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Internal Assessment Test 1 – Sept. 2017

Sub:	Fluid Mechanics				Sub Code:	15CV33	Branch:	Civil
Date:	20/09/2017	Duration:	90 min	Max Marks:	50	Sem / Sec:	III – A & B	OBE

Answer all questions

MARKS

	MARKS	CO	RBT
1 (a) Define the terms – a) Surface tension b) Specific volume.	[04]	CO1	L1
(b) A cube of 0.3m sides and weight 30 N slides down an inclined plane sloped at 30° to the horizontal. The plane is covered by an oil of viscosity 2.3×10^{-3} Pas with 0.03mm thickness. Determine the velocity with which the cube slides.	[06]	CO1	L2
2 (a) Derive an expression for capillary rise between two parallel plates.	[04]	CO1	L2
(b) State and prove Pascal's Law.	[06]	CO2	L2
3 (a) A U-tube differential manometer is attached to 2 points A and B in a horizontal pipeline carrying water, 5m apart. The pressure at A is 0.07N/mm^2 and pressure head is 150mm of Hg. Find the Hg level difference in the manometer.	[05]	CO2	L3
(b) The water is flowing at the rate of 60lps through a tapering pipe of length 500 mm, having diameter 400mm at the upper end and 200mm at the lower end. The pipe has a slope of 1 in 40. Find the pressure at the lower end, if the pressure at the upper end is 0.24N/mm^2 .	[05]	CO4	L3

P. T. O

- 4 (a) From Euler's equation, derive the Bernoulli's equation of motion along a stream tube. List the assumptions for Bernoulli's equation [10]

CO4	1.2
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- 5 (a) What is a notch? Derive an expression for discharge through a V – Notch. [06]

CO5	1.2
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- (b) Write short notes on a) End contractions, b) Cipolletti Notch [04]

CO5	1.1
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All the Best

Sign of CI

Sign of CCI

Sign of HOD

Surface Tension

It is defined as tensile force acting on the surface of a liquid in contact with a gas or on the surface b/w 2 immiscible liquid such that the contact surface behaves like a membrane under tension.

The magnitude of this is

$$\frac{\text{force}}{\text{unit length of the free surface}} = \frac{\text{Surface Energy}}{\text{Unit area}}$$

Symbol - σ

MKS - kgf/m
SI - N/m

$1 \text{ N} = 9.81 \text{ kgf}$

4) Specific Volume ρ_m

It is defined as the volume of a fluid occupied by a unit mass or volume per unit mass of a fluid is called Specific volume..

It is denoted by v_m

$$\text{Specific volume} = \frac{\text{Volume of the fluid}}{\text{Mass of the fluid}}$$

Its unit is m^3/kg (meter³/Kilogram)

Example ρ_m Specific volume of water = $\frac{1}{\rho}$

$$= \frac{1}{1000} = 0.001 m^3/kg$$

A cube 0.3m sides and weight 30N slides down an inclined plane sloped at 30° to the horizontal. The plane is covered by an oil of viscosity 2.3×10^{-3} Pa.s. with 0.03mm thickness. Determine the velocity with which the cube slides?

Given

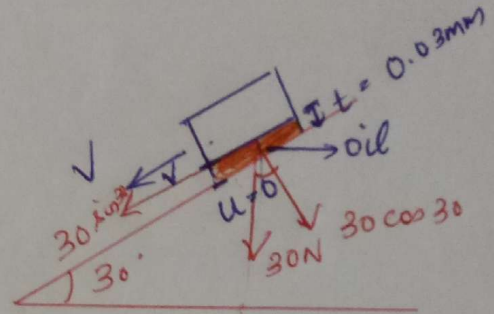
$$\text{side, } a = 0.3\text{m}$$

$$\text{Wt, } W = 30\text{N}$$

$$\theta = 30^\circ$$

$$\mu = 2.3 \times 10^{-3} \text{Ns/m}^2$$

$$t = 0.03\text{mm} = 0.03 \times 10^{-3} \text{m}$$



By Newton's Law of Viscosity

$$\tau = \mu \frac{du}{dy}$$

$$\tau = \frac{F}{A} = \frac{30 \sin 30}{0.3 \times 0.3} \quad \begin{array}{l} \text{[Weight along the} \\ \text{inclined plane]} \\ \text{[Contact surface} \\ \text{area]} \end{array}$$

