







## SCHEME OF EVALUATION



1a) 
$$
f_{\text{b}} = \frac{m_1 \cdot m_2}{\sqrt{m_1^2 + m_2^2 + m_1^2 + \cdots + m_n^2}} = \frac{m_1 \cdot m_2}{\sqrt{m_1^2 + m_2^2 + \cdots + m_n^2}} = \frac{m_1 \cdot m_2}{\sqrt{m_1^2 + m_2^2 + \cdots + m_n^2}} = \frac{m_1 \cdot m_2}{\sqrt{m_1^2 + m_2^2 + \cdots + m_n^2}} = \frac{m_1 \cdot m_2}{\sqrt{m_1^2 + m_2^2 + \cdots + m_n^2}} = \frac{m_1 \cdot m_2}{\sqrt{m_1^2 + m_2^2 + \cdots + m_n^2}} = \frac{m_1 \cdot m_2}{\sqrt{m_1^2 + m_2^2 + \cdots + m_n^2}} = \frac{m_1 \cdot m_2}{\sqrt{m_1^2 + m_2^2 + \cdots + m_n^2}} = \frac{m_1 \cdot m_2}{\sqrt{m_1^2 + m_2^2 + \cdots + m_n^2}} = \frac{m_1 \cdot m_2}{\sqrt{m_1^2 + m_2^2 + \cdots + m_n^2}} = \frac{m_1 \cdot m_2}{\sqrt{m_1^2 + m_2^2 + \cdots + m_n^2}} = \frac{m_1 \cdot m_2}{\sqrt{m_1^2 + m_2^2 + \cdots + m_n^2}} = \frac{m_1 \cdot m_2}{\sqrt{m_1^2 + m_2^2 + \cdots + m_n^2}} = \frac{m_1 \cdot m_2}{\sqrt{m_1^2 + m_2^2 + \cdots + m_n^2}} = \frac{m_1 \cdot m_2}{\sqrt{m_1^2 + m_2^2 + \cdots + m_n^2}} = \frac{m_1 \cdot m_2}{\sqrt{m_1^2 + m_2^2 + \cdots + m_n^2}} = \frac{m_1 \cdot m_2}{\sqrt{m_1^2 + m_2^2 + \cdots + m_n^2}} = \frac{m_1 \cdot m_2}{\sqrt{m_1^2 + m_2^2 + \cdots + m_n^2}} = \frac{m_1 \cdot m_2}{\sqrt{m_1^2 + m_2^2 + \cdots + m_n^2}} = \frac{m_1 \cdot m_2}{\sqrt{m_1^2 + m_2^2 + \cdots + m_n^2}} = \frac{m_1
$$

7.6 Liamal and: *Correlation* moving *a* a window constant magnitude *free*)

\n7.7 *the magnitude* from a window of a velocity of a two magnetic field 
$$
\vec{B}
$$
.

\n8.7  $\vec{F} = g(\vec{v} \cdot \vec{r})$ 

\n9.8  $\vec{F} = g(\vec{v} \cdot \vec{r})$ 

\n1.  $\vec{F} = g(\vec{v} \cdot \vec{r})$ 

\

V

1 b) Maxwell's equations to Point form: (For two varying fields)  
\n1 b) Maxwell's equation  
\n1 b) Muxwell's equation  
\n1 b) Muxwell's equation  
\n1 b) Muxwell's equation  
\n1 c) 
$$
\frac{d^2x}{dx^2} + \frac{d^2y}{dx^2} + \frac{d^2y}{dx^
$$

 $\chi$ 

Displacement

 $2a)$ 

current:

Point from of Ampere's circuital lace for steady magnétic fields  $\frac{\sqrt{2x+1} = 5}{\sqrt{2x+1}} = \frac{2}{\sqrt{2x+1}} = \frac{2}{\sqrt{2x+1}} = \frac{2}{\sqrt{2x+1}} = 0$ But from continuity equation  $\frac{1}{\sqrt{7}}\frac{1}{\sqrt{7}}$   $\frac{1}{\sqrt{7}}$   $\frac$ 

