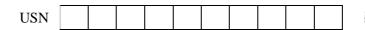
CMR INSTITUTE OF TECHNOLOGY





[10]

CO4

L2

Internal Assesment Test-III									
Sub:	Engineering Electromagnetics Code: 17EC36								
Date:	22/11 /2018	Duration:	90 mins	Max Marks:	50	Sem:	3rd	Branch:	ECE(A,B,C)
Answer FIVE FULL Questions									

		Ol	BE
	Marks	СО	RBT
1.(a) Using Faraday's law derive an expression for e.m.f induced in stationary conductor placed in a time varying magnetic field. Also explain motional e.m.f.	[06]	CO4	L2
(b) List Maxwell's equations in point and integral forms for time varying field.	[04]	CO4	L1
2.(a) What is the inconsistency of Ampere's law with the equation of continuity? Derive modified form of Ampere's law.	[05]	CO4	L2
(b) Let $\mu = 3 \times 10^{-5}$ H/m, $\epsilon = 1.2 \times 10^{-10}$ F/m and $\sigma = 0$ everywhere. If	[05]	CO4	L3
$H = 2\cos(10^{10}t - \beta x)a_z$ A/m, use Maxwell's equations to obtain the expressions for B , D , E .			
3.(a) Discuss TEM wave propagation in a good conductor. Define skin depth.	[07]	CO4	L2
(b) For a medium with $\sigma = 4.0$ S/m and $\varepsilon_r = 81$, evaluate skin depth at 1 MHz.	[03]	CO4	L3
4. State and explain Poynting's theorem.	[10]	CC	05 L2
-	[10]	CC)1 L2
 5. Derive point form of Maxwell's equation of electrostatics. 6. Find the total charge in a volume defined by the six planes for which 1 ≤x ≤2, 2 ≤y ≤3, 3 ≤z ≤4 if D = 4x a_x + 3y² a_y +2z³ a_z C/m². 	[10]	CC	
7.(a) Define current and current density. Derive the equation of continuity of current.	[02+04	4] CC	D2 L2
(b) Let $\mathbf{D} = 5r^2 \mathbf{a_r} \text{ mC/m}^2$ in the region for $r < 0.08m$. Find ρ_v at $r = 0.06m$.	[04]	CC)1 L3
8.(a) Derive an expression for the work done in moving a point charge Q in the presence of an electric field E .	[05]	CC	D2 L2
(b) Non uniform field is given by $\mathbf{E} = \mathbf{y} \mathbf{a}_{\mathbf{x}} + \mathbf{x} \mathbf{a}_{\mathbf{y}} + 2 \mathbf{a}_{\mathbf{z}} \mathbf{V}/\mathbf{m}$. Determine the work don	e [05]	CC)2 L3

in moving a charge of 2C from B(1, 0, 1) to A(0.8, 0.6, 1) along the path $x^2 + y^2 = 1$, z=1.

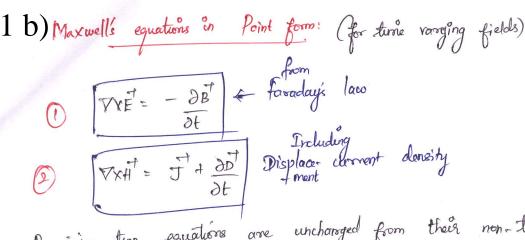
9. Starting from Maxwell's equations, derive wave equation for TEM wave.

SCHEME OF EVALUATION

		Mark Split-Up
1.a)	Transformer e.m.f	3
	Motional e.m.f.	3
1.b)	Point form	2
	Integral form	2
2.a)	Derivation	2
	Final Expression	3
2.b)	B, D, E	1+3+1
3.a)	Wave propagation in a good conductor	5
	Skin depth	2
3.b)	Formula	1
	Approach & Answer	2
4.	Statement	2
	Derivation	7
	Final expression	1
5.	Derivation	8
	Final Expression	2
6.	Formula	3
	Approach & Answer	7
7.a)	Current and Current Density	2
	Continuity Equation	4
7.b)	Formula	2
	Approach & Answer	2
8.a)	Diagram	1
	Derivation	3
	Final Expression	1
8.b)	Formula	2
	Approach & Answer	3
9.	Derivation	8
	Final Expression	2

1a) Pransformer em! Stationary path, magnetic flux is time varying (i) enj = $\int \vec{E} \cdot d\vec{L} = -\int \vec{\partial} \vec{E} \cdot d\vec{s}$. Faraday's lan applied to a fixed path. To obtain point from of this integral equation, Apply stokes theerem $\int (\nabla x \vec{\epsilon}) d\vec{s} = - \int \frac{\partial \vec{\epsilon}}{\partial t} d\vec{s}.$ surface integrals taken over identical surfaces. (VXE). ds = = = = = = = ds. ds. TIXE = - DET -> one of Naxwell's four equations. If B is not a function of time, PET. de so Celectrostatics)

Motional emf: (conductors moring in a uniform constant magnetic fretal)
frace on charge & moring at a velocity it is the magnetic field B. F= 9 (19 x B) F DRB Sliding bor - positive & negative charges experiencing this force. Force per unit charge - motional electric field intensity (Em) Em = 19 KB em = SEM. di = S(ret xist). di x. non zero only if Le is non zero enf = f(etxet)-dt = f veBdx = -Bred. B is not a function of time em = - Bud



Remaining two equations are uncharged from their non-time varying form.

