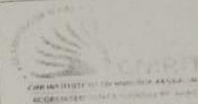


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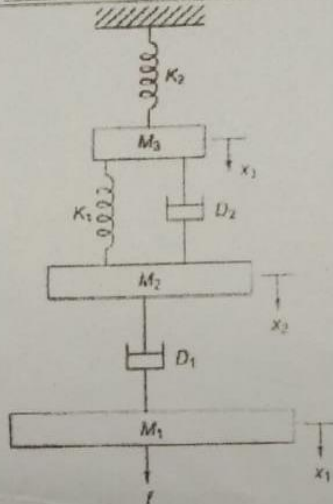


Internal Assessment Test 2 – Dec 2022

Sub:	Control Engineering	Sub Code:	18ME71	Bran
Date:	01/12/22	Duration:	90 min's	Max Marks: 50
			Sem / Sec:	7 th /A & B

Answer all FIVE Questions

1



Draw equivalent mechanical system of the given system. Hence write the set of equilibrium equations for it and obtain FV analogous circuit.

2 A unity feedback system has $G(s) = \frac{K}{s(s+2)(s^2+2s+5)}$

i) For a unit ramp input, it is desired that $e_{ss} \leq 0.2$. Find K.

ii) Determine e_{ss} if $r(t) = 2 + 4t + \frac{t^2}{2}$

3 Derive unit step response for a second order underdamped system.

4 Derive rise time and peak time for an underdamped second order system.

5 A unity feedback system is characterized by $G(s) = \frac{10}{s^2+2s+6}$

Determine :

- i) Undamped natural frequency
- ii) Damping ratio
- iii) Peak Time
- iv) Settling T
- v) Peak Overshoot

Basal
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1)

Sol. : M_2 is under $y_2(t)$. K_2 is between $y_2(t)$ and $y_1(t)$. And M_1 , K_1 and f are under $y_1(t)$. The equivalent mechanical system is shown in the Fig. 4.8.7 (a).

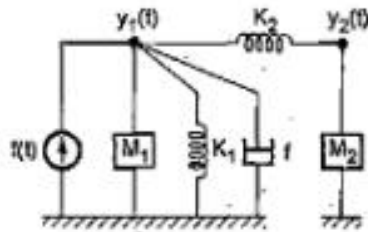


Fig. 4.8.7 (a)

The equilibrium equations are,

$$f(t) = M_1 \frac{d^2 y_1}{dt^2} + K_1 y_1 + f \frac{dy_1}{dt} + K_2 (y_1 - y_2) \quad \dots (1)$$

$$0 = K_2 (y_2 - y_1) + M_2 \frac{d^2 y_2}{dt^2} \quad \dots (2)$$

F-V analogy : $M \rightarrow L$, $f \rightarrow R$, $K \rightarrow \frac{1}{C}$, $y \rightarrow q$,
 $\frac{dy}{dt} \rightarrow \frac{dq}{dt} \rightarrow i$, $y \rightarrow \int i dt$, $\frac{d^2 y}{dt^2} \rightarrow \frac{di}{dt}$

The equations are,

$$v(t) = L_1 \frac{di_1}{dt} + \frac{1}{C_1} \int i_1 dt + R i_1 + \frac{1}{C_2} \int (i_1 - i_2) dt \quad \dots (3)$$

$$0 = \frac{1}{C_2} \int (i_2 - i_1) dt + L_2 \frac{di_2}{dt} \quad \dots (4)$$

Simulating on loop basis the analogous network is as shown in the Fig. 4.8.7 (b).

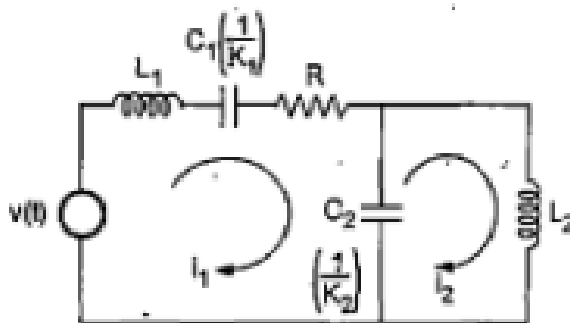


Fig. 4.8.7 (b)

2)