Suppose we add unknown of to 1  $\Rightarrow \boxed{\gamma x \overrightarrow{H} = \overrightarrow{J} + \overrightarrow{G}}$ 

> divergence, Tating  $\nabla \cdot \nabla x H = \nabla \cdot \vec{J} + \nabla \vec{G}$  $0 = F \cdot \vec{J} + F \cdot \vec{G}$  $\Rightarrow \boxed{7.6} = \frac{284}{64}$  $20.5.6$  $\nabla \cdot \vec{D} = \partial v.$  $\nabla \cdot \vec{G} = \frac{\partial \nabla \cdot \vec{D}}{\partial \vec{F}}$  $\nabla \cdot \vec{b} = \nabla \cdot \frac{\partial \vec{b}}{\partial t}$ The seluter's for G is obtained as  $67 = \frac{50}{22}$

Ampere's cardinal law to point form.  
\n
$$
\nabla x \vec{H} = \vec{J} + \frac{\partial \vec{D}}{\partial \vec{E}} \cdot \vec{X}
$$
\n
$$
\frac{\partial \vec{D}}{\partial \vec{E}} \rightarrow \text{has the dimensions } \varnothing \text{ current density } \gamma \cdot \vec{A/m}^2
$$
\n
$$
\hat{J} + \text{results from time varying displacement flux density}
$$
\n
$$
\text{Maxwell formed it as displacement current density}
$$
\n
$$
\nabla x \vec{H} = \vec{J} + \vec{J}d
$$
\n
$$
\nabla x \vec{H} = \vec{J} + \vec{J}d
$$
\n
$$
\vec{J} = \frac{\partial \vec{D}}{\partial \vec{E}}
$$

 $\widehat{83}$ 

In a non-conclucting medium, where 
$$
3y=0
$$
  $\Rightarrow$   $\vec{J}=0$ ,  
 $\nabla x\vec{H} = \frac{\partial \vec{D}}{\partial t}$  if  $\vec{J}=0$ 

Total displacement current crossing any given surface,  
\n
$$
Q = \int \overline{Jd} \cdot d\overline{S} = \int \frac{\partial \overline{D}}{\partial t} \cdot d\overline{S}
$$

$$
A \cdot c \cdot L \cdot \frac{1}{f^{\circ}} \frac{\text{Time varying conditions:}}{\int_{S} (\nabla \times H)^{3} \cdot dS} = \int_{S} \frac{1}{s} \cdot dS + \int_{S} \frac{\partial \vec{d}}{\partial t} \cdot dS
$$

 $2 b)$ <br>  $\epsilon = 1.2 \times 10^{-10} F/m$ <br>  $\epsilon = 1.2 \times 10^{-10} F/m$  $\vec{H} = 2cos(i\omega^{D}k - k\omega)a_{\theta}$ Colcolate  $\overrightarrow{B}$ ,  $\overrightarrow{D}$ ,  $\overrightarrow{E}$  and  $\overrightarrow{P}$ ,  $\vec{B} = \mu \vec{H} = 6 \times 10^{-5} cos(10^{10} \text{K} - \beta \text{K}) \hat{a_2}$  $\vec{d} \times \vec{H} = \frac{\partial \vec{B}}{\partial \vec{k}}$  $\begin{array}{rcl}\n\sqrt{3} \times \hat{H} &=& \hat{A} \times \hat{B} \\
&=& \hat{A} \times \hat{B} \\
&=& \hat{A} \times \hat{B} \\
&=& \hat{B} \times \hat{B} \\
&=& \hat{B} \times \hat{C} \\
&=& \hat{B} \times \hat{C} \\
&=& \hat{C} \times \hat{B} \\
&=& \hat{C} \times \hat{B} \\
&=& \hat{C} \times \hat{C} \\
&=& \hat{C} \times \hat{C} \\
&=& \hat{C} \times \hat{C} \\$  $\hat{a}_{\hat{\sigma}}$   $\hat{a}_{\hat{\sigma}}$  $\frac{3}{27}$   $\frac{1}{22}$ <br>0 2 us (10<sup>10</sup> k - 1<sup>8</sup> k)  $= - \hat{a}_{\partial \Omega} \frac{\partial}{\partial t} \left[ 2 \omega_{\theta} (10^{10} + - \beta t) \right]$  $= -2y$  2  $(-sin (-1)^{10} + -19x) (-19)$ = - 2 in  $(10^{10} + - \beta 1)^{\beta}$  ag  $\overrightarrow{D} = -2 \rho \int x^{\rho} (1^{\rho^{\rho}} + 1^{\rho} A) d\theta dt$ =  $+2\beta cos (\mu^0 + -\beta x) a_0$  $=\frac{2\beta}{10^{10}}cos(\beta^{0}x-\beta x)$   $\frac{\lambda}{\alpha y}sin^2(x)$ 

