

is $B1 = 2ax - 3ay + az mT$. Find B_2 .

SOLUTION

 $1)a)$

(b)

\n3.
$$
rac{cosh\theta}{3}
$$
 = $frac{cosh\theta}{2}$ = $cosh\theta$ = $cosh\theta$ = $cosh\theta$ = $sinh\theta$ = $cosh\theta$ = $sinh\theta$ = $cosh\theta$ = $sinh\theta$ = $cosh\theta$ = $sinh\theta$ = $cosh\theta$ = $sinh\theta$ = $cosh\theta$ = $sinh\theta$ = $sinh\theta$ = $sinh\theta$ = $sinh\theta$ = $cosh\theta$ = $sinh\theta$ = $sinh\theta$ = $cosh\theta$ = $sinh\theta$ = $cosh\theta$ = $sinh\theta$ = $cosh\theta$ = $cosh\theta$

Force per unit length
of two infinitely long
parallel current comping $=$ $F/L = \frac{f_{6}T^{2}}{2\pi d}$ = $\frac{7}{4\pi} \times \frac{10\times10^{-3}}{10}$
= $\frac{7}{10} \times \frac{16}{5}$ conductors $= 20 \times 10^{-7} \times 10^{-6}$ $= 13$ $F/L = 2 \times 10^{-12} N/m$ $F/L = 2 p N/m$ 3) $\sum_{k=1}^{n} x_k + B_{k1} + B_{k2}$
 $\sum_{k=1}^{n} x_k + B_{k2}$
 $\sum_{k=1}^{n} x_k + B_{k2}$
 $\sum_{k=1}^{n} x_k + B_{k1} + B_{k2}$
 $\sum_{k=1}^{n} x_k + B_{k2} + B_{k2}$
 $\sum_{k=1}^{n} x_k + B_{k2}$
 $\sum_{k=1}^{n} x_k + B_{k2}$ conditions: stic boundary γ_{m} þι, ηų AL. Gaussion Sergate Gauss's law for Magnetic fields: $\label{eq:phi} \dot{\phi} = \dot{\oint} \vec{B}^1 \cdot \vec{J}^{\prime}_S = D$ \Rightarrow \int_{top} + $\int_{leftline}$ + $\int_{leftline}$ + $\int_{leftline}$ = $\frac{1}{6!}$. $\frac{1}{6!}$ = 0 B_{rel} (bettern I at A s I , B_{ℓ_1} B_{ℓ_2} B_{ℓ_3} B_{ℓ_4} B_{ℓ_5} B_{ℓ_6} B_{ℓ_7} B_{ℓ_8} B_{ℓ_9} B_{ℓ_1} B_{ℓ_2} B_{ℓ_3} B_{ℓ_4} B_{ℓ_5} B_{ℓ_6} B_{ℓ_7} B_{W2} Δs $+$ B_{H} \overline{e}_{H} \overline{e}_{H} \overline{e}_{H} B_{H} \overline{e}_{H} B_{H} \overline{e}_{H} B_{H} \overline{e}_{H} \overline{e}_{H} \overline{e}_{H} \overline{e}_{H} \overline{e}_{H} \overline{e}_{H} $\$ \Rightarrow $\mathcal{L}_{\mathcal{L}_{\mathcal{L}}}$ $B_{\text{PVI}} \cdot \Delta s = B_{\text{PVI}} \Delta s$ \Rightarrow $\mu_1 \mu_{\mathsf{M}} = \mu_1 \mu_{\mathsf{M2}}$ $B_{N1} = B_{N2}$ \Rightarrow $\frac{h_2}{\mu_1} = \frac{h_2}{\mu_2} = \frac{\mu_{0,2}}{\mu_1}$ $\frac{N_{m2}}{N_{m2}} \Rightarrow \boxed{N_{m1} = \frac{\gamma_{m1}}{\gamma_{m2}} \cdot \frac{\mu_2}{\mu_1}}$ $\frac{\mathsf{M}_{m1}}{\mathsf{N}_{m1}} = \frac{\mathsf{J}_{m1}}{\mathsf{A}_{l}}$

$$
\begin{array}{llll}\n\text{(a)} & \text{Suppose} & \text{div}(x) & \text{Laus.} \\
\int_{B_1} \int_{A_1}^{A_1} \int_{A_2}^{A_2} \int_{B_2}^{B_2} \int_{B_1}^{B_1} \int_{A_2}^{B_2} \int_{A_1}^{B_2} \int_{A_2}^{B_2} \int_{B_2}^{B_2} \int_{A_2}^{B_2} \int_{B_1}^{B_2} \int_{A_2}^{B_2} \int_{B_2}^{B_2} \
$$

