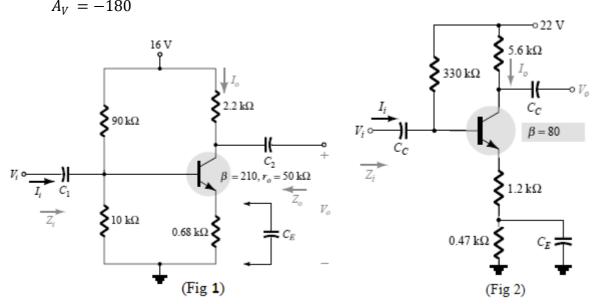
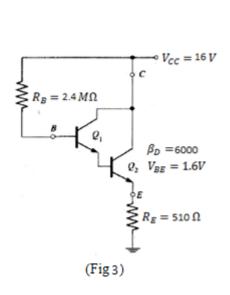


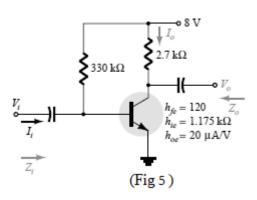


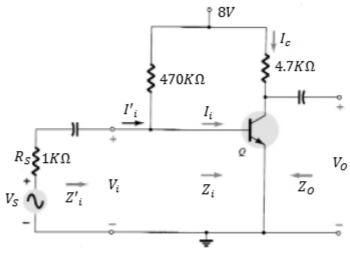
| Internal Assesment Test – I    |               |           |         |            |    |      |     |         |         |  |  |  |
|--------------------------------|---------------|-----------|---------|------------|----|------|-----|---------|---------|--|--|--|
| Sub:                           | ANALOG ELECTR | ONICS     |         |            |    |      |     | Code:   | 15EC32  |  |  |  |
| Date:                          | 18/ 09 / 2017 | Duration: | 90 mins | Max Marks: | 50 | Sem: | III | Branch: | TCE (A) |  |  |  |
| Answer Any FIVE FULL Questions |               |           |         |            |    |      |     |         |         |  |  |  |

|       |  |       | OBE |     |
|-------|--|-------|-----|-----|
|       |  | Marks | CO  | RBT |
| 1     | Derive an expression for input impedance, output impedance, voltage gain and current gain of transistor amplifier using complete hybrid-Model.                     | [10]  | CO1 | L2  |
| 2     | Calculate the following for the network shown in (Fig 1) with and without $C_E$ and compare the voltage gain.<br>(a) $r_e$ (b) $Z_i$ (c) $Z_0$ (d) $A_V$ (e) $A_i$ | [10]  | CO1 | L3  |
| 3     | For the network shown in (Fig 2). Determine $r_e$ , $Z_i$ , $Z_0$ , $A_V$ , $A_i$  | [10]  | CO1 | L3  |
| 4 (a) | Calculate the DC bias voltages and Currents for the given circuit (Fig 3).   | [05]  | CO1 | L3  |
| (b)   | Draw and explain the hybrid- $\pi$ model of transistor in CE configuration mentioning significance of each component in Model.                                     | [05]  | CO2 | L5  |
| 5     | Calculate the input impedance, output impedance, voltage gain and current gain for the given circuit (Fig 4).  | [10]  | CO1 | L3  |
| 6 (a) | Determine the input impedance, output impedance, voltage gain and current gain for the circuit shown below (Fig 5).  | [05]  | CO1 | L3  |
| (b)   | Analyze the $r_e$ parameter model for emitter follower circuit and derive $Z_i$ , $Z_o$ , $A_V$ , $A_i$  | [05]  | CO1 | L4  |
| 7 (a) | Describe the h-parameter model for emitter bias circuit and derive $Z_i$ , $Z_o$ , $A_V$ , $A_i$ using approximate hybrid model.                                   | [05]  | CO1 | L2  |
| (b)   | For the network shown below(Fig 6), determine $V_{CC}$ for a voltage gain of $A_{V} = -180$  | [05]  | CO1 | L3  |

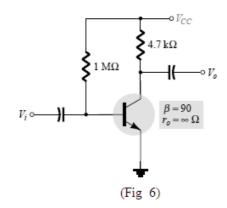








 $h_{fs}=110 \quad h_{is}=1.6K\Omega \quad h_{rs}=2\times 10^{-4} \quad h_{os}=20\frac{\mu A}{V} \label{eq:hfs}$  (Fig 4)