Now, 
$$
\vec{D} = \vec{E}
$$
  
\n
$$
\vec{E} = \frac{\vec{D}}{\epsilon} = \frac{2\beta cos(\vec{b} + \vec{b})}{\vec{a} + \alpha}
$$
  
\n
$$
= 1.66 \beta cos(\vec{b} + \vec{b})
$$
  
\n
$$
\vec{Q} \times \vec{E} = \begin{vmatrix} \frac{1}{2} & \frac{3}{2} & \frac{3}{2} \\ \frac{1}{3} & \frac{3}{2} & \frac{3}{2} \\ 0 & 1.66 \beta cos(\vec{b} + \vec{b}) \end{vmatrix}
$$
  
\n
$$
= 1.66 \beta cos(\vec{b} + \vec{b})
$$
  
\n
$$
\vec{Q} \times \vec{E} = \begin{vmatrix} \frac{1}{2} & \frac{3}{2} & \frac{3}{2} \\ \frac{1}{2} & \frac{3}{2} & \frac{3}{2} \\ 0 & 1.66 \beta cos(\vec{b} + \vec{b}) \end{vmatrix}
$$
  
\n
$$
= +1.66 \beta^2 sin(\beta^2 + \beta^2))
$$
  
\nNow,  $\vec{v} \times \vec{E} = -\frac{3\vec{v}}{2\kappa}$   
\n
$$
= +1.66 \beta^2 \hat{a} \cdot \vec{a} \cdot \vec{b} = -\frac{1.66 \beta^2 (sin(\vec{b} + \beta))}{2\kappa}
$$
  
\n
$$
= -1.66 \beta^2 \hat{a} \cdot \vec{a} \cdot \vec{b} = -\frac{1.66 \beta^2 (sin(\vec{b} + \beta))}{2\kappa} \hat{a} \cdot \vec{b}
$$
  
\n
$$
= -1.66 \beta^2 \hat{a} \cdot \vec{a} \cdot \vec{b} = \frac{cos(\vec{b} + \beta)}{2\kappa}
$$
  
\n
$$
= -1.66 \beta^2 \hat{a} \cdot \vec{a} \cdot \vec{b} = \frac{cos(\vec{b} + \beta)}{2\kappa}
$$
  
\n
$$
= -1.66 \beta^2 \hat{a} \cdot \vec{b} = \frac{cos(\vec{b} + \beta)}{2\kappa}
$$
  
\n
$$
= \frac{1.66 \times 10^{-
$$

 $=$   $\frac{1.66 \times 10^{-10}}{1.66 \times 10^{-10}}$   $\beta = \pm 600$ .