(Charge density is the source of electric flux lines) From Oct equation, electric flux lines may form closed loops

are not known to exist,

Magnetic charges (on poles but every coulomb of charge have one coulomb of electric flux diverging from it)

Magnetic flux is always found En closed loops & never diverges

These four equations from the basis of all electromagnetic theory. They are partial differential equations, relate electric & magnetic fields to each other & to their sources, charge & current density.

Auxiliany equations relating electric & magnetic field quantities are: D'= EF B= HH Concluction current density J=5E assivection current density J= Pro

Maxwell's equations in Integral form:

Experiments must freat physical macroscopic quantities and their nesults are expressed in terms of integral relationships.

Integrating ever surface
$$\xi$$
 apply stokes' theorem
$$\int_{C} \int_{C} \frac{dx}{dx} = -\int_{C} \frac{\partial B'}{\partial t} \cdot dx$$

(()	ot ,
a learning over	surface and apply
Integrating over	
1557=	I+ 1 20 ds
9 H.dL =	s
Ĺ	

stokes

These four integral equations enable us to find boundary conditions on \$1, D, H&E

The boundary conditions are in general unchanged from their forms for static or steady fields.

Displacement current:

Suppose we add unknown of to 1

divergence, Taking

The solution for
$$\vec{G}$$
 is obtained as $\vec{G} = \frac{\partial \vec{D}}{\partial F}$

The sesults from turne varying displacement flux density Maxwell formed it as displacement current density

We have already met other two current densities

Concluction current density (motion of charge in the region by xoro net charge density)

To E

Convection current density.

The region of volume charge density)

In a non conclucting medium, where $S_{V}=0 \Rightarrow J=0$, $\nabla xH = \frac{\partial J}{\partial t}$ if J=0

Total displacement current existing any given surface, $\mathcal{I}_{d} = \int \mathcal{I}_{d} \cdot ds + \int \frac{\partial \mathcal{I}}{\partial t} \cdot ds$

A. C. L. for Time varying conditions: $\int (\nabla x + \vec{t}) \cdot d\vec{s} = \int \vec{s} \cdot d\vec{s} + \int \frac{\partial \vec{b}}{\partial t} \cdot d\vec{s}$ Apply stokes! Theorem $\int \vec{t} \cdot d\vec{t} = \vec{s} + \vec{t} d = \vec{s} + \vec{t} + \int \frac{\partial \vec{b}}{\partial t} \cdot d\vec{s}$

2 b) =
$$3 \times 10^{-5} \text{H/m}$$
 $6 = 0$ $6 \times 10^{-10} \text{F/m}$ $6 = 0$ $6 \times 10^{-10} \text{F/m}$ $6 = 0$ $6 \times 10^{-10} \text{F/m}$ 6×10^{-10}

$$\vec{\nabla} \times \vec{E} = \frac{\vec{D}}{\epsilon} = \frac{2\beta \cos (10^{10} t - \beta t)}{1.4 \times 10^{10} \times 10^{10}} \vec{\Delta}_{3}$$

$$= 1.66 \beta \cos (10^{10} t - \beta t) \vec{\Delta}_{3} \text{ V/m}$$

$$\vec{\nabla} \times \vec{E} = \int_{0}^{\infty} \vec{\Delta}_{4} \vec{\Delta}_{3} \vec{\Delta}_{4} \vec{\Delta}_{5} \vec{$$

Now, $\vec{D} = \vec{E}$

3 a) Wave equation: for Good Conductors and Skin effect
$$\nabla^2 \vec{E_S} = -\vec{v}^2 \vec{E_S} - \vec{v}$$