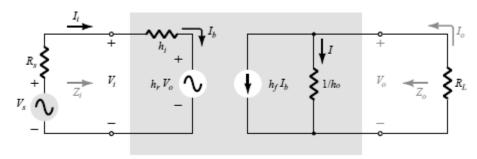
#### **SOLUTION AND SCHEME OF EVALUATION**

## IAT-1: AEC

 Derive an expression for input impedance, output impedance, voltage gain and current gain of transistor amplifier using complete hybrid-Model. [10 Marks]

**COMPLETE HYBRID EQUIVALENT MODEL:** 

[2 Marks]



<u>Current Gain:</u> [2 Marks]

Applying Kirchhoff's current law to the output circuit

$$I_o = h_f I_b + I = h_f I_i + \frac{V_o}{1/h_o} = h_f I_i + h_o V_o$$
 as  $V_o = -I_o R_L$  hence  $I_o = h_f I_i - h_o I_o R_L$ 

$$I_o + h_o I_o R_L = h_f I_i = > I_o (1 + h_o R_L) = h_f I_i = > A_i = \frac{I_o}{I_i} = \frac{h_f}{1 + h_o R_L}$$

Voltage Gain: [2 Marks]

$$V_i = I_i h_i + V_O h_r \quad \text{as } I_i = \frac{(1 + h_o R_L) I_o}{h_f} \quad \text{and} \quad I_o = \frac{-V_o}{R_L} \\ = > V_i = \frac{-(1 + h_o R_L) h_i}{h_f R_L} V_O + V_O h_r$$

$$V_{i} = \frac{V_{O}h_{r}h_{f}R_{L} - (1 + h_{o}R_{L})h_{i}V_{o}}{h_{f}R_{L}} = V_{i} = \frac{V_{O}h_{r}h_{f}R_{L} - h_{i}V_{o} - h_{i}V_{o}h_{o}R_{L}}{h_{f}R_{L}}$$

$$=>V_i=\frac{-V_o\big[h_i+\big(h_ih_o-h_rh_f\big)R_L\big]}{h_fR_L}$$

$$A_V = \frac{V_o}{V_i} = A_V = \frac{-h_f R_L}{h_i + (h_i h_o - h_r h_f) R_L}$$

Input Impedance: [2 Marks]

$$V_i = I_i h_i + h_r V_o$$
 and  $V_o = -I_o R_L$  hence  $V_i = I_i h_i - I_o R_L h_r$  as  $I_o = A_i I_i$ 

$$V_{i} = I_{i}h_{i} - R_{L}h_{r}A_{i}I_{i}$$
 and  $Z_{i} = \frac{V_{i}}{I_{i}} = h_{i} - R_{L}h_{r}A_{i}$  as  $A_{i} = \frac{h_{f}}{1 + h_{o}R_{L}}$  hence  $Z_{i} = h_{i} - \frac{R_{L}h_{r}h_{f}}{1 + h_{o}R_{L}}$ 

output Impedance: The output impedance od an amplifier is defined to be the ratio of the output voltage to the output current with the signal  $V_S$  set to zero.

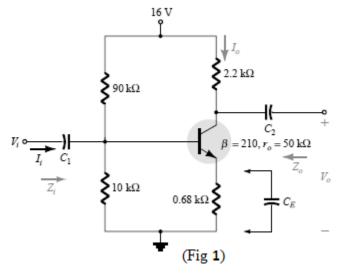
$$V_S - I_i R_S - I_i h_i - h_r V_o = 0$$
 for calculating  $Z_o$ ;  $V_S$  has to be set to zero =>  $I_i (R_S + h_i) = -h_r V_o$ 

$$I_i = \frac{-h_r V_o}{R_S + h_i}$$

$$I_o = h_f I_i + h_o V_o = > I_o = \frac{-h_r h_f V_o}{R_S + h_i} + h_o V_o$$

$$Z_o = \frac{V_o}{I_o} = \frac{1}{h_o - \left[\frac{h_r h_f}{(R_S + h_i)}\right]}$$

2. Calculate the following for the network shown in (Fig 1) with and without  $C_E$  and compare the voltage  $\mathsf{gain.}(a)r_e \ (b) \ Z_i \ (c)Z_0 \ (d)A_V \ (e)A_i$ [10 Marks]



ANSWER: (Without  $C_E$ )

[5 Marks]