3 a) 
$$
\frac{\int \frac{\partial^2 f}{\partial x^2} \cdot \frac{\partial^2 f}{\partial y \partial y} \cdot \frac{\partial^2 f}{\partial z \partial x} \cdot \frac{\partial^2 f}{\partial y \partial y} \cdot \frac{\partial^2 f}{\partial z \partial y} \cdot \frac{\partial^2
$$

For good candidates,  
\n
$$
\sigma \approx \infty
$$
.  
\n $\frac{\sigma}{\omega e} \gg 1$   
\n $j\gamma^2 = j\omega\sqrt{\mu e^2} \sqrt{\frac{1 - j\sigma}{\omega e^2}}$   
\n $j\gamma^2 = j\omega\sqrt{\mu e^2} \sqrt{\frac{1 - j\sigma}{\omega e^2}}$   
\n $j\gamma^2 = j\omega\sqrt{\mu e^2} \sqrt{\frac{1 - j\sigma}{\omega e^2}}$   
\n $j\gamma^2 = j\omega\sqrt{\mu e^2} \sqrt{\frac{1 - j\sigma}{\omega e^2}}$   
\n $j\gamma^2 = j\sqrt{\omega\mu e^2} \sqrt{\frac{1 - j\sigma}{\sqrt{2}}}$   
\n $j\gamma^2 = j\sqrt{\omega\mu e^2} \sqrt{\frac{1 - j\sigma}{\sqrt{2}}}$   
\n $j\gamma^2 = \sqrt{\frac{\omega\mu e}{\sqrt{2}}} + j\sqrt{\frac{\omega\mu e}{\lambda}} = \sqrt{\pi i}$   
\n $j\gamma^2 = \sqrt{\frac{\omega\mu e}{\lambda}} + j\sqrt{\frac{\omega\mu e}{\lambda}} = \sqrt{\pi i/\mu e^2}$   
\n $j\gamma^2 = \sqrt{\frac{\mu}{\lambda}} = \sqrt{\frac{\mu}{\lambda} - \frac{\mu}{\lambda}} = \sqrt{\frac{\mu}{e'(\frac{1 - j\sigma}{e'})} + \frac{\mu}{e'(\frac{1 - j\sigma}{e'})}}$   
\n $j\gamma = \sqrt{\frac{\mu}{e' + \frac{\sigma}{\mu}} = \sqrt{\frac{j\omega\mu}{e'(\frac{1 - j\sigma}{e'})} + \frac{\mu}{e'(\frac{1 - j\sigma}{e'})}}$ 



As 
$$
\vec{F}
$$
 (or  $\vec{n}$ ) have  $\vec{a}$  a and  $\vec{c}$  are the  $\vec{c}$  is at the *u*-axis  $\vec{a}$  is at the *u*-axis  $\vec{c}$  is at the *u*-axis 

 $\begin{array}{c} \begin{array}{c} \hline \end{array} \\ \hline \end{array}$ 

$$
y = (\mu_{j}) \sqrt{\frac{\mu_{k}}{a^{2}}} \Rightarrow y = \sqrt{j} \sqrt{\frac{\mu_{k}}{a^{2}}} \quad \Rightarrow y = \sqrt{j} \sqrt{\frac{\mu_{k}}{a^{2}}} \quad \Rightarrow \quad (4\pi j) \sqrt{\frac{\mu_{k}}{a^{2}}} \quad \Rightarrow \quad (4\pi j) \sqrt{\frac{\mu_{k}}{a^{2}}} \quad \Rightarrow \quad y = \sqrt{\frac{\mu_{k}}{a^{2}}} \frac{1 + e^{2}}{1 + e^{2}} \quad \Rightarrow \quad y = \sqrt{\frac{\mu_{k}}{a^{2}}} \frac{1 + e^{2}}{1 + e^{2}} \quad \Rightarrow \quad y = \sqrt{\frac{\mu_{k}}{a^{2}}} \frac{1 + e^{2}}{1 + e^{2}} \quad \Rightarrow \quad y = \sqrt{\frac{\mu_{k}}{a^{2}}} \frac{1 + e^{2}}{1 + e^{2}} \quad \Rightarrow \quad y = \sqrt{\frac{\mu_{k}}{a^{2}}} \frac{1 + e^{2}}{1 + e^{2}} \quad \Rightarrow \quad y = \sqrt{\frac{\mu_{k}}{a^{2}}} \frac{1 + e^{2}}{1 + e^{2}} \quad \Rightarrow \quad y = \sqrt{\frac{\mu_{k}}{a^{2}}} \quad \Rightarrow \quad y = \sqrt{\frac{\mu_{k
$$