$$= 166.67 \text{ N/m}^2$$

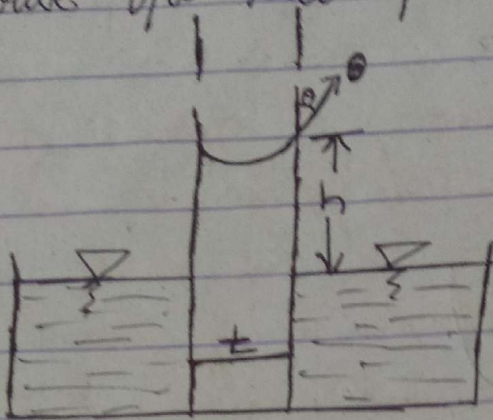
$$\mu \frac{du}{dy} = \frac{\mu (v - u)}{t} = \frac{2.3 \times 10^{-3} (v - 0)}{0.03 \times 10^{-3}}$$

$$\therefore 166.67 = \frac{2.3 \times 10^{-3} v}{0.03 \times 10^{-3}}$$

$u = 0$ [stationary inclined plane]

$$v = 2.17 \text{ m/s}$$

Capillary rise b/w two parallel vertical plates :-



let t be the distance b/w the two parallel plate, let L be the length of the plate in perpendicular direction.

F_1 = Force due to surface tension

$$F_1 = \sigma \cos \theta \times \text{circumference}$$

$$F_1 = \sigma \cos \theta \times 2L$$

F_2 = Force due to the liquid column of height h

$$F_2 = mg$$

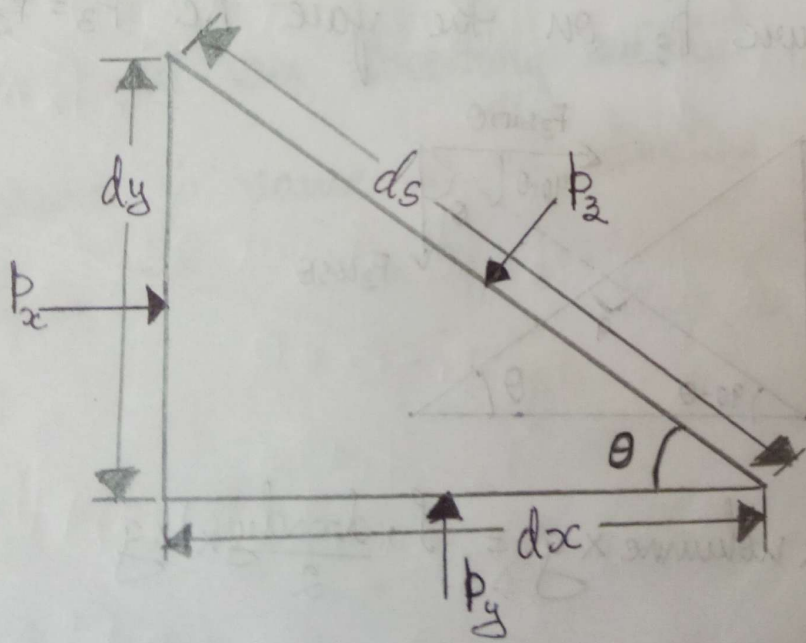
$$= \rho \times \text{volume} \times g$$

$$= \rho \times Lth \times g$$

$$\sigma \cos \theta \times 2L = \rho Lthg$$

$$h = \frac{2\sigma \cos \theta}{\rho g t}$$

Pascal's law :- It states that the pressure or intensity of pressure in a static fluid is equal in all directions is called Pascal's law.



Consider an arbitrary fluid Element of wedge shape of fluid mass at rest. The fluid Element of very small dimension dx, dy, dz and the width of the Element \perp to plane of the paper be unity. Let P_x, P_y and P_z be the intensity of pressure acting on the faces AB, BC, CA respectively. Let angle be θ at C.

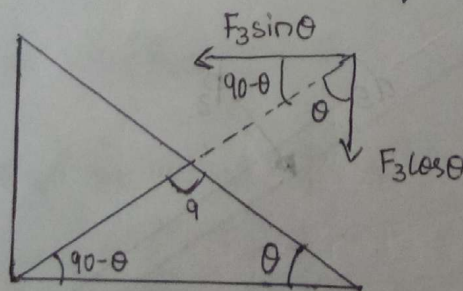
The force acting on the wedge are forces due to pressure P_x, P_y, P_z acting normal to the surface. The second force is weight of the fluid Element.

