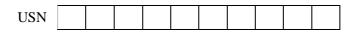
CMR
INSTITUTE OF
TECHNOLOGY





Internal Assesment Test - II									
Sub:	Sub: ENGINEERING ELECTROMAGNETICS						Code:	15EC36	
Date:	07 / 11 / 2017	Duration:	90 mins	Max Marks:	50	Sem:	3rd	Branch:	ECE-Diploma
Answer FIVE FULL Questions									

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N 1							
		Marks	CO	RBT			
1 (a) 1 (b)	Derive Lorentz force equation and mention the applications of its solutions. A charged particle moves with a uniform velocity of $4 a_x m/s$ in a region where	[6]	CO1	L3			
1 (0)	$E = 20 \ a_y \ V/m$ and $B = B_0 \ a_z \ wb/m^2$. Determine B _o such that the velocity of the particle remains constant.	[4]	CO1	L3			
2	[OR] Two infinitely long straight conductors, both carrying current of 10mA each in the same direction are located at x=0; y=0 and x=0; y=10m respectively. Derive the expression for force per unit length between them. Also calculate the force per unit length between them.	[6+4]	CO1	L3			
3	Obtain the boundary conditions at the interface between two magnetic materials. [OR]	[10]	CO1	L3			
4(a)	Given B = 0.05 T and μ_r = 50. Find magnetic susceptibility, Magnetization and Magnetic field Intensity.	[5]	CO1	L3			
4(b)	Two differential current elements are present as follows: $I_1 dl_1 = -3a_y$ A.m at $P_1(5,2,1)$ and $I_2 dl_2 = -4a_z$ A.m at $P_2(1,8,5)$. Determine differential force on element 2 due to element 1.	[5]	CO1	L3			
5(a) 5(b)	Derive the expression for force on a current element placed in a steady magnetic field. Calculate M for the material in which: (a) μ_r =1.4 and H = 350 a_x A/m. (b) μ_r = 6 and there are 2.5 × 10 29 atoms/m ³ , each having magnetic dipole moment of 2.8 × 10 $^{-30}$ a_x A.m ²	[6]	CO1				
	[OR]						
6	Write the equations to compare electric circuit and magnetic circuit with respect to i) e.m.f and m.m.f, ii) Electric and magnetic scalar potential, iii) Electric current and magnetic flux, iv) Resistance and reluctance, v) $\oint E \cdot dl$ and $\oint H \cdot dl$	[10]	CO1	L3			
7(a)	Derive the expression for magnetic torque due to a rectangular current loop.	[5]	CO1	L3			
7(b)	An air core toroid has 500 turns, mean radius of 15 cm, cross-sectional area of 6 cm^2 . The magneto motive force is 2000 A.t. Calculate total reluctance, flux, flux-density, field intensity inside the core.	[5]	CO1	L3			
	[OR]						
8(a) 8(b)	Derive the expression for force between differential current elements The magnetic field intensity is given in a region of space as	[5]	CO1	L3			
	$H = \frac{(x+2y)}{z^2} a_y + \frac{2}{z} a_z A/m$. Calculate current density in that region.	[5]	CO1	L3			
9(a)	At a point P(x,y,z) the components of vector magnetic potential are given as $Ax = 4x + 3y + 2z$, $Ay = 5x + 6y + 3z$, $Az = 2x + 3y + 5z$. Determine B at P.	[4]	CO1	L3			
9(b)	Find the torque on the square wire loop of current 0.6 A , bounded by $x = -1$ to $x = 1$ and $y = -1$ to $y = 1$ about $(2, 3, 4)$ by the field $\mathbf{B} = (0.4\mathbf{a}\mathbf{x} + 0.6\mathbf{a}\mathbf{y} - 0.7\mathbf{a}\mathbf{z})$ T acting only on the side of the loop for which $y = 1$. [OR]		CO1	L3			
10	Let $\mu_1 = 4 \mu_0$ H/m in region 1 where $z > 0$, while $\mu = 7 \mu_0$ H/m where $z < 0$. Let $K = 80 ax A/m$ on the surface $z = 0$. In region1, the magnetic flux density is $B1 = 2ax - 3ay + az$ mT. Find B_2 .	[10]	CO1	L3			

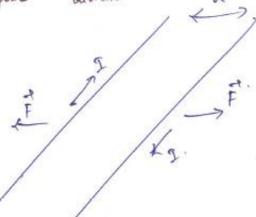
SCHEME OF EVALUATION

		Mark Split-Up
1(-)		* *
1(a)	Derivation	4
(1.)	Final Expression	2
(b)	Formula	2
	Approach & Answer	2
2	Diagram	1
	Derivation	4
	Final Expression	1