۲.J

**Solution.** We first evaluate the loss tangent, using the given data: 3 b)

$$
\textbf{5} \quad \textbf{D} \quad \frac{\sigma}{\omega \epsilon'} = \frac{4}{(2\pi \times 10^6)(81)(8.85 \times 10^{-12})} = 8.9 \times 10^2 \gg 1
$$

Seawater is therefore a good conductor at 1 MHz (and at frequencies lower than this). The skin depth is

$$
\delta = \frac{1}{\sqrt{\pi f \mu \sigma}} = \frac{1}{\sqrt{(\pi \times 10^6)(4\pi \times 10^{-7})(4)}} = 0.25 \text{ m} = 25 \text{ cm}
$$

Now

$$
\lambda = 2\pi \delta = 1.6 \text{ m}
$$

and

$$
v_p = \omega \delta = (2\pi \times 10^6)(0.25) = 1.6 \times 10^6
$$
 m/sec

4)<br>  $\frac{P_{opt}log_2 f}{P_{opt}} = \frac{P_{opt}log_2 f}{$ 

$$
\frac{1}{2} \int_{\alpha}^{2} (\vec{r} \times \vec{n}) = -\int_{\alpha}^{\alpha} \vec{r} \cdot \frac{\partial \vec{r}}{\partial t} - \sigma \vec{r} - \vec{r} \cdot \vec{r} \cdot \frac{\partial \vec{r}}{\partial t}
$$
\n
$$
\frac{1}{2} \int_{\alpha}^{2} (\vec{r} \times \vec{n}) = -\int_{\alpha}^{\alpha} \vec{r} \cdot \frac{\partial \vec{r}}{\partial t} - \int_{\alpha}^{\alpha} \vec{r} \cdot \frac{\partial \vec{r}}{\partial t}
$$
\n
$$
\frac{1}{2} \int_{\alpha}^{\alpha} \frac{\partial \vec{r}}{\partial t} + \int_{\alpha}^{\beta} \frac{\partial \vec{r}}{\partial t} +
$$

Pounting theorem . The equation becomes  $\oint_{S} (\vec{E} \times \vec{n}) \cdot d\vec{s} = -\sigma \iiint_{V} \vec{E}^{2} dV - \frac{d}{dE} \left[ \frac{1}{2} \iiint_{V} \epsilon \vec{E}^{2} dV \right]$ Rate of decrease of stored Concluction net power  $\frac{d}{dt}\left[\frac{1}{2}\iiint\mu H^2 d\nu\right]$ flowing<br>cut/ 8  $\mathcal{F}_{\mathcal{F}}$ Rate of docsease in stored magnetic energy  $\frac{1}{\sqrt{2}}$ Hence proved  $\omega$   $k$   $t$ Electric potentier lenoy  $W_E = \frac{1}{2}\iint e^{z-dy}$ Magnetic potential energy NH = 1/2 Jf MH 2dv Pours flow of an electromagnetic vare  $[ P = \oint_{S} (E \times H) \cdot dE$ มณ์ใ  $E\times H = P$  = Poynting rector = Power density ethere  $\boxed{\odot}$  $E$  $xH = S = \int$  fourthing vector  $\binom{N}{n^2}$ mis avenue.  $M_{\rm{eff}}$  $\alpha$  (b)

5) 
$$
\frac{A_{pp}h_{rad}k\omega}{2}\theta h_{p}k\omega d\omega + k\omega n \text{ (where } \omega \to \text{ cluster } B \text{ is marked}) \text{ and } \omega \to \text{ cluster } B \text{ is marked} \text{ and } \omega \to \text{ cluster } B \text{ is marked} \text{ and } \omega \to \text{ cluster } B \text{ is marked} \text{ and } \omega \to \text{ cluster } B \text{ is marked} \text{ and } \omega \to \text{ cluster } B \text{ is labeled} \text{ and } \omega \to \
$$