4) b)

$$
\frac{p_{\text{r}}\theta_{\text{r}}}{2\pi}\left(\frac{1}{2}a_{11}^{12} - 3\frac{1}{2}a_{11}^{12}a_{11}^{12}a_{12}^{12}a_{11}^{12}a_{12}^{12}a_{11}^{12}a_{12}^{12
$$

5) a)

50b)
\n50b)
\n50a² (a) Given
$$
lnR = 1.4
$$
, $\vec{H} = 350 a2h/m$.
\n \therefore X m = $(lnR - 1) = 0.4$
\n \therefore Maynohization, $\vec{M} = 4.4$
\n \therefore Maynohization, $\vec{M} = 4.4$
\n \therefore M = 18 m = 2.5 × 10²⁹ x 2.8 × 10⁻³⁰ a x
\n \therefore M = 18 m = 2.5 × 10²⁹ x 2.8 × 10⁻³⁰ a x
\n= 0.7 a²h Am

 $\overline{6}$

$$
\frac{\text{Magnetic circuit}}{(\text{relative circuit})}
$$
\n
$$
\vec{F} = -\vec{v}V
$$
\n
$$
V_{a+b} = -\int_{a}^{b} \vec{F} \cdot d\vec{r}
$$
\n
$$
\vec{v} \cdot d\vec{r} = \int_{a}^{b} \vec{F} \cdot d\vec{r}
$$
\n
$$
\vec{v} \cdot d\vec{r} = \int_{a}^{b} \vec{r} \cdot d\vec{r}
$$
\n
$$
T = \int \vec{v} \cdot d\vec{r}
$$

Resistance.

 $V = I R$

 $\frac{1}{3}$

Conclusione

$$
6 = \frac{1}{R}
$$
\n
$$
8 = \frac{1}{\sigma s}
$$

$$
\overbrace{\mathcal{P} = \frac{1}{\mathcal{R}}}
$$
\n
$$
\overbrace{\mathcal{R} = \frac{1}{\mu s}}
$$

 \vec{B} . $\mu \vec{H}$

 $V_m = \oint \frac{R_{\text{ab}}}{R}$
 $V_m = \oint \frac{R}{R}$

 $\phi = \int \overrightarrow{s} \cdot d\overrightarrow{s}$

 $\vec{\mu}^{\dagger}$ = $\vec{\nabla}^{\dagger}$
 $V_{m \, a,b}$ = $\int_{a}^{b} \vec{\mu} \cdot d\vec{L}$

k/L	
$\oint \vec{E} \cdot d\vec{L} = 0$	$\oint \vec{H} \cdot d\vec{L} = \frac{T_{\text{fwel}}}{T_{\text{fwl}}}$
$\oint \vec{H} \cdot d\vec{L} = N\vec{L}$	
$\oint \vec{H} \cdot d\vec{L} = N\vec{L}$	
$\oint \vec{H} \cdot d\vec{L} = N\vec{L}$	
$\oint \vec{H} \cdot d\vec{L} = N\vec{L}$	

 $m \cdot m \cdot \frac{1}{2} \cdot \cdots \cdot \frac{1$

For
\n
$$
\vec{r} = \vec{r} \int dx \vec{u} \times \vec{B} + \vec{r} \int dz \vec{u} \times \vec{B}
$$
\n
$$
= \vec{r} \int dz \vec{u} \times \vec{B} + \vec{r} \int dz \vec{u} \times \vec{B}
$$
\n
$$
= \vec{r} \cdot \vec{r} - \vec{r} \quad \text{where} \quad |\vec{r} \cdot| = |\vec{B}| \text{ if } \vec{B} \text{ is the same point}
$$
\n
$$
\vec{r} = 0 \quad \therefore \quad \text{No. force on the length, when}
$$