From Haxwell's equations,

$$\overrightarrow{\nabla} \times \overrightarrow{E_{S}} = -j\omega\mu \overrightarrow{H_{S}}$$

$$\overrightarrow{\nabla} \times \overrightarrow{F_{S}} = -j\omega\mu \overrightarrow{\nabla} \times \overrightarrow{H_{S}}$$

$$\overrightarrow{\nabla} \times \overrightarrow{F_{S}} = -j\omega\mu \overrightarrow{\nabla} \times \overrightarrow{H_{S}}$$

$$\overrightarrow{\nabla} \times \overrightarrow{\nabla} \times \overrightarrow{E_{S}} = -j\omega\mu \int \sigma \overrightarrow{E_{S}} + j\omega\varepsilon \overrightarrow{E_{S}}$$

$$\overrightarrow{\nabla} \times \overrightarrow{\nabla} \times \overrightarrow{E_{S}} = -j\omega\mu \int \sigma \overrightarrow{E_{S}} + j\omega\varepsilon \overrightarrow{E_{S}}$$

$$-\nabla^{2} \overrightarrow{E_{S}} = -j\omega\mu \sigma \overrightarrow{E_{S}} + \omega^{2} \mu\varepsilon \overrightarrow{E_{S}}$$

$$\nabla^2 E_S^{\dagger} = -\left(-j\omega\mu\sigma E_S^{\dagger} + \left(\omega^2\mu E\right)E_S^{\dagger}\right)$$

$$\pm j\vec{r} = \pm \sqrt{j\omega\mu} 6 - \omega^2 \mu \varepsilon = \pm \sqrt{j\omega\mu} 6 + j^2 \omega^2 \mu \varepsilon$$

$$j = \sqrt{(j\omega)\mu\epsilon \left[\frac{\sigma}{\omega\epsilon j} + 1\right]}$$

$$\int_{\mathcal{J}} = \int_{\mathcal{U}} \omega \int_{\mathcal{U}} \left[1 - \int_{\mathcal{U}} \frac{\delta}{\omega \varepsilon} \right] \qquad (60)$$

$$\frac{G}{w\epsilon} > 1$$

$$j = j w \sqrt{\mu \epsilon^2} \sqrt{1 - j \frac{G}{w\epsilon}}$$

$$j = \sqrt{\frac{\omega_{\mu} \sigma}{a}} + j \sqrt{\frac{\omega_{\mu} \sigma}{a}} = \alpha + j \beta$$

$$d = b = \sqrt{\frac{\omega \mu \sigma}{a}} = \sqrt{\pi f \mu \sigma}$$

$$\int_{\xi'-j\xi''}^{\mu} \frac{\mu}{\xi'-j\xi''} = \int_{\xi'-j\xi''}^{\mu} \frac{\mu}{\xi'-j\xi''}$$

$$\eta = \int \frac{\mu}{\epsilon' + \frac{\sigma}{i\omega}} = \int \frac{j\omega\mu}{\sigma + j\omega\epsilon'}$$

$$= \sqrt{\frac{\mu}{\varepsilon'(1-j\frac{\varepsilon''}{\varepsilon'})}} = \sqrt{\frac{\mu}{\varepsilon'(1-j\frac{\sigma}{w\varepsilon'})}}$$

$$\vec{E} = \vec{E}_{S} e^{j\omega t}$$

$$\vec{E} = \left(\vec{E}_{NO} e^{-j\gamma Z} j\omega t + \vec{E}_{NO} e^{-j\gamma Z} j\omega t\right) \vec{a}_{N}$$

Consider only forward ware

$$\vec{E} = \vec{E}_{x0} e^{-d^2} \cos(\omega t - \beta^2) \vec{a}_x$$

$$H = \frac{F_{NO}}{e} e^{-d^2} \cos(\omega t - \beta^2) = \frac{1}{171} \frac{F_{NO}}{e^{-\Delta^2}} \cos(\omega t - \beta^2) = \frac{1}{171} \frac{F_{NO}}{e^{-\Delta^2}} = \frac{1}{1$$

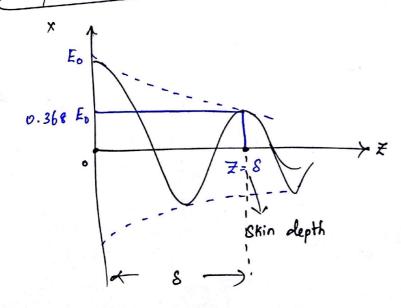
$$H = \frac{E_{NO}}{\sqrt{\frac{\omega \mu}{\delta}}} e^{-d^{2} + \frac{1}{2}} \cos \left(\omega t - \beta^{2} - 4s\right) = \frac{1}{\sqrt{\frac{\omega \mu}{\delta}}}$$

As \vec{F} (or \vec{H}) travels in a conducting medium, it amplitude is affenuated by a factor \vec{e} $\alpha \vec{E}$.