Sol : For a given system,

$$G(s)H(s) = \frac{K}{s(s+2)(s^2+2s+5)}$$

i) For unit ramp input, K_v is required.

$$\begin{aligned}\therefore K_v &= \lim_{s \rightarrow 0} sG(s)H(s) \\ &= \lim_{s \rightarrow 0} s \frac{K}{s(s+2)(s^2+2s+5)} = \frac{K}{10}\end{aligned}$$

and $A = \text{Magnitude of ramp} = 1$

$$\therefore e_{ss} = \frac{A}{K_v} = \frac{10}{K}$$

But $e_{ss} \leq 0.2$ i.e. $\frac{10}{K} \leq 0.2$ i.e. $K \geq 50$

Thus for given condition $50 \leq K < \infty$.

ii) $r(t)$ is $A_1 = 2$ step, $A_2 = 4$ ramp, $A_3 = 1$ parabolic

And $K_p = \lim_{s \rightarrow 0} sG(s)H(s) = \infty$

$$K_a = \lim_{s \rightarrow 0} s^2 G(s)H(s) = 0$$

$$\therefore e_{ss} = e_{ss1} + e_{ss2} + e_{ss3} = \frac{A_1}{1+K_p} + \frac{A_2}{K_v} + \frac{A_3}{K_a}$$

$$= \frac{2}{1+\infty} + \frac{4}{\left(\frac{K}{10}\right)} + \frac{1}{0} = \infty$$

3)

For underdamped systems, $\xi < 1$.

$\therefore s^2 + 2\xi\omega_n s + \omega_n^2 = 0$ has two roots,

$$s_{1,2} = -\xi\omega_n \pm j\omega_n\sqrt{1-\xi^2}$$

Now let $\xi\omega_n = \alpha$

and $\omega_n\sqrt{1-\xi^2} = \omega_d$ (as discussed earlier)

$\therefore s_{1,2} = -\alpha \pm j\omega_d$

For unit step input $R(s) = 1/s$ and

$$\frac{C(s)}{R(s)} = \frac{\omega_n^2}{s^2 + 2\xi\omega_n s + \omega_n^2}$$

Substituting $R(s)$, $C(s) = \frac{\omega_n^2}{s(s^2 + 2\xi\omega_n s + \omega_n^2)}$

The partial fraction can be calculated for the Laplace inverse as below,

$$C(s) = \frac{a_1}{s} + \frac{s_2 s + a_3}{s^2 + 2\xi\omega_n s + \omega_n^2}$$

$$\therefore \frac{\omega_n^2}{s(s^2 + 2\xi\omega_n s + \omega_n^2)} = \frac{a_1(s^2 + 2\xi\omega_n s + \omega_n^2) + s(a_2 s + a_3)}{s(s^2 + 2\xi\omega_n s + \omega_n^2)}$$

equating numerators on both sides, $\omega_n^2 = s^2(a_1 + a_2) + s(a_1 2\xi\omega_n + a_2) + a_1\omega_n^2 + a_3$

$\therefore a_1\omega_n^2 = \omega_n^2$ equating constant

$a_1 + a_2 = 0$ equating coefficients of s^2

$a_1 2\xi\omega_n + a_3 = 0$ equating coefficients of s

$\therefore a_1 = 1, a_2 = -1, a_3 = -2\xi\omega_n$

As $\xi\omega_n = \alpha$ assumed earlier for ease of computations.

$\therefore a_1 = 1, a_2 = -1, a_3 = -2\alpha$

$$\therefore C(s) = \frac{1}{s} + \frac{-s-2\alpha}{s^2 + 2\alpha s + \omega_n^2}$$

$$\therefore C(s) = \frac{1}{s} - \left\{ \frac{s+2\alpha}{s^2 + 2\alpha s + \omega_n^2} \right\} \quad \dots \text{(Taking negative sign outside)}$$

So adjusting denominator as, $s^2 + 2\alpha s + \alpha^2 + \omega_n^2 - \alpha^2 = (s+\alpha)^2 + \omega_n^2 - \alpha^2$

but $\alpha = \xi\omega_n \therefore \alpha^2 = \xi^2 \omega_n^2$

Substituting in above we get, $(s+\alpha)^2 + \omega_n^2 - \xi^2 \omega_n^2 = (s+\alpha)^2 + \omega_n^2 (1-\xi^2)$