	Solution	4
3	Normal Conditions	3
	Tangential Conditions	3
4(a)	Formula	1
	Approach	3
	Answer	1
(b)	Formula	1
	Approach	3
	Answer	1
5(a)	Derivation	4
	Final Expression	2
5(b)	(i) Approach & Answer	2
	(ii) Approach & Answer	2
6	Comparison of each (i),(ii),(iii),(iv) and	5*2=10
	(v)	
7(a)	Diagram	1
	Derivation	3
	Final Expression	1
(b)	Formula & Approach	4
	Answer	1
8(a)	Derivation	4
	Final Expression	1
(b)	Formula	1
	Approach	3
	Answer	1
9(a)	Formula	1
	Approach	2
	Answer	1
(b)	Formula	1
	Approach	4
	Answer	1
10	Formula & Approach	8
	Answer	2

```
Electric field assures a force to be exerted on a statemany or morning change
abouty magnetic field - exert force only on a morning charge
 (produced by moring charges)
 for a moving charge
      Hostor force on a changed particle, \vec{E} = \vec{\alpha} \vec{E} - \vec{D}.
          If the change is in motion, the above equation gives the force at any point in its hojectory.
Force on a particle win medicin in a magnetic speld of flow density . B
          F = Q V x B direction of force is to to both it and B
                  Fappled It to the dan in which change is moving .
              Arebration vector is always revore to rebuilty vector
                          Pricapable of transferring energy to a moving charge
   flective field - exerts force on porticle which is independent of the
                         dro of programmy charge
                & effects an energy transfer between field and purlicle is general
Freez on a moving particle arising from combined electric & magnetic field.
         (by superpositions)
                 F = A(F + VTRB) - Lorentz force equation
            Solution is required in deformining
                       plasmo characteristics in a magneto hychrodynamic (MHD)
                    charged particle meture in combinued electric and magnetic
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a particle moves with constant velocity, its arrelacation is

Find Force of repulsion between two infinitely long, straight parallel flamontory anductors with separation d' and carrying equal but



current at either come

F = BIL

force per und bength of infinite conductors

Force per unit length

of two infinitely long =
$$F/L = \frac{\mu_0 I^2}{2\pi d}$$

parallel current corrying

conductors = $\frac{\chi}{4\pi \chi_0^{-7}} \times \frac{\chi}{4\pi \chi_$

$$= \frac{4\pi \hat{x}_{10}^{-7} \times (10 \times 10^{-3})^{2}}{\cancel{x}_{11}^{-7} \times \cancel{x}_{10}^{-7}}$$

$$= 20 \times 10^{-7} \times 10^{-6}$$

Magnetic boundary conditions:

$$\vec{B}_{1} = \vec{B}_{12} + \vec{B}_{N2}$$

$$\vec{B}_{2} = \vec{B}_{13} + \vec{B}_{N2}$$

$$\vec{B}_{3} = \vec{\mu} + \vec{H}$$

$$\vec{M}_{1} = \vec{M}_{11} + \vec{M}_{N1}$$

$$\vec{H}_{1} = \vec{H}_{12} + \vec{H}_{N2}$$

O Games law for Mayrible fields:

top bettern latered
$$B_{N2} \cdot \Delta S + B_{E_1} \cdot \Delta S = B_{N2} \cdot \Delta S + B_{E_2} \cdot \Delta S = B_{N3} \cdot \Delta S + B_{E_3} \cdot \Delta S = B_{N3} \cdot \Delta$$

By . As - By As =0

Description Law:

$$\int_{L} AI \cdot dI = F_{enc}$$

$$\int_{L} + \int_{AL} +$$

Magnetization,
$$M = Y_m H$$

$$= Y_m \cdot B$$

$$= A_0 \times B$$

= 7.961 x15 S

4) b)

Problem:

Given
$$P_{1}(5|2,1)$$
, $B_{1}(1,815)$,

 $I_{1}dI_{1} = -3ay_{1}$, $A.m$
 $I_{2}dI_{2}^{T} = -4ax_{2}$, $A.m$
 $I_{3}dI_{2}^{T} = -4ax_{2}$, $A.m$
 $I_{2}dI_{3}^{T} = -4ax_{2}$, $I_{3}dI_{2}$
 $I_{2}dI_{3}^{T} = -4ax_{2}$, $I_{3}dI_{2}$
 $I_{2}dI_{3$

5) a)

Soln. (a) Criven
$$\mu_R = 1.4$$
, $\vec{H} = 350 \, \vec{a}_x \, A/m$.