$$\sqrt{S=1}$$

$$S = \frac{1}{\sqrt{\pi + \mu \sigma}}$$

Skin depth is the measure of the depth to which an EM wave can penetrate the medium



for good conductors)
$$d = \beta = \frac{1}{8} = \sqrt{11} f_{\mu\sigma}$$

$$\vec{F}$$
: $\vec{F}_{no} = \begin{pmatrix} -\alpha \\ \alpha \end{pmatrix} \cos \left(\omega t - \beta \\ \vec{z} \right) = \begin{pmatrix} -\alpha \\ \alpha \end{pmatrix}$

$$\vec{F} = E_{xx} e^{-\frac{7}{8}/g} \cos \left(wt - \frac{7}{8}\right) \vec{a}_{x}$$
 \forall \forall m

$$\vec{H} = \frac{\vec{E}_{NO}}{\eta} = \frac{-\frac{7}{8}}{8} \cos \left(\omega t - \frac{7}{8}\right) \vec{a}_{y}$$

$$= \frac{E\pi o}{\left(\frac{\sqrt{2}}{8\sigma}\right)} \frac{-\frac{7}{8}}{e} \cos\left(\omega t - \frac{Z}{8}\right) \frac{\partial}{\partial y}$$

$$\vec{H} = \frac{E_{xx}}{\sqrt{2}} 8\sigma e^{-\frac{Z}{8}} \cos \left(\omega t - \frac{Z}{8} - \frac{\pi}{4}\right) \alpha \vec{y} / A/m$$

Solution. We first evaluate the loss tangent, using the given data:

3 b)

$$\frac{\sigma}{\omega \epsilon'} = \frac{4}{(2\pi \times 10^6)(81)(8.85 \times 10^{-12})} = 8.9 \times 10^2 \gg 1$$

Seawater is therefore a good conductor at 1 MHz (and at frequencies lower than this). The skin depth is

$$\delta = \frac{1}{\sqrt{\pi f \mu \sigma}} = \frac{1}{\sqrt{(\pi \times 10^6)(4\pi \times 10^{-7})(4)}} = 0.25 \text{ m} = 25 \text{ cm}$$

Now

$$\lambda = 2\pi \delta = 1.6 \text{ m}$$

and

$$v_p = \omega \delta = (2\pi \times 10^6)(0.25) = 1.6 \times 10^6 \text{ m/sec}$$

Poynting's theorem & Wave power:

Poynting's theorem.

It states that the not power flowing out of a given volume is equal to the time rate of decrease in Stored energy within the volume minus conduction losses.

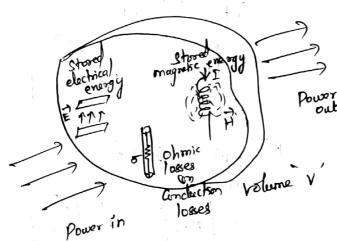


Fig. Illustraturo of poucer balance for EM fields.

Maxwell's equations

$$\vec{\nabla} \times \vec{E} = - \mu \frac{\partial \vec{H}}{\partial L}$$

$$\vec{\nabla} \times \vec{B} = 0$$

$$\vec{\nabla} \times \vec{H} = \sigma \vec{E} + E \partial \vec{E}$$

Vector identity: ♥, (로xガ) = ਜ. ਰxヹ - ヹ. ਰxमें

Apply Marwell's equations isto this vector identity, V. (Exi) = H. HOH - E. [OE + EDE]

$$\vec{\nabla}_{o} (\vec{\xi} \times \vec{h}) = -\mu \vec{h}_{o} \frac{\partial \vec{h}}{\partial t} - \sigma \vec{\epsilon}^{2} - \epsilon \vec{\xi} \cdot \frac{\partial \vec{\xi}}{\partial t}$$

$$\vec{\nabla} \cdot (\vec{E}_{XH}) = -\delta \vec{E}^2 - \epsilon \vec{E} \cdot \frac{\partial \vec{E}}{\partial t} - \mu \cdot \vec{H} \cdot \frac{\partial \vec{H}}{\partial t}$$

$$E \cdot \frac{\partial E}{\partial t} = ?$$
 $\frac{\partial E^2}{\partial t} = 2 E \cdot \frac{\partial E}{\partial t}$

$$= \int_{\overline{\partial t}} \frac{\partial \vec{t}}{\partial t} = \int_{\overline{\partial t}} \frac{\partial \vec{t}}{\partial t}$$

