$$g_m = 2I_D/V_{OV} = 0.5\text{mS}$$

$$r_o = V_A/I_D = 200\text{k}\Omega$$

$$A_v = -0.5\text{m} \cdot (200 \parallel 15 \parallel 15)\text{k}$$

$$= -7.3\text{V/V}$$

$$R_{out} = 13.9\text{k}\Omega$$

$$G_v = A_v = -7.3\text{V/V}$$