 $\chi m = (\mu_R - 1) = 0.4$
 $\gamma m_{\text{agnotization}}, \vec{M} = \chi m \vec{H} = 0.4 \times 350 \, \vec{a}_x$
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 $\gamma m_{\text{agnotization}}, \vec{M} = \chi m \vec{H} = \chi m \vec{H}$

Magnetic Circuit:

(Electric circuit)

$$\vec{E}^{\dagger} = -\vec{\nabla}V$$
 $V_{a,b} = -\int \vec{F} \cdot \vec{di}$
 $\vec{D} \cdot \vec{E} = \int \vec{F} \cdot \vec{di}$
 $\vec{E} = \int \vec{F} \cdot \vec{F} \cdot \vec{F}$
 $\vec{F} = \int \vec{F} \cdot \vec{F$

m.m.g. = # = on R

Magnetic Porque and Moment:

Forgue (or mechanical moment of first) on the loop is the Wester F and the moment arm F

Rectangular loop of length it and width 'w ploced in a uniform magnetic fold B.

Force
$$\vec{F} = I \int d\vec{k} \times \vec{k} + I \int d\vec{k} \times \vec{k}$$

$$= I \int dz \ \vec{az} \times \vec{k}^2 + I \int dz \ \vec{az} \times \vec{k}^2$$

$$= I \int dz \ \vec{az} \times \vec{k}^2 + I \int dz \ \vec{az} \times \vec{k}^2$$

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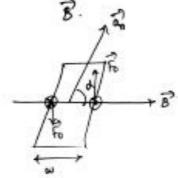
$$= I \int dz \ \vec{az} \times \vec{k}^2 + I \int dz \ \vec{az} \times \vec{k}^2$$

$$= I \int dz \ \vec{az} \times \vec{k}^2 + I \int dz \ \vec{az} \times \vec{k}^2 + I \int dz \ \vec{az} \times \vec{k}^2$$

$$= I \int dz \ \vec{az} \times \vec{k}^2 + I \int dz \ \vec{k} \times \vec{k} \times \vec{k}^2 + I \int dz \ \vec{k} \times \vec{k} \times \vec{k} \times \vec{k} \times \vec{k}^2 + I \int dz \ \vec{k} \times \vec{k}$$

Accounter, to and -to act at different points on the loop, thereby creating a couple.

Let Normal to the plane of the loop makes as angle of with R.



Tongue (moment of couple) on the shop $\vec{T} = \vec{T} \times \vec{F}$ $|\vec{T}| = |\vec{F}_0| \approx \sin x$ $|\vec{T}| = 811 \approx \sin x$ $|\vec{T}| = 811 \approx \sin x$ $|\vec{T}| = 1 \approx 100$

Magnetic dipole moment,

Magnetic dipole moment,

M = IS and Am²

- product of occurrent and one a 8 the loop.

- its direction normal to the book.

7 = 7 8

Torque is is the direction of and of relation.

A is directed with the aim of reducing a solvent in and 8 are is same direction (is at equilibrium).

If bop is perpendicular to magnetic field, will be zono.