Now $\omega_d = \omega_n\sqrt{1-\xi^2}$ i.e. $\omega_d^2 = \omega_n^2 (1-\xi^2)$

Substituting this in the expression of $C(s)$ we get,

$$\therefore C(s) = \frac{1}{s} - \left\{ \frac{s+2\alpha}{(s+\alpha)^2 + \omega_d^2} \right\}$$

$$L^{-1} \left\{ \frac{(s+\alpha)}{(s+\alpha)^2 + \omega_d^2} \right\} = e^{-\alpha t} \cos \omega_d t \quad \text{and} \quad L^{-1} \left\{ \frac{\omega_d}{(s+\alpha)^2 + \omega_d^2} \right\} = e^{-\alpha t} \sin \omega_d t$$

Adjusting $C(s)$ as,

$$C(s) = \frac{1}{s} - \left\{ \frac{s+\alpha}{(s+\alpha)^2 + \omega_d^2} + \frac{\alpha}{(s+\alpha)^2 + \omega_d^2} \right\}$$

Multiplying and dividing by ω_d to the last term,

$$C(s) = \frac{1}{s} - \left\{ \frac{s+\alpha}{(s+\alpha)^2 + \omega_d^2} + \frac{\alpha}{\omega_d} \frac{\omega_d}{(s+\alpha)^2 + \omega_d^2} \right\}$$

Taking Laplace inverse,

$$c(t) = 1 - e^{-\alpha t} \cos \omega_d t - \frac{\alpha}{\omega_d} e^{-\alpha t} \sin \omega_d t$$

Using $\alpha = \xi \omega_n$, $\omega_d = \omega_n \sqrt{1-\xi^2}$

$$c(t) = 1 - e^{-\xi \omega_n t} \left[\cos \omega_d t + \frac{\xi}{\sqrt{1-\xi^2}} \sin \omega_d t \right]$$

$$= 1 - \frac{e^{-\xi \omega_n t}}{\sqrt{1-\xi^2}} \left[\sqrt{1-\xi^2} \cos \omega_d t + \xi \sin \omega_d t \right]$$

• Now, $\sin(\omega_d t + \theta) = \sin \omega_d t \cos \theta + \cos \omega_d t \sin \theta$
 Comparing this with the expression in bracket we can write $\sin \theta = \frac{\xi}{\sqrt{1-\xi^2}}$ and $\cos \theta = \frac{\sqrt{1-\xi^2}}{\sqrt{1-\xi^2}}$.

Hence $\tan \theta = \frac{\xi}{\sqrt{1-\xi^2}}$

$$\therefore \theta = \tan^{-1} \frac{\xi}{\sqrt{1-\xi^2}} \text{ radians}$$

• Hence using this in the expression.

$$\therefore c(t) = 1 - \frac{e^{-\xi \omega_n t}}{\sqrt{1-\xi^2}} \sin(\omega_d t + \theta) \quad \dots \text{ Required expression}$$

where $\omega_d = \omega_n \sqrt{1-\xi^2}$
 and $\theta = \tan^{-1} \left(\frac{\xi}{\sqrt{1-\xi^2}} \right)$ radians

4)

7.16.1 Derivation of Peak Time T_p

Transient response of second order underdamped system is given by,

$$c(t) = 1 - \frac{e^{-\xi \omega_n t}}{\sqrt{1-\xi^2}} \sin(\omega_d t + \theta) \text{ where } \theta = \tan^{-1} \frac{\xi}{\sqrt{1-\xi^2}}$$

As at $t = T_p$, $c(t)$ will achieve its maxima. According to Maxima theorem,

$$\left. \frac{dc(t)}{dt} \right|_{t=T_p} = 0$$

So differentiating $c(t)$ w.r.t. 't' we can write,

$$\text{i.e. } -\frac{e^{-\xi \omega_n t} (-\xi \omega_n) \sin(\omega_d t + \theta)}{\sqrt{1-\xi^2}} - \frac{e^{-\xi \omega_n t}}{\sqrt{1-\xi^2}} \omega_d \cos(\omega_d t + \theta) = 0$$