 $\beta R_E \ge 10 R_2 = > 210 \times 0.68 K\Omega \ge 10 \times 10 K\Omega = > 142.8 K\Omega \ge 100 K\Omega (Satisfied)$ 

$$V_{B} = \frac{V_{CC}R_{2}}{R_{1} + R_{2}} = \frac{16 \times 10K\Omega}{90K\Omega + 10K\Omega} = 1.6V$$

$$V_{E} = V_{B} - V_{BE} = 1.6 - 0.7 = 0.9V$$

$$I_{E} = \frac{V_{E}}{R_{E}} = \frac{0.9}{0.68K\Omega} = 1.32mA$$

$$r_{e} = \frac{26mV}{I_{E}} = \frac{26mV}{1.32mA} = 19.69\Omega$$

$$V_E = V_B - V_{BE} = 1.6 - 0.7 = 0.9$$

$$V_E = V_B - V_{BE} = 1.6 - 0.7 = 0.9V$$

$$I_E = \frac{V_E}{R_E} = \frac{0.9}{0.68K\Omega} = 1.32mA$$

$$r_e = \frac{26mV}{I_E} = \frac{26mV}{1.32mA} = 19.69\Omega$$

$$Z_b = \beta r_e + (\beta + 1) R_E = 210 \times 19.69 \Omega + (210 + 1) 0.68 K \Omega = 147.6 K \Omega$$

$$R' = \frac{R_1 R_2}{R_1 + R_2} = \frac{90K\Omega \times 10K\Omega}{90K\Omega + 10K\Omega} = 9K\Omega$$

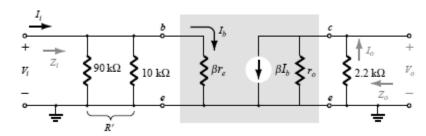
$$Z_i = R' \big| |Z_b = 9K\Omega| \big| 147.6K\Omega = 8.48K\Omega$$

$$Z_o = R_C = 2.2K\Omega$$

$$A_V = \frac{-R_C}{(R_E + r_e)} = \frac{-2.2K\Omega}{(19.69\Omega + 0.68K\Omega)} = -3.14$$

$$A_i = -A_V \frac{Z_i}{R_C} = 3.14 \times \frac{8.48 K\Omega}{2.2 K\Omega} = 12.10$$

(With  $C_E$ ) [5 Marks]



$$R' = \frac{R_1 R_2}{R_1 + R_2} = \frac{90K\Omega \times 10K\Omega}{90K\Omega + 10K\Omega} = 9K\Omega$$

$$Z_i = R' \big| |\beta r_e = 9K\Omega| \big| 4.135K\Omega = 2.83K\Omega$$

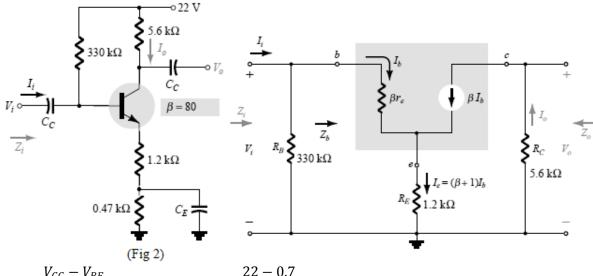
$$A_V = \frac{-R_C}{r_e} = \frac{-2.2K\Omega}{19.69\Omega} = -111.73$$

$$A_i = -A_V \frac{Z_i}{R_C} = 111.73 \times \frac{2.83K\Omega}{2.2K\Omega} = 143.72$$

$$Z_o = R_C = 2.2K\Omega$$

# $Z_o=R_{\mathcal{C}}=2.2K\Omega$ 3. For the network shown in (Fig 2). Determine $r_e,Z_i,Z_0,A_V$ , $A_i$

[10 Marks]



$$I_B = \frac{V_{CC} - V_{BE}}{R_B + (\beta + 1)R_E} = \frac{22 - 0.7}{330 \times 10^3 + (80 + 1)(1.2 + 0.47) \times 10^3} = 45.77 \mu A$$

$$I_E = (\beta + 1)I_B = (80 + 1)45.77\mu A = 3.708mA$$

$$r_e = \frac{26mV}{I_E} = \frac{26mV}{3.708mA} = 7.01\Omega$$
 [2 Marks]

$$Z_b = \beta r_e + (\beta + 1)R_E = (80 \times 7.01\Omega) + (80 + 1)1.2K\Omega = 97.76K\Omega$$