Find the 
$$
x \rightarrow 2
$$
 hence  $\frac{a}{3} \rightarrow \frac{b}{3}$   
\n
$$
\frac{D_{a,c}F_{out}}{2a} = \frac{D_{a} + \frac{d_1}{a_1} \cdot \frac{D_1}{a_2}}{2a} = \frac{D_{a} + \frac{d_1}{a_1} \cdot \frac{D_1}{a_2}}{2a} = \frac{2a}{3}
$$
\n
$$
\frac{1}{2a} \times \frac{a}{3a} = \frac{a}{3a} = \frac{a}{3a}
$$
\n
$$
\frac{1}{2a} \times \frac{a}{3a} = \frac{2b}{3a} = \frac{a}{3a} = \frac{a}{3a}
$$
\n
$$
\frac{1}{2a} \times \frac{a}{3a} = \frac{a}{3a} = \frac{a}{3a} = \frac{a}{3a} = \frac{a}{3a}
$$
\n
$$
\frac{1}{2a} \times \frac{a}{3a} = \frac{a}{3a} = \frac{a}{3a} = \frac{a}{3a} = \frac{a}{3a}
$$
\n
$$
\frac{1}{2a} \times \frac{1}{2a} = \frac{a}{3a} = \frac{a}{3a} = \frac{a}{3a} = \frac{a}{3a} = \frac{a}{3a}
$$
\n
$$
\frac{1}{2a} \times \frac{1}{2a} = \frac{a}{3a} = \frac{a}{3a}
$$

$$
\int_{0}^{1} \int_{0}^{1} f \cdot d\overline{J} = \frac{\partial D_{\overline{A}}}{\partial x} dx dy dz + \frac{\partial P_{\overline{A}}}{\partial y} du dy dz + \frac{\partial P_{\overline{A}}}{\partial y} du
$$

Two has other the second relation	velocity	by	by	by	by	by	by
\n $\left(\frac{\partial pa}{\partial x} + \frac{\partial p}{\partial y} + \frac{\partial p}{\partial z}\right) \cdot \frac{\partial^2 f}{\partial y} \cdot \frac{df}{\partial y} \cdot \frac{df$							

Divergence of  $\vec{p}$  = div  $\vec{B}$  = lim  $\frac{\oint \vec{p}^T \cdot d\vec{s}}{\oint \vec{p}^T \cdot d\vec{s}}$ Bivergne of the Irective flux density it is the outflow of flow from a  $\begin{array}{ccc} \hline \text{div } b: & \frac{\partial D_{n-1}}{\partial n} & \frac{\partial D_{y}}{\partial y} & \frac{\partial D_{z}}{\partial z} \end{array} \quad \begin{array}{ccc} \text{Rotangular} \end{array}$ Cylindrical  $\int d\pi r \vec{p} = \frac{1}{6} \frac{\partial}{\partial \rho} (\rho p \rho) + \frac{1}{6} \frac{\partial p}{\partial y} + \frac{\partial p}{\partial z}$  $\int d^{3}P \, \rho^{2} = \int_{\gamma^{2}} \frac{\partial}{\partial x} \left( \gamma^{2}D_{Y} \right) + \frac{1}{\gamma_{SMD}} \frac{\partial}{\partial \theta} \left( \sin \theta \right) \frac{\partial}{\partial \theta} + \frac{1}{\gamma_{SMD}} \frac{\partial p \phi}{\partial \phi}$ 