The forces are calculated below :-

Force due to pressure P_x on the face AB $F_1 = P_x dy \times 1$

Force due to pressure P_y on the face BC $F_2 = P_y dy \times 1$

Force due to pressure P_z on the face AC $F_3 = P_z ds \times 1$



$$F_4 = mg = \rho \times \text{volume} \times g = \rho \times \frac{dx \times dy \times 1}{2} \times g$$

for fluid at rest $\Sigma F_x = 0$

$$F_1 - F_3 \sin \theta = 0$$

$$P_x dy - P_3 ds \sin \theta = 0$$

Substitute $dy = ds \sin \theta$

$$P_x ds \sin \theta - P_3 ds \sin \theta = 0$$

$$\boxed{P_x = P_3} \quad (1)$$

||| resolving forces along y $\Sigma F_y = 0$

$$F_2 - F_4 - F_3 \cos \theta = 0$$

$$P_y dy - \frac{\rho dx dy g}{2} - P_3 ds \cos \theta = 0$$

$$\boxed{P_y = P_3} \quad (2)$$

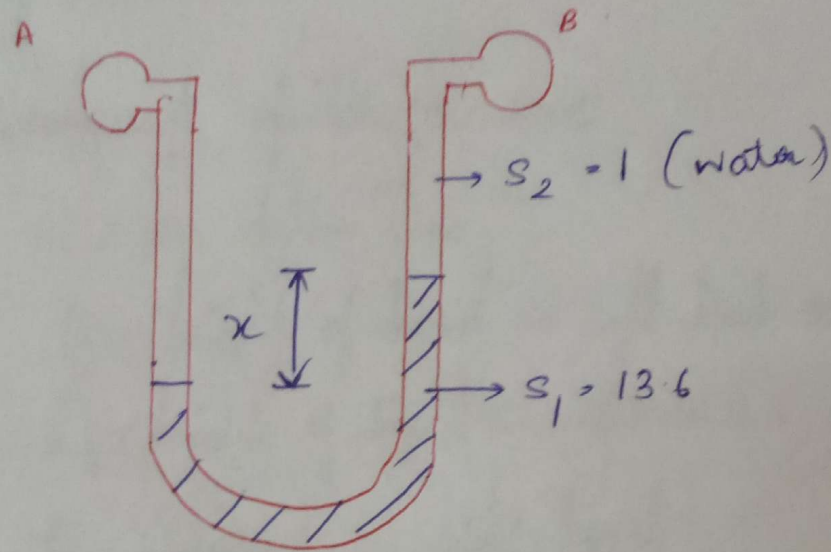
[$F_4 = 0$, since dx & dy were very small and their product can be neglected, $dy = ds \cos \theta$]

Equating (1) and (2)

$$P_3 = P_y = P_x$$

Since θ is an arbitrary constant, the Equation proves that pressure is same in all direction at a point in a static liquid.

A U-tube differential manometer is attached to 2 points A and B in a horizontal pipeline carrying water, 5 m apart. The pressure at A is 0.07 N/mm^2 and pressure head is 150 mm of Hg. Find the Hg level difference in the manometer.



Given

$$P_A = 0.07 \text{ N/mm}^2 = 0.07 \times 10^6 \text{ N/m}^2$$

$$P_B = 150 \text{ mm} = 0.15 \text{ m}$$

$$P_{Hg} = 0.15 \times 13.6 \times 1000 \times 9.81 = 20012.4 \text{ N/m}^2$$

$$= 0.02 \times 10^6 \text{ N/m}^2$$

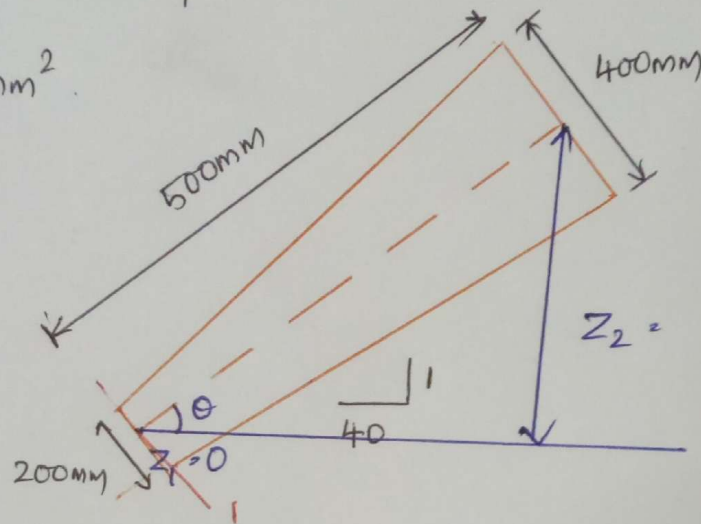
Since $P_A > P_B$, the level of Hg connected to column A will be lower than B.