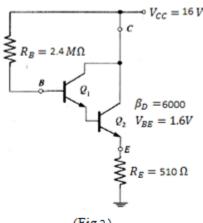
$$Z_i = R_B | |Z_b = 330K\Omega | | 97.76K\Omega = 75.41K\Omega$$
 [2 Marks]

$$Z_o = R_C = 5.6K\Omega$$
 [2 Marks]

$$A_V = \frac{-R_C}{(R_E + r_e)} = \frac{-5.6K\Omega}{(1.2K\Omega + 7.01\Omega)} = -4.639$$
 [2 Marks]

$$A_i = -A_V \frac{Z_i}{R_C} = 4.639 \times \frac{75.41 K\Omega}{5.6 K\Omega} = 62.469$$
 [2 Marks]

4. (a) Calculate the DC bias voltages and Currents for the given circuit (Fig 3). [5 Marks]



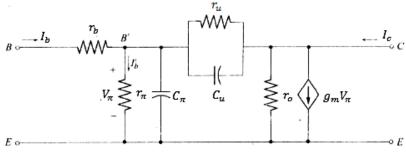
$$I_B = \frac{V_{CC} - V_{BE}}{R_B + (\beta_D + 1)R_E}$$

$$I_B = \frac{16 - 1.6}{2.4 \times 10^6 + (6000 + 1)510} = 2.637 \mu A$$
[2 Marks]

$$I_E = (\beta_D + 1)I_B = (6000 + 1)2.637\mu A = 15.82mA$$
 [2 Marks]  
 $V_E = I_E R_E = 15.82 \times 10^{-3} \times 510 = 8.0709V$  [1 Mark]

$$V_E = I_E R_E = 15.82 \times 10^{-5} \times 510 = 8.0709V$$

(b) Draw and explain the hybrid-  $\pi$  model of transistor in CE configuration mentioning significance of each component in Model. [5 Marks]



[1 Mark]

[1 Mark]

**HYBRID**  $\pi$  **MODEL:** It is the more accurate model for High frequency effects. For low frequency approximations, the model can be made with the  $r_e$  model. **[4 Marks]** 

The capacitors appear in the hybrid  $\pi$  model are stray capacitors. The capacitive effect only come into play at high frequencies. For low and mid frequencies their reactance is very large, and they can be considered open circuit. The capacitance value is in few pico farad(pf) to few tens of pico farad (pf).

 $r_u$ ,  $r_\pi$  &  $r_o$  are the resistance between the indicated terminals of the device, when the device is in the active region.

u provides the union, it provides between collector and base terminals.

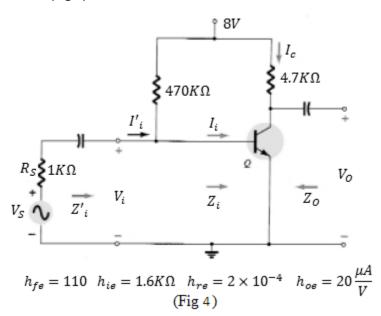
 $r_b$  is usually very small it can be replaced by a short-circuit equivalent.

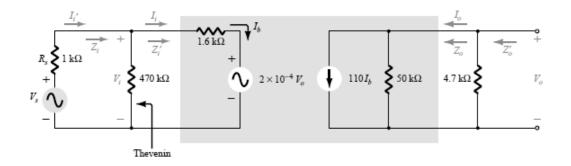
 $r_u$  is usually so large it can be ignored for most applications.

$$r_{\pi} = \beta r_{e}$$
  $g_{m} = \frac{1}{r_{e}}$   $r_{o} = \frac{1}{h_{oe}}$   $h_{re} = \frac{r_{\pi}}{r_{\pi} + r_{u}} = \frac{r_{\pi}}{r_{u}}$ 

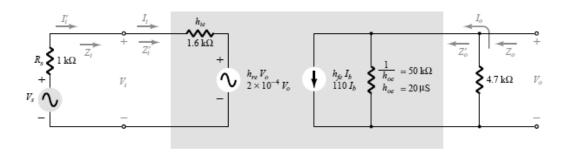
CE amplifier is most widely used because CE transistor have high gain than any other configuration.