 $\left(\begin{array}{cc} \frac{\partial \rho_a}{\partial x} + \frac{\partial \rho_y}{\partial y} + \frac{\partial \rho_z}{\partial z} \end{array}\right)$  :  $\frac{\oint \tilde{b}^2 \cdot d\tilde{b}}{\Delta \Psi}$  :  $\frac{\partial \tilde{f}}{\partial v}$ .  $\left(\begin{array}{ccc}\n\frac{\partial P}{\partial x} & \frac{\partial P}{\partial y} & \frac{\partial P}{\partial z}\n\end{array}\right)$  =  $\lim_{\Delta x \to 0} \frac{\oint_{P} f \cdot ds}{\int_{P} f \cdot ds}$  =  $\left(\lim_{\Delta x \to 0} \frac{\partial P}{\partial x}\right) \to \lim_{\Delta x \to 0} \frac{\partial \log \log f}{\partial x}$  $\frac{\partial p_{\chi}}{\partial x} + \frac{\partial p_{\gamma}}{\partial y} + \frac{\partial p_{\tau}}{\partial z}$  =  $\frac{\partial p_{\eta}}{\partial x}$  =  $\frac{\oint p_{\tau}^{-1} d\zeta}{\partial x}$  $\frac{\partial n}{\partial x}$  =  $\frac{\partial v}{\partial x}$  $\rightarrow \circledcirc$ Dan et **SCANNED DY CANDOCANNER** 

As the volume shows to xero,  $lim_{\Delta v\rightarrow0}$   $\frac{f^{\beta}D^{r}\cdot d\overline{s}^{\beta}}{\Delta v}$   $lim_{\Delta v\rightarrow0}$  $\frac{9}{4}$ denoty volume  $cho$ Dungence  $R_{r}$ .  $dw =$  $(\hat{X})$ fist of Marcoell's four equations The electic flux per ceril volume learing a Vanishirgly small volume und<br>is exactly equal to the volume charge density there. Hatement Poul from Games's law Maxwells Arst equalarin Gauss law  $\rightarrow$   $\int_s^s f^1 ds = 0$  =  $\int_s^s f_v ds$ . Integral form of Marwell's first equality

6), find the double of the x is volume defined by a y planes  
\n
$$
\int \frac{1}{2}x^2y^2 = 3x^2 - 4x^2 - 8y^2 - 3y^2 + 3x^2 - 6y^2 - 6y^2 - 6z^2
$$
\n
$$
15x^2 - 6y^2 - 15x - 6x^2 - 8y^2 - 3y^2 + 3x^2 - 6z^2 - 6z^2
$$
\n
$$
8x^2 - 6y^2 - 15x - 6x^2 - 6y^2 - 6z^2 - 6z^2 - 6z^2 - 6z^2
$$
\n
$$
8x^2 - 6y^2 - 6z^2 -
$$

7 a) 
$$
\frac{1}{2} \int \frac{d\theta}{\theta} \frac{d\theta}{\theta} = \frac{d\theta}{2} \arctan \frac{d\theta}{\theta} = \frac{d\theta}{
$$

 $\sqrt{v \cdot f} = -\frac{\partial \mathcal{P}v}{\partial t}$  Point from of Continuity equality aurrent or change per second dimosang from a small volume por writ volume

 $\mathbf{u}$ 7 b)<br>
(1)  $\delta_v = \frac{1}{v^2} \frac{1}{v} \frac{1}{v} \frac{1}{v^2} \frac{1}{v} \frac{1}{v^3} \frac{1}{v^4} \frac{1}{v^5}$ <br>
The  $Sv^2a\overline{v}$ <br>  $= \frac{1}{v^2} \frac{1}{v^2} \frac{1}{v^5} \frac{1}{v^5} \frac{1}{v^5}$ <br>  $= \frac{1}{v^2} \frac{1}{v^5} \frac{1}{v^5} \frac{1}{v} \frac{1}{v^5} \frac{1}{v^5}$ <br>  $= \frac{1}{v^2}$ 