$$0 \quad R = \frac{l}{\mu s} = \frac{a_0 g}{\mu s}$$

(3) Flux density,
$$B = \frac{\phi}{S} = \frac{1.6 \times 10^{-6}}{6 \times 10^{-7}} = 2.667 \times 10^{-3} \text{ with } 2$$

(4) field intensity
$$A = \frac{B}{\mu} = \frac{2667 \times 10^{-3}}{451 \times 10^{-9}} = 2123.4 \text{ At/m}.$$

8)a)

Force between differential ourment elements:

Consider Two current elements, to find force blow two current abovents

Differential force on a differential event about $d\vec{r}' : \vec{j}'' d\vec{k} \times \vec{k}$

paperential flux density (dB₂) at point 2 caused by current element 1 (2dL₁) differential amount of force on element 2, $d(dF_2) = \frac{1}{2} dL_2^T \times dE_2^T$ where $dE_3 = \frac{1}{4} dE_2^T = \frac{1}{4} dL_1^T \times qE_{12}^T$ $d(dF_2^T) = \frac{1}{4} dL_2^T \times qE_{12}^T = \frac{1}{4} dL_2^T$

From the differential force, one can get

Potal force between two filamentary circuit

$$\begin{bmatrix}
F_2 : & F_{12} I_2 & \int dI_3 \times \int dI_3 \times q_{R12} \\
\hline
F_3 : & \int dI_4 I_2 & \int dI_5 \times dI_1 \times q_{R12}
\end{bmatrix}$$
Gen

$$\begin{bmatrix}
F_3 : & \int dI_4 I_2 & \int dI_5 \times dI_1 \\
\hline
F_{112} I_4 I_3 & \int dI_5 \times dI_1 \\
\hline
F_{112} I_4 I_4 I_5 & \int dI_5 \times dI_5
\end{bmatrix} \times dI_5$$

8)b) $\overrightarrow{\nabla} \times \overrightarrow{H} = \begin{vmatrix} \widehat{a}_{1} & \widehat{a}_{2} & \widehat{a}_{2} \\ \widehat{d}_{1} & \widehat{d}_{3} & \widehat{d}_{2} \\ \widehat{d}_{1} & \widehat{d}_{3} & \widehat{d}_{2} \end{vmatrix} = 2(\underline{a} + \underline{a}_{2}) \hat{a}_{1} + \frac{1}{2} \hat{a}_{2}$ $0 \quad \underline{(a + \underline{a}_{3})}_{2} \stackrel{?}{=} 2$

$$CT = \int \vec{J} \cdot d\vec{x} = \int \left(\frac{2(x+2y)}{z^{2}} \vec{a}_{x} + \frac{1}{z^{2}} \vec{a}_{x} \right) \cdot dx \, dy \, \vec{a}_{x}$$

$$= \frac{1}{z^{2}} \int dx \, dy = \frac{1}{6} \cdot \left[z^{-1} \right] \left[s - 3 \right] = \frac{1}{8} A$$

$$x = 1 y = 3$$

$$\vec{B} = \vec{\nabla} \times \vec{A} = \begin{bmatrix} \vec{a} & \vec{a} & \vec{a} \\ \vec{b} & \vec{b} \\ \vec{b} & \vec{a} \end{bmatrix} \qquad \vec{a}$$

$$\vec{b} = \vec{\nabla} \times \vec{A} = \begin{bmatrix} \vec{a} & \vec{a} \\ \vec{b} & \vec{b} \\ \vec{b} & \vec{c} \end{bmatrix} \qquad \vec{b}$$

$$\vec{b} = \vec{b} \times \vec{b} = \begin{bmatrix} \vec{a} & \vec{b} \\ \vec{b} & \vec{c} \end{bmatrix} \qquad \vec{b} = \begin{bmatrix} \vec{a} & \vec{b} \\ \vec{a} & \vec{c} \end{bmatrix} \qquad \vec{b} = \begin{bmatrix} \vec{a} & \vec{b} \\ \vec{c} & \vec{c} \end{bmatrix} \qquad \vec{b} = \begin{bmatrix} \vec{a} & \vec{b} \\ \vec{c} & \vec{c} \end{bmatrix} \qquad \vec{b} = \begin{bmatrix} \vec{a} & \vec{c} \\ \vec{c} & \vec{c} \end{bmatrix} \qquad \vec{b} = \begin{bmatrix} \vec{c} & \vec{c} \\ \vec{c} & \vec{c} \end{bmatrix} \qquad \vec{b} = \begin{bmatrix} \vec{c} & \vec{c} \\ \vec{c} & \vec{c} \end{bmatrix} \qquad \vec{b} = \begin{bmatrix} \vec{c} & \vec{c} \\ \vec{c} & \vec{c} \end{bmatrix} \qquad \vec{b} = \begin{bmatrix} \vec{c} & \vec{c} \\ \vec{c} & \vec{c} \end{bmatrix} \qquad \vec{b} = \begin{bmatrix} \vec{c} & \vec{c} \\ \vec{c} & \vec{c} \end{bmatrix} \qquad \vec{b} = \begin{bmatrix} \vec{c} & \vec{c} \\ \vec{c} & \vec{c} \end{bmatrix} \qquad \vec{b} = \begin{bmatrix} \vec{c} & \vec{c} \\ \vec{c} & \vec{c} \end{bmatrix} \qquad \vec{b} = \begin{bmatrix} \vec{c} & \vec{c} \\ \vec{c} & \vec{c} \end{bmatrix} \qquad \vec{b} = \begin{bmatrix} \vec{c} & \vec{c} \\ \vec{c} & \vec{c} \end{bmatrix} \qquad \vec{b} = \begin{bmatrix} \vec{c} & \vec{c} \\ \vec{c} & \vec{c} \end{bmatrix} \qquad \vec{b} = \begin{bmatrix} \vec{c} & \vec{c} \\ \vec{c} & \vec{c} \end{bmatrix} \qquad \vec{b} = \begin{bmatrix} \vec{c} & \vec{c} \\ \vec{c} & \vec{c} \end{bmatrix} \qquad \vec{b} = \begin{bmatrix} \vec{c} & \vec{c} \\ \vec{c} & \vec{c} \end{bmatrix} \qquad \vec{b} = \begin{bmatrix} \vec{c} & \vec{c} \\ \vec{c} & \vec{c} \end{bmatrix} \qquad \vec{b} = \begin{bmatrix} \vec{c} & \vec{c} \\ \vec{c} & \vec{c} \end{bmatrix} \qquad \vec{b} = \begin{bmatrix} \vec{c} & \vec{c} \\ \vec{c} & \vec{c} \end{bmatrix} \qquad \vec{b} = \begin{bmatrix} \vec{c} & \vec{c} \\ \vec{c} & \vec{c} \end{bmatrix} \qquad \vec{b} = \begin{bmatrix} \vec{c} & \vec{c} \\ \vec{c} & \vec{c} \end{bmatrix} \qquad \vec{b} = \begin{bmatrix} \vec{c} & \vec{c} \\ \vec{c} & \vec{c} \end{bmatrix} \qquad \vec{b} = \begin{bmatrix} \vec{c} & \vec{c} \\ \vec{c} & \vec{c} \end{bmatrix} \qquad \vec{b} = \begin{bmatrix} \vec{c} & \vec{c} \\ \vec{c} & \vec{c} \end{bmatrix} \qquad \vec{b} = \begin{bmatrix} \vec{c} & \vec{c} \\ \vec{c} & \vec{c} \end{bmatrix} \qquad \vec{b} = \begin{bmatrix} \vec{c} & \vec{c} \\ \vec{c} & \vec{c} \end{bmatrix} \qquad \vec{b} = \begin{bmatrix} \vec{c} & \vec{c} \\ \vec{c} & \vec{c} \end{bmatrix} \qquad \vec{b} = \begin{bmatrix} \vec{c} & \vec{c} \\ \vec{c} & \vec{c} \end{bmatrix} \qquad \vec{b} = \begin{bmatrix} \vec{c} & \vec{c} \\ \vec{c} & \vec{c} \end{bmatrix} \qquad \vec{b} = \begin{bmatrix} \vec{c} & \vec{c} \\ \vec{c} & \vec{c} \end{bmatrix} \qquad \vec{b} = \begin{bmatrix} \vec{c} & \vec{c} \\ \vec{c} & \vec{c} \end{bmatrix} \qquad \vec{b} = \begin{bmatrix} \vec{c} & \vec{c} \\ \vec{c} & \vec{c} \end{bmatrix} \qquad \vec{b} = \begin{bmatrix} \vec{c} & \vec{c} \\ \vec{c} \end{bmatrix} \qquad \vec{b} = \begin{bmatrix} \vec{c} & \vec{c} \\ \vec{c} \end{bmatrix} \qquad \vec{b} = \begin{bmatrix} \vec{c} & \vec{c} \\ \vec{c} \end{bmatrix} \qquad \vec{b} = \begin{bmatrix} \vec{c} & \vec{c} \\ \vec{c} \end{bmatrix} \qquad \vec{b} = \begin{bmatrix} \vec{c} & \vec{c} \\ \vec{c} \end{bmatrix} \qquad \vec{b} = \begin{bmatrix} \vec{c} & \vec{c} \\ \vec{c} \end{bmatrix} \qquad \vec{b} = \begin{bmatrix} \vec{c} & \vec{c} \\ \vec{c} \end{bmatrix} \qquad \vec{b} = \begin{bmatrix} \vec{c} & \vec{c} \\ \vec{c} \end{bmatrix} \qquad \vec{b} = \begin{bmatrix} \vec{c} & \vec{c} \\ \vec{c} \end{bmatrix} \qquad \vec{b} = \begin{bmatrix} \vec{c} & \vec{c} \\ \vec{c} \end{bmatrix} \qquad \vec{b} = \begin{bmatrix} \vec{c} & \vec{c} \\ \vec{c} \end{bmatrix} \qquad \vec{c}$$