$$\frac{P_A}{\rho g} - \frac{P_B}{\rho g} = h = x \left(\frac{S_1}{S_2} - 1 \right)$$

$$\frac{(0.07 - 0.02) \times 10^6}{1000 \times 9.81} = x \left(\frac{13.6 - 1}{1} \right)$$

$$x = 0.404 \text{ m}$$

The water is flowing at the rate of 60 lps through a tapering pipe of length 500mm, having diameter 400mm at the upper end and 200mm at the lower end. The pipe has a slope of 1 in 40. Find the pressure at the lower end, if the pressure at the upper end is 0.24 N/mm^2 .



$$P_2 = 0.24 \text{ N/mm}^2$$

When θ is very small

$$\sin \theta = \tan \theta$$

$$z_2 = \frac{1 \times 0.5}{40}$$

$$\text{Datum} = 0.0125 \text{ m}$$

Given

$$\text{Discharge, } Q = 60 \text{ l/s} = 0.06 \text{ m}^3/\text{s}$$

$$L = 500 \text{ mm} = 0.5 \text{ m}$$

$$d_1 = 200 \text{ mm} = 0.2 \text{ m}$$

$$d_2 = 400 \text{ mm} = 0.4 \text{ m}$$

$$A_1 = \frac{\pi}{4} \times 0.2^2 = 0.0314 \text{ m}^2$$

$$A_2 = \frac{\pi}{4} \times 0.4^2 = 0.1256 \text{ m}^2$$

$$V_1 = \frac{Q}{A_1} = 1.91 \text{ m/s}$$

$$V_2 = 0.477 \text{ m/s}$$

$$P_2 = 0.24 \text{ N/mm}^2 = 0.24 \times 10^6 \text{ N/m}^2$$

Applying Bernoulli's Equation at (1) & (2)

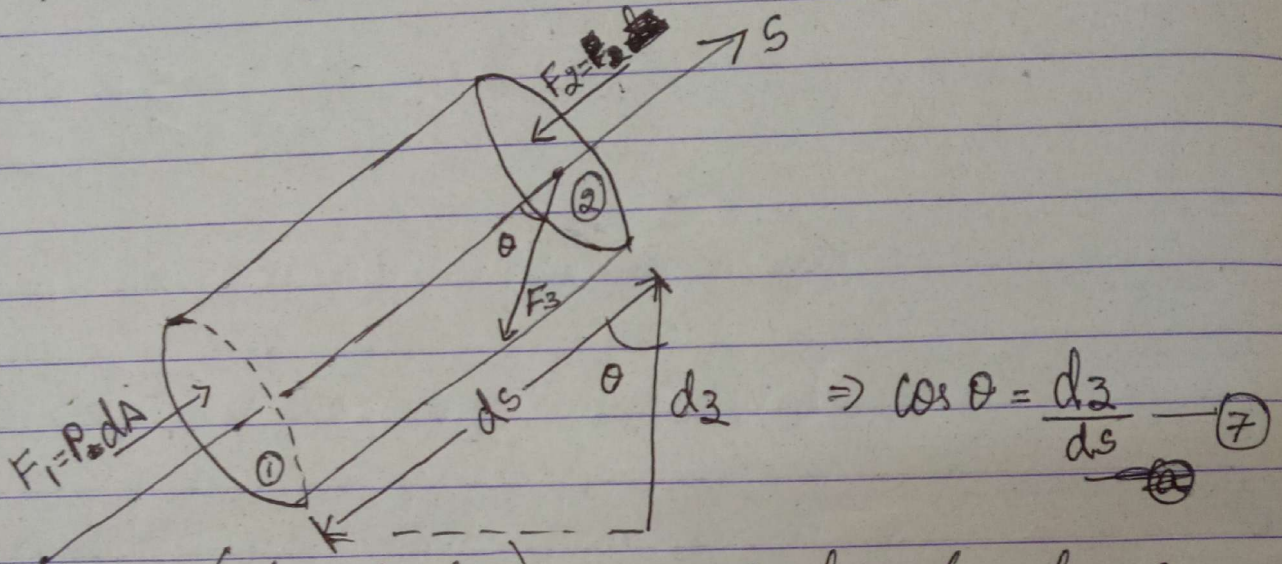
$$\frac{P_1}{\rho g} + \frac{V_1^2}{2g} + z_1 = \frac{P_2}{\rho g} + \frac{V_2^2}{2g} + z_2$$