 90 ution $\overline{\mathcal{A}}$ $25f$ $0 \quad R = \frac{1}{\mu s} = \frac{80}{\mu s}$ $=$ thrush 46767×616216 $R = 1.85 \times 0^9$ At/ob ϕ . R . F \odot $\phi = \frac{f}{R} = \frac{2000}{1.25 \times 10^9}$ $=$ 1600 x10⁹ $p = 1.6 \frac{1}{10} \text{ m}^2$ Flux density, $B = \frac{\phi}{s}$ = $\frac{1.6 \times 10^{-6}}{6 \times 10^{6}}$ = $\frac{2.8 \times 669 \times 10^{-3} \text{ mJ/m}^2}{\phi}$ 0 $5 = 2.667 \times 10^{16}h^{2.60}T$ $= 2123 + 4$ (b) Field intensity , $H = \frac{B}{\mu} = \frac{a \cdot 64 \cdot x/a^{-3}}{4\pi x/a^{-3}}$ $A + \frac{1}{2}$ At/m 8)a)

eurrent elements: olifferential Fonze belowen Consider First current elements, do find fina bles two current elements Magnetic field at point 2 due to current element at $1, 1, 2, 3, 5$ $d\vec{h_2}^{\tau} = -\frac{T_{t}\,d\vec{L_{t}}\times ~\alpha_{n_{t+1}}^{\tau\tau}}{4\pi~\int R_{t+1}^{\tau\tau}\rangle^2}$ overest element Differential force on a differential $d\vec{r}$, \vec{j} $d\vec{k}\times\vec{s}$

7) b)

The world flow density
$$
(\frac{dR_2}{da})
$$
 at point a equal by current element 1 (2.01).
\n $\phi = \frac{dR_2}{da}$ and $\frac{dR_3}{da}$ and $\frac{dR_2}{da}$
\n $d(d\vec{F}_2) = \frac{1}{a} \frac{dL_3}{da} \times d\vec{F}_2$
\n $d\vec{F}_3 = \frac{1}{a} \phi = \frac{1}{a} \frac{dL_1}{da} \times d\vec{F}_2$
\n $d\vec{F}_3 = \frac{1}{a} \phi = \frac{1}{a} \frac{dL_1}{da} \times \frac{dL_2}{da}$
\n $\therefore \frac{d}{dt} (d\vec{F}_3) = \frac{1}{a} \phi = \frac{2 \cdot T_2}{4a \cdot R_1 a} \frac{dL_1}{da} \times (dL_1 \times a_{R_1 a}^T) \frac{d}{da}$
\n $d(d\vec{F}_1) \neq d(d\vec{F}_2)$ because γ the nonphysical vector γ the current element.

From the differential force, are can get
\n
$$
q_{\text{total}} = \frac{1}{2}mc
$$
\n
$$
p_{\text{total}} = \frac{1}{2}mc
$$
\n
$$
\frac{1}{2} + \frac{1}{2}mc
$$
\n

(b)
\n
$$
\vec{q} \times \vec{r} = \begin{vmatrix} \vec{a} & \vec{a} & \vec{a} \\ \frac{\partial}{\partial x} & \frac{\partial}{\partial y} & \frac{\partial}{\partial z} \\ \frac{\partial}{\partial x} & \frac{\partial}{\partial y} & \frac{\partial}{\partial z} \end{vmatrix} = 2(\vec{a} + \vec{a}) \vec{a} \times \vec{a} + \frac{1}{2} \vec{a} \vec{a} \times \vec{a}
$$

\n
$$
\vec{r} \cdot \vec{r} = \vec{v} \times \vec{h} = 2(\vec{a} + \vec{a}) \vec{a} \times \vec{a} + \frac{1}{2} \vec{a} \vec{a} \times \vec{a}
$$

\n
$$
\vec{r} \cdot \vec{r} = \begin{vmatrix} \vec{r} \cdot \vec{a} & \vec{a} \\ \vec{r} \cdot \vec{a} & \vec{r} \end{vmatrix} = 2(\vec{a} + \vec{a}) \vec{a} \times \vec{a} + \frac{1}{2} \vec{a} \vec{a} \times \vec{a}
$$