5. Calculate the input impedance, output impedance, voltage gain and current gain for the given circuit (Fig 4). [10 Marks]





[2 marks]



[2 marks]

$$Z'_{i} = h_{ie} - \frac{R_{L}h_{re}h_{fe}}{1 + h_{oe}R_{L}} = > Z'_{i} = 1.6K\Omega - \frac{(4.7K\Omega)(2 \times 10^{-4})110}{1 + (20\mu S \times 4.7K\Omega)} = 1.505K\Omega$$

$$Z_i = 470K\Omega ||Z_i| \Rightarrow Z_i = 1.5K\Omega$$
 [2 marks]

$$A_V = \frac{-h_{fe}R_L}{h_{ie} + \left(h_{ie}h_{oe} - h_{re}h_{fe}\right)R_L} = > A_V = \frac{-110(4.7K\Omega)}{1.6K\Omega + (1.6K\Omega \times 20\mu S - (2 \times 10^{-4}) \times 110)(4.7K\Omega)}$$

$$A_V = -313.9$$
 [1 mark]

$$A_i = \frac{I_o}{I_i} = \frac{h_{fe}}{1 + h_{oe}R_L} = \frac{110}{1 + (20\mu S \times 4.7K\Omega)} = 100.54$$
 [1 mark]

$$Z'_{o} = \frac{1}{h_{oe} - \left[\frac{h_{re}h_{fe}}{(R_{S} + h_{ie})}\right]} = \frac{1}{20\mu S - \left[(2 \times 10^{-4}) \times \frac{110}{(1K\Omega + 1.6K\Omega)}\right]} = 86.67K\Omega$$

$$Z_0 = R_C ||Z_0|| = |Z_0|| = 4.7K\Omega || |86.67K\Omega|| = |Z_0|| = 4.45K\Omega$$
 [2 marks]

6. (a) Determine the input impedance, output impedance, voltage gain and current gain for the circuit shown below (Fig 5). [5 Marks]

$$V_i$$

$$I_i$$

$$Z_i$$

$$V_i$$

$$I_i$$

$$V_o$$

(a) 
$$Z_i = R_B || h_{ie} = 330 \text{ k}\Omega || 1.175 \text{ k}\Omega$$
  
 $\cong h_{ie} = 1.171 \text{ k}\Omega$  [1 mark]

(b) 
$$r_o = \frac{1}{h_{oe}} = \frac{1}{20 \ \mu\text{A/V}} = 50 \ \text{k}\Omega$$
  
 $Z_o = \frac{1}{h_{oe}} ||R_C = 50 \ \text{k}\Omega||2.7 \ \text{k}\Omega = 2.56 \ \text{k}\Omega \cong R_C \ [1 \ \text{mark}]$ 

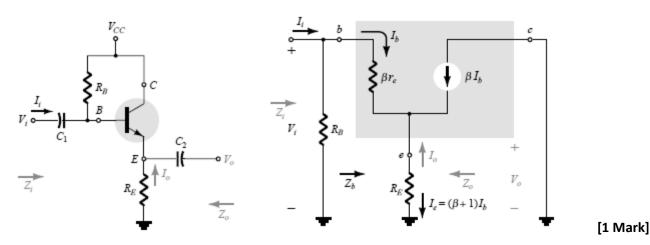
(c) 
$$Av = -\frac{h_{fe}(R_C || 1/h_{oe})}{h_{ie}} = -\frac{(120)(2.7 \text{ k}\Omega || 50 \text{ k}\Omega)}{1.171 \text{ k}\Omega} = -262.34$$
[1 mark]

$$A_i = -A_V \frac{Z_i}{R_C} = 262.34 \times \frac{1.171K\Omega}{2.7K\Omega} = 113.77$$
 [1 Mark]

(b) Analyze the  $r_{\it e}$  parameter model for emitter follower circuit and derive

 $Z_i$  ,  $Z_o$  ,  $A_V$  ,  $A_i$  [5 Marks]

# **EMITTER FOLLOWER CIRCUIT/COMMON COLLECTOR CONFIGURATION:**



For emitter follower circuit the output is taken from the emitter terminal. The output is slightly less than the input signal hence  $A_V \approx 1$ 

$$V_{i} = I_{b}\beta r_{e} + I_{e}R_{E} => V_{i} = I_{b}\beta r_{e} + (\beta + 1)I_{b}R_{E}$$

$$Z_{b} = \frac{V_{i}}{I_{b}} => Z_{b} = \beta r_{e} + (\beta + 1)R_{E}$$

$$=> Z_{b} \approx \beta(r_{e} + R_{E})$$

 $Z_i = R_B || Z_b$  [1 Mark]