$$\frac{P_1}{1000 \times 9.81} + \frac{1.91^2}{2 \times 9.81} + 0 = \frac{0.24 \times 10^6}{1000 \times 9.81} + \frac{0.477^2}{2 \times 9.81} + 0.0125$$

$$P_1 = 238412.3395 \text{ N/m}^2$$

Module - 3
Fluid Dynamics

Euler's Equation along a stream line turbine



Euler's Equation (or Euler's Equation) is an Equation of motion in which forces due to gravity and pressure are taken into consideration. This is derived by considering the motion of the fluid Element along a stream line.

Consider a stream line / Stream tube in which flow is taking place in "s" direction. Consider a cylindrical Element of cross-section dA and length ds. The forces acting on a fluid Element are

F_1 be the force due to pressure at section ① = $P_1 dA$ — ①

F_2 be the force due to pressure at section ② = $(P + \frac{dP}{ds}) \times ds \times dA$ — ②

F_3 is the weight of the fluid Element = $m g$

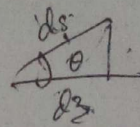
Let ρ be the density of fluid

$$= \rho \times \text{Volume} \times g$$

$$F_3 = \rho \times \left(\frac{\pi}{4} dA \times ds \right) \times g$$

— ③

$$\frac{dv}{dx} = \frac{dv}{dz} \times \frac{dz}{dx} + \frac{dv}{dt}$$



Applying Equilibrium Equation along x-axis $\Sigma F_x = Ma_x$

$$F_1 - F_2 - F_3 \cos \theta = Ma_x$$

where a_x is the acceleration along x-axis = $\frac{dv}{dt}$, where v is the function of s and t . $a_x = \frac{dv}{dt}$, v is function of s and t .

$$\frac{dv}{ds} \times \frac{ds}{dt} + \frac{dv}{dt}$$

for a steady flow, $\frac{dv}{dt} = 0$

$$\frac{ds}{dt} = \frac{ds}{dt} = v \quad (\because s \text{ is only depended on } t)$$

$$a_x = \frac{dv}{ds} \times v + 0$$

Substitute (1), (2), (3), (5) in (4)

$$P dA - (P + \frac{\partial P}{\partial s} ds) dA - \rho (dA ds) g \cos \theta = \rho (dA ds) \times \frac{dv}{ds} \times v$$

$$P - P - \frac{\partial P}{\partial s} ds - \rho ds g \cos \theta = \rho ds \frac{dv}{ds} v$$

Dividing the Equation by $\rho ds g$

$$-\frac{\partial P}{\partial s} \times \frac{1}{\rho g} - \cos \theta = \frac{dv}{ds} \frac{v}{g} \quad \text{--- (6)}$$

replace $\frac{\partial P}{\partial s} = \frac{dP}{ds}$ $\frac{dv}{ds} = \frac{dv}{ds}$ --- (8)

Substitute (8) & (7) in (6)

$$-\frac{dP}{ds} \times \frac{1}{\rho g} - \frac{dz}{ds} = \frac{dv}{ds} \times \frac{v}{g}$$

$$\boxed{0 = + \frac{dP}{\rho g} + dz + \frac{v}{g} dv} \rightarrow \text{in the Euler's Equation}$$

$$\frac{1}{2}mv^2$$

By integrating the Equation.

$$\int \frac{dp}{\rho g} + \int dz + \int \frac{v}{g} dv = 0$$

$$\frac{p}{\rho g} + z + \frac{v^2}{2g} = \text{constant}$$

$\frac{p}{\rho g}$ is the pressure head in meters.

z is the datum or potential head.