\n
$$
\vec{r} \cdot \vec{r} = \begin{vmatrix} \vec{r} \cdot \vec{a} & \vec{r} \\ \vec{r} \cdot \vec{a} & \vec{r} \end{vmatrix} = 2(\vec{a} + \vec{a}) \vec{a} \times \vec{a} + \frac{1}{2} \vec{a} \vec{a} \times \vec{a}
$$

\n
$$
\vec{r} \cdot \vec{r} = \begin{vmatrix} \vec{r} \cdot \vec{a} & \vec{r} \\ \vec{r} \cdot \vec{a} & \vec{r} \end{vmatrix} = \begin{vmatrix} \vec{a} \cdot (\vec{r} - \vec{r}) & \vec{r} \\ \vec{r} \cdot \vec{r} & \vec{r} \end{vmatrix} = \frac{1}{8} \vec{a}
$$

$$
\vec{B} = \vec{U} \times \vec{A} = \begin{bmatrix} a\vec{A} & a\vec{y} & a\vec{z} \\ a\vec{z} & a\vec{y} & a\vec{z} \\ b & b & c\vec{z} \\ f\vec{z} & f\vec{z} & f\vec{z} \end{bmatrix}
$$

\n
$$
= a\vec{A} \begin{bmatrix} 3 & -3 \end{bmatrix} \times f\vec{A} = \begin{bmatrix} a\vec{A} & a\vec{B} \\ f\vec{B} & f\vec{C} \end{bmatrix}
$$

\n
$$
= a\vec{A} \begin{bmatrix} 3 & -3 \end{bmatrix} \times f\vec{A} = \begin{bmatrix} a\vec{B} & -a\vec{B} \\ f\vec{C} & f\vec{C} \end{bmatrix}
$$

\n
$$
= \begin{bmatrix} \vec{B} & -a\vec{B} & a\vec{B} \\ g\vec{C} & g\vec{C} & g\vec{C} \\ h\vec{C} & h\vec{C} & h\vec{C} \end{bmatrix}
$$

\n
$$
= \begin{bmatrix} 3 & 0 & 0 \\ 0 & 0 & 0 \\ 0 & 0 & 0 \end{bmatrix} \times f\vec{A} = \begin{bmatrix} a\vec{A} & a\vec{B} \\ f\vec{A} & f\vec{C} \end{bmatrix}
$$

 $\vec{\tau} = \vec{R} \times \vec{F}$

$$
\vec{F} \text{ is acting on right side only }.
$$

$$
\vec{F} = \vec{J} \vec{c} \times \vec{B}
$$
\n
$$
\vec{B} = 0.4 \vec{a} + 0.6 \vec{a} \vec{y} - 0.742
$$
\n
$$
\vec{B} = 0.4 \vec{a} \vec{y} + 0.6 \vec{a} \vec{y} - 0.742
$$
\n
$$
\vec{F} = \vec{L} \vec{c} \times \vec{B} = \begin{vmatrix} \vec{a} \cdot & \vec{a} \cdot \vec{b} \\ \vec{a} \cdot & \vec{a} \cdot \vec{b} \\ 0.4 & 0.4 & 0.6 & -0.74 \end{vmatrix}
$$
\n
$$
= 0.4 \vec{a} \vec{y} + 0.6 \vec{a} \vec{y} - 0.742
$$
\n
$$
= 0.64 \vec{a} \vec{y} - 0.742
$$
\n
$$
\vec{a} \vec{a} \cdot (0.7) - \vec{a} \cdot (1.250 \cdot 7 - 0) + \vec{a} \cdot (1.250 \cdot 6 - 0.7) + \vec{a} \cdot (1.250 \cdot 6 - 0.7
$$

$$
\frac{se^{kA...}}{B_{N1}} = \left[\frac{e^{2}}{4}, \frac{e^{2}}{4N_{12}}, \frac{e^{2}}{4N_{12}}, \frac{e^{2}}{4N_{12}}\right] \cdot \left(-\frac{e^{2}}{4}\right) \cdot \left(-\frac{e^{2}}{4}\right)^{2} \cdot \left(-\frac{e^{
$$