Output impedance is calculated by setting  $V_i$  to zero hence  $Z_o = R_E || r_e$  [1 Mark]

$$V_o = \frac{V_i R_E}{R_E + r_e} = A_V = \frac{V_o}{V_i} = \frac{R_E}{R_E + r_e}$$
 as  $R_E + r_e \approx R_E = A_V \approx 1$  [1 Mark]

the + ve sign indicates there is no phase shift between  $V_o \& V_i$ 

$$I_b = \frac{I_i R_B}{R_B + Z_b} = I_i = \frac{(R_B + Z_b)I_b}{R_B}$$
 and  $I_o = -I_e = -(\beta + 1)I_b$ 

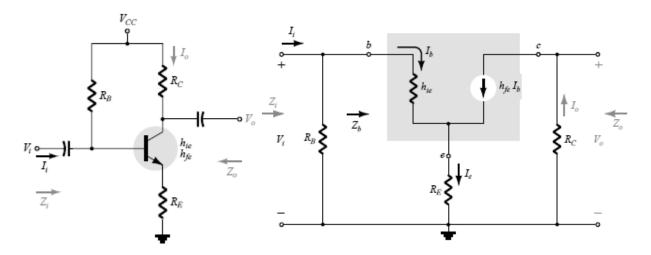
$$A_{i} = \frac{I_{o}}{I_{i}} = \frac{-(\beta + 1)I_{b}}{\left[\frac{(R_{B} + Z_{b})I_{b}}{R_{B}}\right]} = -(\beta + 1)I_{b} \times \frac{R_{B}}{(R_{B} + Z_{b})I_{b}} = \frac{-(\beta + 1)R_{B}}{R_{B} + Z_{b}} = \frac{-\beta R_{B}}{R_{B} + Z_{b}} \quad as \quad \beta + 1 \approx \beta$$

The current gain can also be calculated as

$$A_i = -A_V \frac{Z_i}{R_E}$$
 [1 Mark]

7. (a) Describe the h-parameter model for emitter bias circuit and derive  $Z_i$ ,  $Z_o$ ,  $A_V$ ,  $A_i$  using approximate hybrid model. [5 Marks]

### **EMITTER BIAS CONFIGURATION:**



$$Z_b = h_{ie} + (h_{fe} + 1)R_E$$

$$Z_i = R_B || Z_b$$

$$Z_O = R_C$$

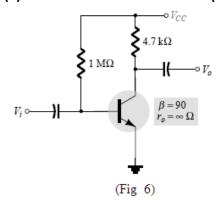
$$A_V = \frac{V_o}{V_i} = \frac{-h_{fe} R_C I_b}{Z_b I_b} = > A_V = \frac{-h_{fe} R_C}{h_{fe} R_E} = > A_V = \frac{-R_C}{R_E}$$

$$I_o = h_{fe}I_b$$
 and  $I_b = \frac{I_iR_B}{R_B + Z_b} = > I_i = \frac{(R_B + Z_b)I_b}{R_B}$ 

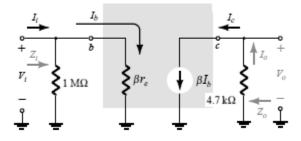
$$A_i = \frac{I_o}{I_i} = \frac{\left[h_{fe}I_b\right]}{\left[\frac{(R_B + Z_b)I_b}{R_B}\right]} = h_{fe}I_b \times \frac{R_B}{(R_B + Z_b)I_b} = \frac{h_{fe}R_B}{Z_b + R_B}$$

The current gain can also be calculated as  $A_i = -A_V \frac{Z_i}{R_C}$ 

(b) For the network shown below (Fig 6), determine  $V_{\it CC}$  for a voltage gain of  $A_{\it V}\,=-180$ 



[5 Marks]



[1 Mark]

 $As r_o \ge 10R_C$  (Satisfied)

Hence 
$$A_V = \frac{-R_C}{r_e} = -180 = > r_e = \frac{R_C}{180} = > r_e = 26.11\Omega$$
 [1 Mark]

$$r_e = \frac{26mV}{I_E} = I_E = \frac{26mV}{26.11\Omega} = 0.9957mA$$
 [1 Mark]

$$I_B = \frac{I_E}{(\beta + 1)} = 10.94 \mu A$$
 [1 Mark]

$$I_B = \frac{V_{CC} - V_{BE}}{R_B} = V_{CC} = I_B R_B + V_{BE} = V_{CC} = 11.64V$$
 [1 Mark]