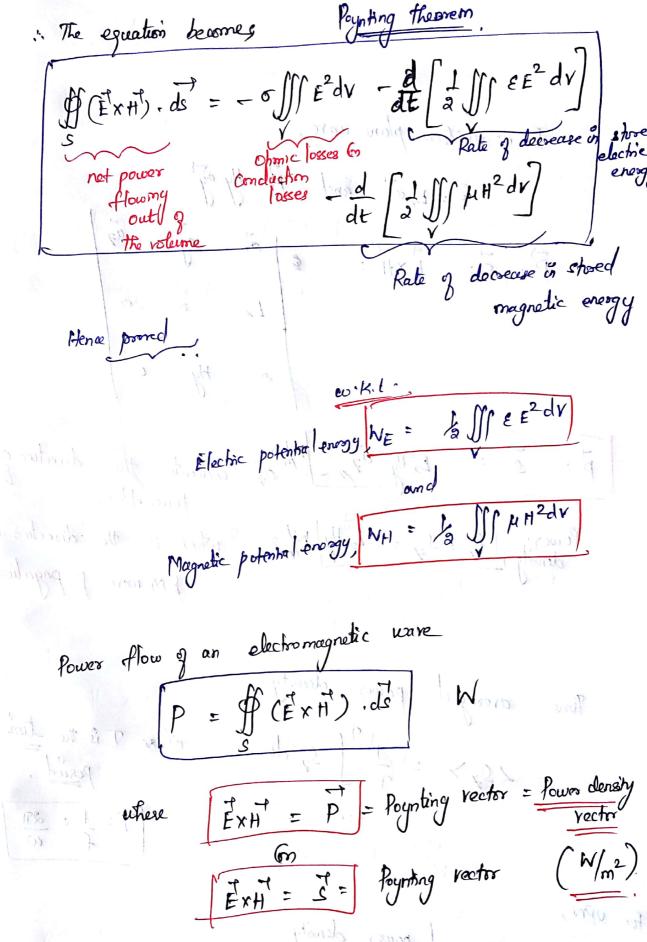
$$\frac{\partial H^2}{\partial t} = 2H^2 \cdot \frac{\partial H^2}{\partial t}$$

$$=) \int_{H}^{H} \frac{\partial H}{\partial t} = \frac{1}{2} \frac{\partial H^2}{\partial t}.$$

$$\nabla \cdot (\vec{E} \times \vec{H}) = -\sigma \vec{E}^2 - 1 \cdot \vec{E} \cdot \vec{\partial} \vec{E}^2 - 1 \cdot \vec{D} \cdot \vec{\partial} \vec{E}^2$$

Integrating over the given volume,

Divergence theosem,
$$\iint (\vec{p}. \vec{A}) dv = \iint \vec{A} \cdot d\vec{s}$$



Sport Sport

Front

Pront

= Dafoont. Sysz

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We now obtain the exact relation ship by
$$40 \rightarrow 0$$
.

$$\left(\frac{\partial m}{\partial x} + \frac{\partial ny}{\partial y} + \frac{\partial nz}{\partial z}\right) : \frac{\partial^2 f}{\partial y} \cdot \frac{\partial f}{\partial z} : \frac{\partial g}{\partial y}$$

$$\left(\frac{\partial m}{\partial x} + \frac{\partial ny}{\partial y} + \frac{\partial m}{\partial z}\right) : \lim_{n \to \infty} \frac{\partial^2 f}{\partial x} \cdot \frac{\partial f}{\partial x}$$

$$\left(\frac{\partial m}{\partial x} + \frac{\partial ny}{\partial y} + \frac{\partial m}{\partial z}\right) : \lim_{n \to \infty} \frac{\partial^2 f}{\partial x} \cdot \frac{\partial f}{\partial x}$$

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$$\left(\frac{\partial m}{\partial x} + \frac{\partial ny}{\partial y} + \frac{\partial m}{\partial z}\right) : \lim_{n \to \infty} \frac{\partial f}{\partial x} \cdot \frac{\partial f}{\partial x}$$

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$$\left(\frac{\partial m}{\partial x} + \frac{\partial ny}{\partial y} + \frac{\partial m}{\partial z}\right) : \lim_{n \to \infty} \frac{\partial f}{\partial x} \cdot \frac{\partial f}{\partial x}$$

$$\left(\frac{\partial m}{\partial x} + \frac{\partial ny}{\partial z} + \frac{\partial m}{\partial z}\right) : \lim_{n \to \infty} \frac{\partial f}{\partial x} \cdot \frac{\partial f}{\partial x}$$

$$\left(\frac{\partial m}{\partial x} + \frac{\partial ny}{\partial z} + \frac{\partial m}{\partial z}\right) : \lim_{n \to \infty} \frac{\partial f}{\partial x} \cdot \frac{\partial f}{\partial x}$$

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$$\left(\frac{\partial m}{\partial x} + \frac{\partial ny}{\partial z} + \frac{\partial m}{\partial z}\right) : \lim_{n \to \infty} \frac{\partial f}{\partial z} \cdot \frac{\partial m}{\partial z}$$

$$\left(\frac{\partial m}{\partial x} + \frac{\partial ny}{\partial z} + \frac{\partial m}{\partial z}\right) : \lim_{n \to \infty} \frac{\partial f}{\partial z}$$