$\frac{v^2}{2g}$ is velocity or kinetic head in meters.

$$\text{Energy head} = \frac{\text{Energy}}{\text{weight}} ;$$

$$KE = \frac{1}{2}mv^2$$

$$KH = \frac{1}{2} \frac{mv^2}{mg} = \frac{v^2}{2g}$$

$$Pd H = \frac{Mg z}{mg}$$

$$Pd H = \frac{Mg z}{mg} = z$$

Bernoulli's Equation :

In a steady incompressible flow

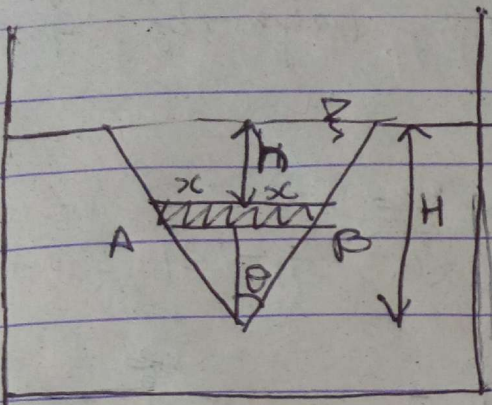
In an ideal incompressible fluid when a flow is steady and continuous, sum of pressure head, KEH and PdH is a constant along a stream line.

$$\frac{p}{\rho g} + z + \frac{v^2}{2g} = \text{constant}$$

Assumptions (for derivation of Bernoulli's eqn)

- 1) The liquid is ideal & incompressible
- 2) the flow is steady & continuous
- 3) The flow is along a streamline (ie) it is one-dimensional
4. vel is uniform over a sectⁿ & is equal to the mean vel.
5. The only forces acting on the fluid are gravity forces & pressure forces.

steady flow of an incompressible



$$dA = AB \times dh$$

$$v = \sqrt{2gh}$$

$$\tan \theta = \frac{x}{(H-h)}$$

$$(H-h) \tan \theta = x$$

$$2(H-h) \tan \theta = 2x = AB$$

$$\therefore dA = 2(H-h) \tan \theta \times dh$$

$$dQ = dA \times v$$

$$dQ = 2 \tan \theta (H-h) \times dh \times \sqrt{2gh}$$

$$\int_0^Q dQ = 2 \tan \theta \sqrt{2g} \int_0^H (H-h) \sqrt{h} \cdot dh$$

$$Q = 2 \tan \theta \sqrt{2g} \left(\frac{Hh^{3/2}}{3/2} - \frac{h^{5/2}}{5/2} \right)_0^H$$

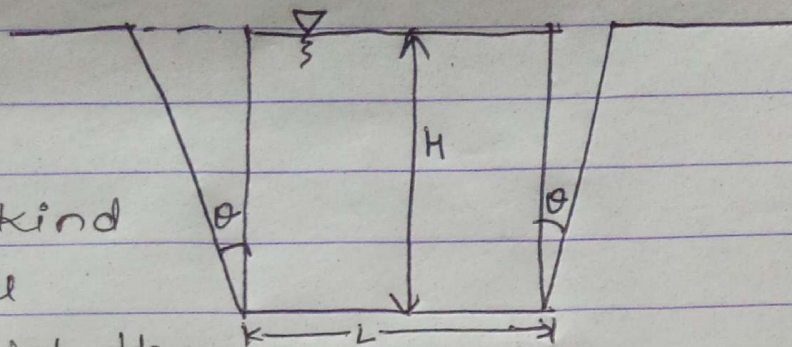
$$Q = 2 \tan \theta \sqrt{2g} \left(\frac{2H^{5/2}}{3} - \frac{2H^{5/2}}{5} \right)$$

$$Q = \frac{8 \tan \theta \sqrt{2g}}{15} H^{5/2}$$

Cipolletti notch

It is a special kind of trapezoidal notch in which the

sides are given as 4 vertical : 1 horizontal.



$$\Rightarrow \frac{2}{3} L \sqrt{2g} H^{3/2} + \frac{8}{15} \sqrt{2g} \tan \theta H^{5/2}$$

$$\tan \theta = \frac{1}{4}$$

$$= \frac{2}{3} L \sqrt{2g} H^{3/2} + \frac{8}{15} \times \frac{1}{4} \sqrt{2g} H^{5/2}$$

$$= \frac{2}{3} \sqrt{2g} H^{3/2} (L + 1/5 H)$$

$$= \frac{2}{3} \sqrt{2g} H^{3/2} (L + 0.2 H) \quad [\text{without end contraction}]$$

With end contraction,

$$Q_{th} = \frac{2}{3} \sqrt{2g} H^{3/2} (L - 0.2 H + 0.2 H)$$

$$Q_{th} = \frac{2}{3} \sqrt{2g} H^{3/2} L$$

$$\left. \begin{array}{l} L \rightarrow L - 0.1 \times 2H \\ L - 0.2H \end{array} \right\}$$