We are given the nonuniform field

$$
\mathbf{E} = y\mathbf{a}_x + x\mathbf{a}_y + 2\mathbf{a}_z
$$

and we are asked to determine the work expended in carrying 2C from *B*(1, 0, 1) to *A*(0.8, 0.6, 1) along the shorter arc of the circle

$$
x^2 + y^2 = 1 \quad z = 1
$$

**Solution.** We use  $W = -Q \int_B^A \mathbf{E} \cdot d\mathbf{L}$ , where **E** is not necessarily constant. Working in rectangular coordinates, the differential path  $d\mathbf{L}$  is  $dx\mathbf{a}_x + dy\mathbf{a}_y + dz\mathbf{a}_z$ , and the integral becomes

$$
W = -Q \int_{B}^{A} \mathbf{E} \cdot d\mathbf{L}
$$
  
= -2 \int\_{B}^{A} (y\mathbf{a}\_{x} + x\mathbf{a}\_{y} + 2\mathbf{a}\_{z}) \cdot (dx \mathbf{a}\_{x} + dy \mathbf{a}\_{y} + dz \mathbf{a}\_{z})  
= -2 \int\_{1}^{0.8} y \, dx - 2 \int\_{0}^{0.6} x \, dy - 4 \int\_{1}^{1} dz

where the limits on the integrals have been chosen to agree with the initial and final values of the appropriate variable of integration. Using the equation of the circular path (and selecting the sign of the radical which is correct for the quadrant involved), we have

$$
W = -2 \int_1^{0.8} \sqrt{1 - x^2} \, dx - 2 \int_0^{0.6} \sqrt{1 - y^2} \, dy - 0
$$
  
=  $-\left[ x \sqrt{1 - x^2} + \sin^{-1} x \right]_1^{0.8} - \left[ y \sqrt{1 - y^2} + \sin^{-1} y \right]_0^{0.6}$   
=  $-(0.48 + 0.927 - 0 - 1.571) - (0.48 + 0.644 - 0 - 0)$   
=  $-0.96 \text{ J}$ 

9)<br>  $\frac{Q_{\text{cr,rad}}}{q}$   $\frac{Q_{\text{c}}}{q}$   $\frac{Q_{\text{c}}}{q}$ <br>  $\frac{Q_{\text{c}}}{q}$   $\frac{Q_{\text{c}}}{q}$ <br>  $\frac{Q_{\text{c}}}{q}$ 

General Wire continue (4 the media considered  $\sinh(\alpha x)y$ Take curl on both sides of (4)  $\vec{r}$   $\vec{r}$   $\vec{r}$   $\vec{r}$  =  $\vec{r}$   $\sqrt{\sigma_E^2 + \epsilon \frac{\partial E}{\partial t}}$  $\vec{r}(\vec{v}^*_{t}) - \vec{v}^*_{t} = \sigma(\vec{v}^*_{t}) + \varepsilon \frac{\partial(\vec{v}^*_{t})}{\partial t}$ applying equation 2 Applying equation 5  $\mu \rightarrow \gamma^2 \vec{H} = -\sigma \cdot \mu \frac{\partial \vec{H}}{\partial t} = -2\mu \frac{\partial^2 \vec{H}}{\partial t^2}$  $\widehat{\nabla^2H}$  =  $\mu \sigma \frac{\partial H}{\partial t}$  +  $\mu \epsilon \frac{\partial^2 H}{\partial t^2}$ and  $\vec{H}(\varepsilon,t)$  $\n *T* + <$  $\frac{3^{2}h^{\dagger}}{3z^{2}}$  =  $\mu\sigma \frac{3h^{\dagger}}{3t} + \mu\epsilon \frac{3^{2}h^{\dagger}}{8t^{2}}$  =  $\frac{6}{5}$  feneral note equation equations (3 and 6 becomes. For free space  $6 - 6$ <br> $6 - 6$  $\mu$  =  $\mu$ Nave equation for free space for Edd  $\Rightarrow \left[\frac{\partial^2 \vec{E}}{\partial z^2} - \mu_0 \epsilon_0 \frac{\partial^2 \vec{E}}{\partial t^2}\right] \text{ (6)} \left[\frac{\partial^2 \vec{E}}{\partial t^2} - \mu_0 \epsilon_0 \frac{\partial^2 \vec{E}}{\partial t^2}\right]$ ا در این آ 

 $\alpha$   $\alpha$   $\alpha$