Divergence of
$$p = \text{div } p =$$

Divergence of the rection flow density of is the outflow of flow form a small closed surface per writ volume as the volume Strinks to Zero-

div
$$p' := \frac{\partial Dn d}{\partial n} \frac{\partial Dy}{\partial 2} \frac{\partial Dz}{\partial 2}$$
 Rectangular

$$\int \frac{\partial Dn d}{\partial n} \frac{\partial Dy}{\partial 2} \frac{\partial Dz}{\partial 2} = \frac{\partial Dz}{\partial 2} \frac{\partial Dz}{\partial 2}$$

Captindrical

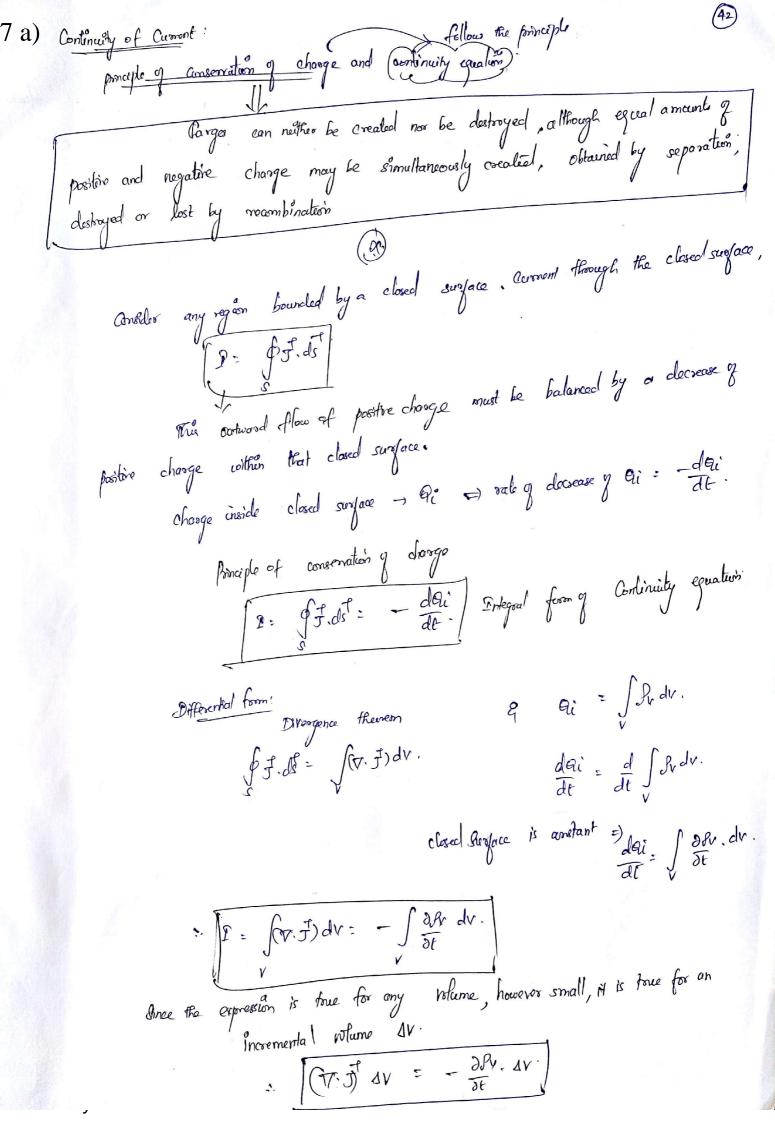
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MAXWELL'S FIRST EQUATION OF ELECTROSTATICS: ("Definition" of divergence) 1) div D= lim & D. ds 2) du D: $\frac{\partial Dx}{\partial x} + \frac{\partial Dy}{\partial y} + \frac{\partial Dz}{\partial z}$ (Result of applying the differential volume element (In Rectangular co-ordinates) chut = R Grows's law offer bearing any closed response SB.J.: Q Charge enclosed Gauss' law per unit volume,

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As the volume shows to xero, First of Maxwell's four equations The electric flux per cerit volume leaving a Vanishingly small volume and Maxwells Gauss law - I & B.ds = Q = Sp.dr.

Integral form y Marwell's forst equalion



TV. J = - 284 Point from of Continuity equaltion. Oursend or charge per second almosting from a small volume per with volume to equal to the time rate of decrease of charge per with volume at every point.

$$J_{v} = \nabla \cdot \vec{D} = \frac{1}{x^{2}} \frac{\partial}{\partial x} (x^{2} D_{r}) + o + o$$

$$T = 0.06$$

$$T = 5x^{2} a_{r}$$

$$= \frac{1}{x^{2}} \frac{\partial}{\partial x} (5x^{4}) m$$

$$= \frac{1}{x^{2}} \cdot a_{0}x^{3} m$$

Sv = 20r m

= 1.2 m e/m 32

for force por wit test charge at P. to Move the fest charge against E, as require force equal & opposite to the field. oreguines expend energy (on) do work, of are wish to Nove a charge Q, a distance \overline{dL} in an electric field \overline{E}^{\dagger} . Force on a clue to FE = QE. Asia arrises from electric field. The component of this force in the direction of FEL = FE (a) cunit vector in the direction g de Scanned by CamScanner

moring a point change in an electic field:

FEL = QE aL. The force we must apply is equal and opposite to Fer. Fappl = - QE.ac. Frengy expended = force x distance Differential work done by an external source morning change Q is aw = - QE, at de due - GE. di Hook required to more a charge or finite distance, N= - Q Fidi Anital par must be specified Change is assumed at rest of both it initial & final position $8 \ b) \frac{}{\text{We are given the nonuniform field}}$

$$\mathbf{E} = y\mathbf{a}_x + x\mathbf{a}_y + 2\mathbf{a}_z$$

and we are asked to determine the work expended in carrying 2C from B(1, 0, 1) to A(0.8, 0.6, 1) along the shorter arc of the circle

$$x^2 + y^2 = 1$$
 $z = 1$

Solution. We use $W = -Q \int_{R}^{A} \mathbf{E} \cdot d\mathbf{L}$, where **E** is not necessarily constant. Working in rectangular coordinates, the differential path $d\mathbf{L}$ is $dx\mathbf{a}_x + dy\mathbf{a}_y + dz\mathbf{a}_z$, and the integral becomes

$$W = -Q \int_{B}^{A} \mathbf{E} \cdot d\mathbf{L}$$

$$= -2 \int_{B}^{A} (y\mathbf{a}_{x} + x\mathbf{a}_{y} + 2\mathbf{a}_{z}) \cdot (dx \, \mathbf{a}_{x} + dy \, \mathbf{a}_{y} + dz \, \mathbf{a}_{z})$$

$$= -2 \int_{1}^{0.8} y \, dx - 2 \int_{0}^{0.6} x \, dy - 4 \int_{1}^{1} dz$$

where the limits on the integrals have been chosen to agree with the initial and final values of the appropriate variable of integration. Using the equation of the circular path (and selecting the sign of the radical which is correct for the quadrant involved), we have

$$W = -2 \int_{1}^{0.8} \sqrt{1 - x^{2}} \, dx - 2 \int_{0}^{0.6} \sqrt{1 - y^{2}} \, dy - 0$$

$$= -\left[x\sqrt{1 - x^{2}} + \sin^{-1}x\right]_{1}^{0.8} - \left[y\sqrt{1 - y^{2}} + \sin^{-1}y\right]_{0}^{0.6}$$

$$= -(0.48 + 0.927 - 0 - 1.571) - (0.48 + 0.644 - 0 - 0)$$

$$= -0.96 \,\text{J}$$

and a both when a land

Marwell's equations:

$$\vec{\nabla} \cdot \vec{D} = 0 \qquad \Rightarrow \vec{\nabla} \cdot \vec{E} = 0 \qquad \Rightarrow 0$$

$$\vec{\nabla} \times \vec{E} = -\mu \frac{\partial H^{\dagger}}{\partial t} \qquad \Rightarrow \vec{\nabla} \times \vec{E} = -\mu \frac{\partial H^{\dagger}}{\partial t} \Rightarrow 0$$

$$\vec{\nabla} \cdot \vec{B} = 0 \qquad \Rightarrow \vec{\nabla} \cdot \vec{H} = 0 \qquad \Rightarrow 0$$

$$\vec{\nabla} \times \vec{H} = 0 \qquad \Rightarrow \vec{\nabla} \times \vec{H} = 0 \qquad \Rightarrow 0$$

$$\vec{\nabla} \times \vec{H} = 0 \qquad \Rightarrow \vec{\nabla} \times \vec{H} = 0 \qquad \Rightarrow 0$$

Vector TX TX E = F(F. E) - VE

$$\vec{\nabla}(\vec{\nabla},\vec{k}) - \vec{\nabla}\vec{E}^{\dagger} = -\mu \frac{\partial}{\partial t} (\vec{\nabla} \times \vec{A})$$
Apply equation $\vec{\Phi}$

$$-\nabla^2 \vec{t} = -\mu \frac{\partial}{\partial t} \left[\vec{\sigma} \vec{E} + \vec{E} \frac{\partial \vec{E}}{\partial t} \right]$$

$$-\nabla^{2}\vec{E} = -\mu\sigma \frac{\partial \vec{E}}{\partial t} - \mu\varepsilon \frac{\partial \vec{E}}{\partial t^{2}}$$

$$\nabla^2 \vec{E}^{\dagger} = \mu \sigma \frac{\partial \vec{E}^{\dagger}}{\partial t} + \mu \varepsilon \frac{\partial^2 \vec{E}^{\dagger}}{\partial t^2}$$