9) b)

$$\vec{f} = \vec{I} \vec{z} \times \vec{B}$$

$$\sum_{B=0.4}^{12} \frac{1}{6} = 0.407 + 0.604 - 0.702$$

$$\vec{F} = \vec{\Sigma} \vec{X} \vec{B} = \begin{bmatrix} \vec{a} \vec{x} & \vec{a} \vec{y} & \vec{a} \vec{z} \\ -1.2 & 0 & 0 \\ 0.4 & 0.6 & -0.7 \end{bmatrix}$$

$$= \frac{1}{4\pi} \left(0.00 - \overline{ay} \left(1.2 \times 0.9 - 0 \right) + \overline{az} \left(-1.2 \times 0.6 - 0 \right) \right)$$

$$\vec{R} = ?$$

$$\vec{R} = -2\vec{a_2} - 2\vec{a_1} - 4\vec{a_2}$$

$$\vec{T} = \vec{R} \times \vec{F} = \begin{vmatrix} \vec{a_1} & \vec{a_1} & \vec{a_2} \\ -2 & -2 & -4 \\ -2 & -2 & -4 \end{vmatrix} = \vec{a_2} \cdot \begin{pmatrix} (-1.92) & -\vec{a_1} & (1.44) \\ +\vec{a_2} & (1.66) \\ -1.92 & \vec{a_1} & -1.44 & \vec{a_2} \\ +1.66 & \vec{a_2} & Nm \end{vmatrix}$$

Soln: The normal component of
$$B_1$$
 is,
$$B_{N_1} = \begin{bmatrix} \vec{B_1} & \hat{a_{N_1 2}} \\ \vdots & \hat{a_{N_1 2}} \end{bmatrix} \cdot \hat{a_{N_1 2}} = \begin{bmatrix} (2\hat{a_1} - 3\hat{a_2} + \hat{a_2}) & (-\hat{a_2}) \end{bmatrix} \cdot (-\hat{a_2}) T$$

$$= \begin{bmatrix} \hat{a_2} & \text{mT} \\ \vdots & \vdots & \vdots \\ B_{N_2} = B_{N_1} = \hat{a_2} \text{mT} \end{bmatrix}$$
The tangential component of flux-density in again $\begin{bmatrix} \lambda_1 \\ B_{N_1} = B_1 - B_{N_1} = 2\hat{a_2} - 3\hat{a_2} \end{bmatrix} + \hat{a_2} - \hat{a_2}$

$$B_{N_1} = B_1 - B_{N_1} = 2\hat{a_2} - 3\hat{a_2} \end{bmatrix} \text{ mT}$$

The tangential field intensity in region 1 is, $H_{t_1} = \frac{B_{t_1}}{M_1} = \frac{2a_x - 3a_y}{4 \times 10^{-6}} = \frac{500a_x - 750a_y}{4 \times 10^{-6}}$ The tangential field intensity in region 2, the field intensity in region 2, the entire of the field intensity in region 2, the field intensity in region 2 is a sound of the field intensity in region 2 is a sound of the field intensity in region 2 is a field flux density in region 2 is a field flux of the field intensity in region 2 is a field flux of the field intensity in region 2 is a field flux of the field intensity in region 2 is a field flux of the field intensity in region 2 is a field flux of the field intensity in region 2 is a field flux of the field intensity in region 2 is a field flux of the field intensity in region 2 is a field flux of the field intensity in region 2 is a field flux of the field intensity in region 2 is a field flux of the field intensity in region 2 is a field flux of the field intensity in region 2 is a field flux of the field intensity in region 2 is a field flux of the field intensity in region 2 is a field flux of the field intensity in region 2 is a field inte