Substituting $\omega_d = \omega_n \sqrt{1-\xi^2}$

$$\frac{\xi \omega_n e^{-\xi \omega_n t}}{\sqrt{1-\xi^2}} \sin(\omega_d t + \theta) - \frac{e^{-\xi \omega_n t}}{\sqrt{1-\xi^2}} \omega_n \sqrt{1-\xi^2} \cos(\omega_d t + \theta) = 0$$

$$\xi \sin(\omega_d t + \theta) - \sqrt{1-\xi^2} \cos(\omega_d t + \theta) = 0 \text{ i.e. } \tan(\omega_d t + \theta) = \frac{\sqrt{1-\xi^2}}{\xi}$$

Now $\theta = \tan^{-1} \frac{\xi}{\sqrt{1-\xi^2}} \text{ i.e. } \frac{\sqrt{1-\xi^2}}{\xi} = \tan \theta$

$$\tan(\omega_d t + \theta) = \tan \theta$$

From trigonometric formula,

$$\tan(n\pi + \theta) = \tan \theta$$

$$\omega_d t = n\pi \text{ where } n = 1, 2, 3$$

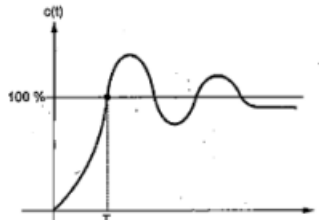
But T_p , time required for first peak overshoot. $\therefore n = 1$

$$\omega_d T_p = \pi$$

$$T_p = \frac{\pi}{\omega_d} = \frac{\pi}{\omega_n \sqrt{1-\xi^2}} \text{ sec}$$

7.16.3 Derivation of T_r

- Time required by output to achieve 100 % of its final value, starting from zero during the first attempt is the rise time.



$c(t)_{t = T_r} = 1$ for unit step input

$$\therefore 1 = 1 - \frac{e^{-\xi \omega_n T_r}}{\sqrt{1 - \xi^2}} \sin(\omega_d T_r + \theta)$$

$$\therefore - \frac{e^{-\xi \omega_n T_r}}{\sqrt{1 - \xi^2}} \sin(\omega_d T_r + \theta) = 0$$

Equation will get satisfied only if,

$$\sin(\omega_d T_r + \theta) = 0$$

Trigonometrically this is true only if,

$$\omega_d T_r + \theta = n \pi \text{ where } n = 1, 2, \dots$$

As we are interested in first attempt use $n = 1$

$$\therefore \omega_d T_r + \theta = \pi$$

$$\therefore T_r = \frac{\pi - \theta}{\omega_d} \text{ sec}$$

5)

Sol. :
$$\frac{C(s)}{R(s)} = \frac{20}{(s+1)(s+4)} = \frac{20}{s^2 + 5s + 24}$$

Fig. 7.16.4

Key Point Now though T.F. is not in standard form, denominator always reflect $2\xi \omega_n$ and ω_n^2 from middle term and the last term respectively.

\therefore Comparing, $s^2 + 5s + 24$ with $s^2 + 2\xi \omega_n s + \omega_n^2$

$$\therefore \omega_n^2 = 24 \therefore \omega_n = 4.8989 \text{ rad/sec.}$$

$$2\xi \omega_n = 5 \therefore \xi = 0.51031$$

$$\omega_d = \omega_n \sqrt{1 - \xi^2} = 4.2129 \text{ rad/sec.}$$

Now, for $c(t)$ we can use standard expression for $\frac{C(s)}{R(s)}$ in standard form. So writing

$$\frac{C(s)}{R(s)} = \frac{20}{24} \left[\frac{24}{s^2 + 5s + 24} \right]$$

For the bracket term use standard expression, and then $c(t)$ can be obtained by multiplying this expression by constant $\frac{20}{24}$.

$$\therefore c(t) = \frac{20}{24} \left[1 - \frac{e^{-\xi \omega_n t}}{\sqrt{1 - \xi^2}} \sin(\omega_d t + \theta) \right]$$

$$\theta = \tan^{-1} \frac{\sqrt{1 - \xi^2}}{\xi} \text{ radians} = 1.03 \text{ radians}$$

$$\therefore c(t) = \frac{20}{24} [1 - 1.1628 e^{-2.5t} \sin(4.2129 t + 1.03)]$$