$$\frac{\partial^2 \vec{E}}{\partial z^2} = \mu \sigma \frac{\partial \vec{E}}{\partial t} + \mu \vec{E} \frac{\partial^2 \vec{E}}{\partial z^2} = \frac{\partial^2 \vec{E}}{\partial z^2}$$

$$\frac{\partial^2 \vec{E}}{\partial z^2} = \mu \sigma \frac{\partial \vec{E}}{\partial t} + \mu \vec{E} \frac{\partial^2 \vec{E}}{\partial z^2}$$

$$\frac{\partial^2 \vec{E}}{\partial z^2} = \mu \sigma \frac{\partial \vec{E}}{\partial z} + \mu \vec{E} \frac{\partial^2 \vec{E}}{\partial z^2}$$

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$$\frac{\partial \vec{E}}{\partial z} = \mu \sigma \frac{\partial \vec{E}}{\partial z} + \mu \vec{E} \frac{\partial \vec{E}}{\partial$$

Similarly,

General War equation of the the medic considered

$$\frac{1}{2} \frac{1}{2} \frac{1}$$

$$-VH = -\sigma \cdot \mu \frac{\partial H}{\partial t} - \epsilon \mu \frac{\partial^2 H}{\partial t^2}$$

$$\frac{\partial^2 H^{\dagger}}{\partial z^2} = \frac{\mu \sigma}{\partial t} \frac{\partial H^{\dagger}}{\partial t} + \frac{\mu \varepsilon}{\partial t} \frac{\partial^2 H^{\dagger}}{\partial t^2} \Rightarrow \text{Genoval wave equation}$$

$$\frac{\partial^2 H^{\dagger}}{\partial z^2} = \frac{\mu \sigma}{\partial t} \frac{\partial H^{\dagger}}{\partial t} + \frac{\partial^2 H^{\dagger}}{\partial t} \Rightarrow \text{Genoval wave equation}$$

$$\frac{\partial^2 H^{\dagger}}{\partial z^2} = \frac{\mu \sigma}{\partial t} \frac{\partial H^{\dagger}}{\partial t} + \frac{\mu \varepsilon}{\partial t} \frac{\partial^2 H^{\dagger}}{\partial t} \Rightarrow \text{Genoval wave equation}$$

$$\frac{\partial^2 H^{\dagger}}{\partial z^2} = \frac{\mu \sigma}{\partial t} \frac{\partial H^{\dagger}}{\partial t} + \frac{\mu \varepsilon}{\partial t} \frac{\partial^2 H^{\dagger}}{\partial t} \Rightarrow \text{Genoval wave equation}$$

$$\frac{\partial^2 H^{\dagger}}{\partial z^2} = \frac{\mu \sigma}{\partial t} \frac{\partial H^{\dagger}}{\partial t} + \frac{\mu \varepsilon}{\partial t} \frac{\partial^2 H^{\dagger}}{\partial t} \Rightarrow \text{Genoval wave equation}$$

$$\frac{\partial^2 H^{\dagger}}{\partial z^2} = \frac{\mu \sigma}{\partial t} \frac{\partial H^{\dagger}}{\partial t} + \frac{\mu \varepsilon}{\partial t} \frac{\partial^2 H^{\dagger}}{\partial t} \Rightarrow \text{Genoval wave equation}$$

wave equation for free space for
$$\frac{1}{8}$$
 $\frac{\partial^2 E^{\dagger}}{\partial t^2} = \frac{1}{40\%} \frac{\partial^2 E^{\dagger}}{\partial t^2}$

Wave equation for free pare for H-field.

(b) =
$$\frac{3^2H^7}{3t^2} = \frac{1}{\mu_0 \epsilon_0} \frac{3^2H^7}{3t^2}$$
 (or $\frac{3^2H^7}{3t^2} = \frac{1}{\mu_0 \epsilon_0} \frac{3^2H^7}{3t^2} = \frac{1}$

Have equations for force space can be written as
$$\frac{\partial^2 \vec{E}'}{\partial \vec{x}^2} = \frac{1}{\sqrt{p^2}} \frac{\partial^2 \vec{E}'}{\partial t^2} \left(v_D \right) \frac{\partial^2 \vec{E}'}{\partial t^2} = \frac{\sqrt{p^2}}{\sqrt{p^2}} \frac{\partial^2 \vec{E}'}{\partial t^2}$$
and

and
$$\frac{\partial^2 \vec{H}}{\partial z^2} = \frac{1}{y_p^2} \frac{\partial^2 \vec{H}}{\partial t^2} \qquad \text{(on)} \qquad \frac{\partial^2 \vec{H}}{\partial t^2} = y_p^2 \frac{\partial^2 \vec{H}}{\partial z^2}$$